

16.6 Surface Integrals

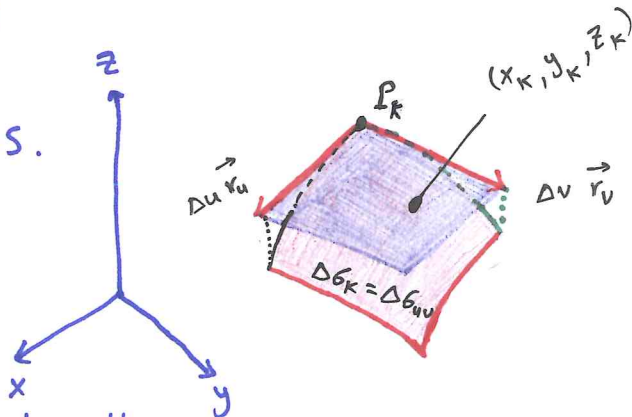
176

- Recall that the line integral is computed over a curve (16.1).
- Now we extend line integral to **surface integral** over surface.
- This helps to compute flow of liquid across membrane (سليمة) or upward force on a falling parachute (إلتراس).

• Suppose there is an electrical charge over a surface S .

• Suppose $G(x, y, z)$ is the function that gives charge density (per unit area) at each point on S .

• We need to calculate the total charge on S .



• Assume, as in section 16.5, that

the surface S is defined parametrically on region R in the uv -plane by:

$$\vec{r}(u, v) = f(u, v)\vec{i} + g(u, v)\vec{j} + h(u, v)\vec{k}, \quad (u, v) \in R$$

• The subdivisions of R divide S into surface elements with area

$$\Delta \sigma_k = \Delta \sigma_{uv} = |\vec{r}_u \times \vec{r}_v| du dv$$

• Choose a point (x_k, y_k, z_k) in the k^{th} surface element (not plane).

• Multiply the value of the function G at (x_k, y_k, z_k) by the area $\Delta \sigma_k$ and form Riemann sum over S :

$$\sum_{k=1}^n G(x_k, y_k, z_k) \Delta \sigma_k$$

• Take limit as $n \rightarrow \infty$ ($\Delta u \rightarrow 0$ and $\Delta v \rightarrow 0$). This limit, if it exists, define the **surface integral** of G over the surface S as

$$\iint_S G(x, y, z) d\sigma = \lim_{n \rightarrow \infty} \sum_{k=1}^n G(x_k, y_k, z_k) \Delta \sigma_k$$

Note The formula for evaluating the surface integral 177 depends on whether S is parametrically, implicitly or explicitly described.

① For a smooth surface S defined parametrically as $\vec{r}(u,v) = f(u,v)\vec{i} + g(u,v)\vec{j} + h(u,v)\vec{k}$, $(u,v) \in R$ and a continuous function $G(x,y,z)$ defined on S , the surface integral of G over S is the double integral over R

$$\iint_S G(x,y,z) d\sigma = \iint_R G(f(u,v), g(u,v), h(u,v)) |\vec{r}_u \times \vec{r}_v| du dv$$

② For a surface S given implicitly by $F(x,y,z) = c$, where F is a continuously diff function and S lying above its closed and bounded shadow region R , the surface integral of the continuous function G over S is the double integral over R

$$\iint_S G(x,y,z) d\sigma = \iint_R G(x,y,z) \frac{|\nabla F|}{|\nabla F \cdot \vec{p}|} dA,$$

where \vec{p} is a unit vector normal to R and $\nabla F \cdot \vec{p} \neq 0$.

③ For a surface given explicitly as $z = f(x,y)$, where f is a continuously diff function over a region R in the xy -plane, the surface integral of the continuous function G over S is the double integral over R

$$\iint_S G(x,y,z) d\sigma = \iint_R G(x,y,f(x,y)) \sqrt{f_x^2 + f_y^2 + 1} dx dy$$

Remark: If S is partitioned by smooth curves S_1, S_2, \dots, S_n nonoverlapping, then

$$\iint_S G d\sigma = \iint_{S_1} G d\sigma + \iint_{S_2} G d\sigma + \dots + \iint_{S_n} G d\sigma$$

Exp Integrate the given function over the given surface:

178

$F(x, y, z) = z$ over the portion of the plane $x + y + z = 4$ that lies above the square $0 \leq x \leq 1$ and $0 \leq y \leq 1$ in the xy -plane.

• Parametrization $\vec{r}(x, y) = x\vec{i} + y\vec{j} + (4 - x - y)\vec{k}$

• $\vec{r}_x = \vec{i} - \vec{k}$
 $\vec{r}_y = \vec{j} - \vec{k}$

$$\vec{r}_x \times \vec{r}_y = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ 1 & 0 & -1 \\ 0 & 1 & -1 \end{vmatrix} = \vec{i} + \vec{j} + \vec{k}$$

$$|\vec{r}_x \times \vec{r}_y| = \sqrt{1+1+1} = \sqrt{3}$$

• $\iint_S F(x, y, z) d\sigma = \iint_R F(x, y, z) |\vec{r}_x \times \vec{r}_y| dx dy$
 $= \sqrt{3} \int_0^1 \int_0^1 (4 - x - y) dx dy = \int_0^1 \sqrt{3} \left(\frac{7}{2} - y\right) dy = 3\sqrt{3}$

Exp Integrate $G(x, y, z) = x + y + z$ over the portion of the plane $2x + 2y + z = 2$ that lies in the first octant.

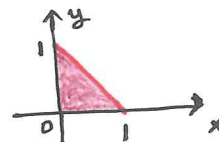
• $f(x, y, z) = 2x + 2y + z \Rightarrow \nabla f = 2\vec{i} + 2\vec{j} + \vec{k}$

• $z = 2 - 2x - 2y \Rightarrow G(x, y, z) = x + y + (2 - 2x - 2y)$
 $= 2 - x - y \Rightarrow \vec{P} = \vec{k}$

• $|\nabla f| = \sqrt{4+4+1} = 3$ and $|\nabla f \cdot \vec{P}| = |1| = 1$

• $\iint_S G(x, y, z) d\sigma = \iint_R (2 - x - y) \frac{|\nabla f|}{|\nabla f \cdot \vec{P}|} dA$
 $= \int_0^1 \int_0^{1-x} (2 - x - y) 3 dy dx$
 $= 3 \int_0^1 \left(\frac{3}{2} - 2x + \frac{x^2}{2}\right) dx = 2$

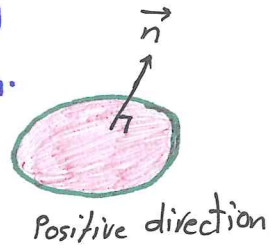
when $z = 0 \Rightarrow$
 $x + y = 1 \Rightarrow$
 $y = 1 - x$



Orientation

179

- A smooth surface S is **orientable** (or **two-sided**) if it is possible to define a field \vec{n} of unit normal vectors on S that varies continuously with position.
- Any patch or subportion of an orientable surface is orientable.
- Spheres and smooth closed surfaces (enclose solids) like cones are orientable.
- The surface together with its normal field is called an **oriented surface**.
- The vector \vec{n} at any point is called the **positive direction** at that point.



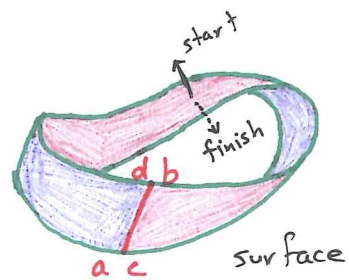
Exp Give an example of nonorientable (or one-sided) surface.

- The Möbius band is not orientable



Paper

⇒ Match a with c
and b with d



surface

- No matter where we start to construct a continuous unit normal field, moving the vector continuously around the surface will return the vector to the starting point with a direction apposit to the one we start with.
- The vector at that point can not point both ways
- Hence, no such field exists.

Surface Integral for Flux

180

- Recall that, from section 16.2, the flux of a two-dimensional field \vec{F} across a plane curve C is $\int_C \vec{F} \cdot \vec{n} \, ds$.

Def The flux of a three-dimensional vector field \vec{F} across an oriented surface S in the direction of \vec{n} is

$$\text{Flux} = \iint_S \vec{F} \cdot \vec{n} \, d\sigma$$

- If \vec{F} is the velocity field of a three-dimensional fluid flow, then the flux of F across S is the net rate at which fluid is crossing S in the chosen positive direction

Exp* Find the flux $\vec{F} = z\vec{i} + x\vec{j} - 3z\vec{k}$ outward (normal away from the x -axis) through the surface cut from the parabolic cylinder $z = 4 - y^2$ by the planes $x=0, x=1, z=0$.

S₁ Parametrization: $\vec{r}(x,y) = x\vec{i} + y\vec{j} + (4-y^2)\vec{k}, 0 \leq x \leq 1$

- when $z=0 \Rightarrow 0 = 4 - y^2 \Rightarrow y = \pm 2 \Rightarrow -2 \leq y \leq 2$

- $\vec{r}_x = \vec{i}$ and $\vec{r}_y = \vec{j} - 2y\vec{k}$

$$\vec{r}_x \times \vec{r}_y = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ 1 & 0 & 0 \\ 0 & 1 & -2y \end{vmatrix} = 2y\vec{j} + \vec{k}$$

$$\vec{n} = \frac{\vec{r}_x \times \vec{r}_y}{|\vec{r}_x \times \vec{r}_y|}$$

- Flux = $\iint_S \vec{F} \cdot \vec{n} \, d\sigma = \int_0^1 \int_{-2}^2 \vec{F} \cdot \frac{\vec{r}_x \times \vec{r}_y}{|\vec{r}_x \times \vec{r}_y|} |\vec{r}_x \times \vec{r}_y| \, dy \, dx$
 $= \int_0^1 \int_{-2}^2 [2xy - 3(4-y^2)] \, dy \, dx = \int_0^1 -32 \, dx = -32$

S_2 • The gradient of $g(x, y, z) = y^2 + z = 4$ is

181

$$\nabla g = 2y \vec{j} + \vec{k} \quad \text{with} \quad |\nabla g| = \sqrt{4y^2 + 1}$$

• The outward normal field on S is

$$\vec{n} = \frac{\nabla g}{|\nabla g|} = \frac{2y \vec{j} + \vec{k}}{\sqrt{4y^2 + 1}}$$

• With $\vec{p} = \vec{k}$, we have $|\nabla g \cdot \vec{p}| = |1| = 1$

$$\text{Flux} = \iint_S \vec{F} \cdot \vec{n} \, d\sigma = \iint_R \vec{F} \cdot \frac{\nabla g}{|\nabla g|} \frac{|\nabla g|}{|\nabla g \cdot \vec{p}|} \, dA$$

$$= \iint_R (2xy - 3z) \, dA$$

$$= \int_0^1 \int_{-2}^2 (2xy - 12 + 3y^2) \, dy \, dx$$

$$= \int_0^1 -32 \, dx$$

$$= -32$$

• $\vec{F} = z^2 \vec{i} + x \vec{j} - 3z \vec{k}$
 $= (4 - y^2)^2 \vec{i} + x \vec{j} - 3(4 - y) \vec{k}$

• $\vec{F} \cdot \nabla g = 2xy - 3(4 - y^2)$

• when $z = 0 \Rightarrow$
 $y^2 = 4 \Rightarrow y = \pm 2$

Moments and Masses of Thin shells (similar to section 16.1) 182

Thin shells like bowl (كؤن قصبية), drums (طبول), dome (قبة)....

• Mass $M = \iint_S \delta \, d\sigma$ where $\delta = \delta(x, y, z)$ is density at (x, y, z) as mass per unit area.

• First moments about the coordinate planes

$$M_{yz} = \iint_S x \delta \, d\sigma, \quad M_{xz} = \iint_S y \delta \, d\sigma, \quad M_{xy} = \iint_S z \delta \, d\sigma$$

• Coordinates of center of mass

$$\bar{x} = \frac{M_{yz}}{M}, \quad \bar{y} = \frac{M_{xz}}{M}, \quad \bar{z} = \frac{M_{xy}}{M}$$

• Moments of inertia about coordinate axes

$$I_x = \iint_S (y^2 + z^2) \delta \, d\sigma, \quad I_y = \iint_S (x^2 + z^2) \delta \, d\sigma$$

$$I_z = \iint_S (x^2 + y^2) \delta \, d\sigma, \quad I_L = \iint_S r^2 \delta \, d\sigma \quad \text{where}$$

$r(x, y, z)$ is the distance from point (x, y, z) to line L .

Notes [1] These formulas are like those for line integrals in section 16.1

[2] Their derivations are similar to those in section 6.6

Exp Find the centroid $(\bar{x}, \bar{y}, \bar{z})$ of the portion of the sphere $x^2 + y^2 + z^2 = a^2$ that lies in the first octant.

183

$$\bullet f(x, y, z) = x^2 + y^2 + z^2 = a^2 \Rightarrow \nabla f = 2x \vec{i} + 2y \vec{j} + 2z \vec{k}$$
$$|\nabla f| = \sqrt{4x^2 + 4y^2 + 4z^2} = 2a$$

$$\bullet \text{To find the integral for } M_{xy}, \text{ we take } \vec{p} = \vec{k}$$
$$\Rightarrow |\nabla f \cdot \vec{p}| = |2z| = 2z$$

$$\bullet \text{Since } z \geq 0 \Rightarrow d\sigma = \frac{|\nabla f|}{|\nabla f \cdot \vec{p}|} dA = \frac{2a}{2z} dA = \frac{a}{z} dA$$

$$\bullet \text{Mass } M = \iint_S \delta d\sigma = \delta \iint_S d\sigma = a\delta \iint_R \frac{1}{z} dA$$
$$= a\delta \int_0^{\frac{\pi}{2}} \int_0^a \frac{1}{\sqrt{a^2 - r^2}} r dr d\theta = a\delta \int_0^{\frac{\pi}{2}} a d\theta = \frac{\delta \pi a^2}{2}$$

$$\bullet M_{xy} = \iint_S z \delta d\sigma = \delta \iint_R z \frac{a}{z} dA = a\delta \iint_R dA$$
$$= a\delta \int_0^{\frac{\pi}{2}} \int_0^a r dr d\theta = \frac{\delta \pi a^3}{4}$$

$$\bullet \bar{z} = \frac{M_{xy}}{M} = \frac{\delta \pi a^3}{4} \frac{2}{\delta \pi a^2} = \frac{a}{2}$$

Because of symmetry $\bar{x} = \bar{y} = \bar{z} = \frac{a}{2} \Rightarrow \text{centroid} = (\frac{a}{2}, \frac{a}{2}, \frac{a}{2})$

Exp Find the moment of inertia about z-axis of a 184 thin shell of constant density δ cut from the cone $4x^2 + 4y^2 - z^2 = 0$, $z \geq 0$ by the circular cylinder $x^2 + y^2 = 2x$

• $f(x, y, z) = 4x^2 + 4y^2 - z^2 = 0$

$\nabla f = 8x \vec{i} + 8y \vec{j} - 2z \vec{k}$

$|\nabla f| = \sqrt{64x^2 + 64y^2 + 4z^2}$

$= 2\sqrt{16x^2 + 16y^2 + z^2}$

$= 2\sqrt{4z^2 + z^2} = 2\sqrt{5} z$

• Take $\vec{p} = \vec{k} \Rightarrow |\nabla f \cdot \vec{p}| = |-2z| = 2z$

• $d\sigma = \frac{|\nabla f|}{|\nabla f \cdot \vec{p}|} dA = \frac{2\sqrt{5} z}{2z} dA = \sqrt{5} dA$

• $I_z = \iiint_S (x^2 + y^2) \delta d\sigma = \sqrt{5} \delta \iint_R (x^2 + y^2) dx dy$

$= \sqrt{5} \delta \int_{-\frac{\pi}{2}}^{\frac{\pi}{2}} \int_0^{2\cos\theta} r^2 r dr d\theta$

$= \frac{3\sqrt{5}\pi\delta}{2}$

