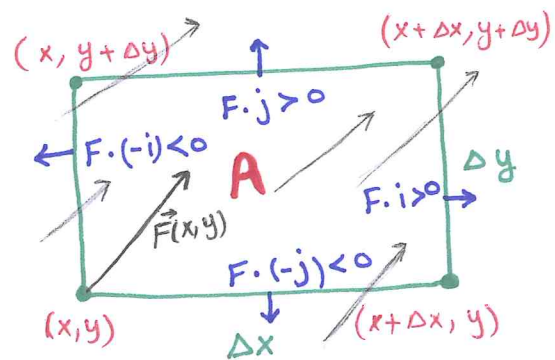


- Recall that if \vec{F} is a conservative vector field, then $\vec{F} = \nabla f$ for a diff function f . Thus, we calculate the line integral of \vec{F} over any path C joining A to B as

$$\text{work} = \int_C \vec{F} \cdot d\vec{r} = f(B) - f(A)$$
- In this section we derive a method (Green's Theorem) to compute a work or flux integral over a closed curve C in the plane when the field \vec{F} is not conservative.
- We will see Green's Theorem applies to any vector field, but we focus on velocity fields of fluid flows like a liquid flow (not compressible) and gas flow (compressible) as they are easy to visualize.

Divergence:

- Let $\vec{F}(x,y) = M(x,y)\vec{i} + N(x,y)\vec{j}$ be a velocity field of a fluid flowing in the plane.
- Suppose the first partial derivatives of M and N are continuous at each point of a region R .
- Let (x,y) be a point in R and a corner point of a rectangle A as in this figure, where A lies entirely in R .
- The small rectangle A has sides Δx and Δy parallel to the coordinate axes.
- Assume the components M and N do not change sign throughout a small region containing A .



• The rate at which fluid leaves the rectangle across the rectangle is approximately

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$$\approx \text{top edge flow} + \text{bottom edge flow} + \text{right edge flow} + \text{left edge flow}$$

$$\approx \vec{F}(x, y + \Delta y) \cdot \vec{j} \Delta x + \vec{F}(x, y) \cdot (-\vec{j}) \Delta x + F(x + \Delta x, y) \cdot \vec{i} \Delta y + F(x, y) \cdot (-\vec{i}) \Delta y$$

$$= N(x, y + \Delta y) \Delta x - N(x, y) \Delta x + M(x + \Delta x, y) \Delta y - M(x, y) \Delta y$$

$$= [N(x, y + \Delta y) - N(x, y)] \Delta x + [M(x + \Delta x, y) - M(x, y)] \Delta y$$

$$= \frac{N(x, y + \Delta y) - N(x, y)}{\Delta y} \Delta x \Delta y + \frac{M(x + \Delta x, y) - M(x, y)}{\Delta x} \Delta x \Delta y$$

$$\approx N_y \Delta x \Delta y + M_x \Delta x \Delta y$$

Hence, the net effect of the flow rates or the

$$\text{Flux across rectangle boundary} \approx (M_x + N_y) \Delta x \Delta y$$

• To estimate the total flux per unit area (or flux density) for the rectangle, we divide by $\Delta x \Delta y$ to get:

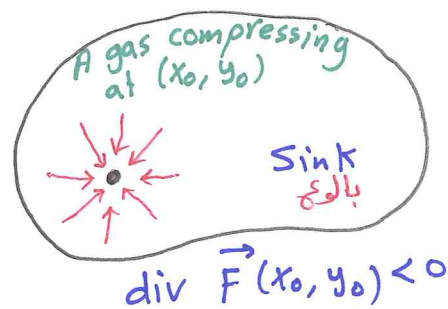
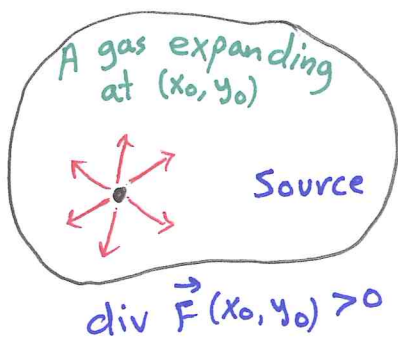
$$\frac{\text{Flux across rectangle boundary}}{\text{Rectangle area}} \approx M_x + N_y$$

• Finally, let $\Delta x \rightarrow 0$ and $\Delta y \rightarrow 0$ to define the flux density of \vec{F} at the point (x, y) or the divergence of \vec{F} at (x, y) :

$$\boxed{\text{div } \vec{F} = M_x + N_y}$$

Remark: • A gas is compressible and liquid is not. 160

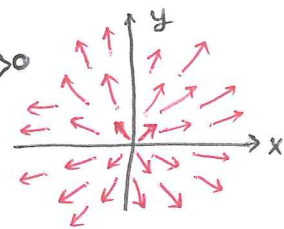
- If gas is **expanding** at the point (x_0, y_0) , then lines of flow would diverge there and gas would be flowing out of a small rectangle about (x_0, y_0) which makes $\text{div } \vec{F}(x_0, y_0) > 0$.
- If gas is **compressing** at the point (x_0, y_0) , then lines of flow would be flowing in about (x_0, y_0) which makes $\text{div } \vec{F}(x_0, y_0) < 0$.



Exp The following vector fields represent the velocity of a gas flowing in the xy -plane. Find the divergence of each vector field and interpret its physical meaning.

[a] Uniform expansion $\vec{F}(x, y) = cx\vec{i} + cy\vec{j}, c > 0$

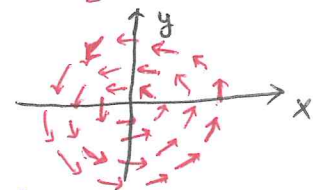
$$\text{div } \vec{F} = M_x + N_y = c + c = 2c > 0$$



[b] Uniform rotation $\vec{F}(x, y) = -cy\vec{i} + cx\vec{j}$

$$\text{div } \vec{F} = M_x + N_y = 0 + 0 = 0$$

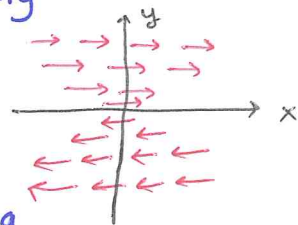
The gas is neither expanding nor compressing



[c] Shearing flow $\vec{F}(x, y) = y\vec{i}$

$$\text{div } \vec{F} = M_x + N_y = 0 + 0 = 0$$

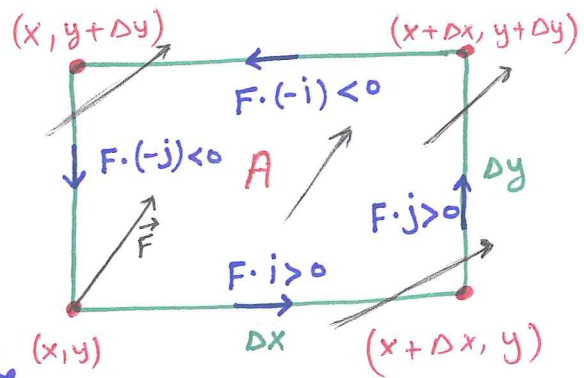
The gas is neither expanding nor compressing



Spin around an axis: The k-component of Curl

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- After divergence, we need a second idea for Green's Theorem which is the **circulation density** of a vector field $\vec{F} = M\vec{i} + N\vec{j}$ at point (x, y) .



- Same as before, but we approximate the rate of flow along each edge in the directions of blue arrows

$$\begin{aligned} &\approx \vec{F}(x, y + \Delta y) \cdot (-\vec{i}) \Delta x + \vec{F}(x, y) \cdot \vec{i} \Delta x + \vec{F}(x + \Delta x, y) \cdot \vec{j} \Delta y + \vec{F}(x, y) \cdot (-\vec{j}) \Delta y \\ &= -M(x, y + \Delta y) \Delta x + M(x, y) \Delta x + N(x + \Delta x, y) \Delta y - N(x, y) \Delta y \\ &= - \left[\frac{M(x, y + \Delta y) - M(x, y)}{\Delta y} \right] \Delta x \Delta y + \frac{[N(x + \Delta x, y) - N(x, y)]}{\Delta x} \Delta x \Delta y \end{aligned}$$

$$\approx -M_y \Delta x \Delta y + N_x \Delta x \Delta y$$

Hence, the net circulation counterclockwise orientation is

$$\text{Circulation around rectangle} \approx (N_x - M_y) \Delta x \Delta y$$

- To estimate the circulation density of \vec{F} at the point (x, y) , we divide by $\Delta x \Delta y$ to get

$$\frac{\text{Circulation around rectangle}}{\text{Rectangle area}} \approx N_x - M_y$$

- Finally, let $\Delta x \rightarrow 0$ and $\Delta y \rightarrow 0$ to define the circulation density (or the k-component of the curl) of a vector field \vec{F} at (x, y) is

$$\boxed{(\text{curl } \vec{F}) \cdot \vec{k} = N_x - M_y}$$

$\vec{k} \perp \text{obs}$

Exp Find the circulation density (with interpretation) for the vector fields described in Exp':

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(a) Uniform expansion $\vec{F}(x,y) = cx \vec{i} + cy \vec{j}$ $M = cx$
 $N = cy$

$(\text{curl } \vec{F}) \cdot \vec{k} = N_x - M_y = 0 - 0 = 0$

• The gas is not circulating at very small scales.

(b) Uniform rotation $\vec{F}(x,y) = -cy \vec{i} + cx \vec{j}$ $M = -cy$
 $N = cx$

$(\text{curl } \vec{F}) \cdot \vec{k} = N_x - M_y = c + c = 2c$

• The circulation density is constant and there is a rotation at every point

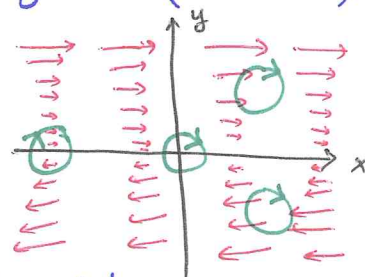
• If $c > 0$, then the rotation is counterclockwise and if $c < 0$, then the rotation is clockwise.

(c) Shearing flow $\vec{F}(x,y) = y \vec{i}$ $M = y$
 $N = 0$

$(\text{curl } \vec{F}) \cdot \vec{k} = N_x - M_y = 0 - 1 = -1$

• The circulation density is constant and negative (clockwise)

• The average effect of the fluid flow is to push fluid clockwise around each of the small circles



• The rate of rotation is the same at each point.

Recall that • the curve C is simple if it does not cross itself. (147) page

• the outward flux of \vec{F} across C is (see also page 147)

$$\oint_C M dy - N dx = \int_C \vec{F} \cdot \vec{n} ds$$

• the circulation around the curve C that starts and ends at same point is the flow integral $\int_C \vec{F} \cdot \vec{T} ds$ (see page 145)

Th (Green's Theorem)

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Let C be a piecewise smooth and simple closed curve enclosing a region R in the plane.

Let $\vec{F} = M\vec{i} + N\vec{j}$ be a vector field with M and N having continuous first partial derivatives in an open region containing R .

Then • the outward flux of \vec{F} across C equals the double integral of $\text{div } \vec{F}$ over the region R enclosed by C :

Normal form

$$\oint_C \vec{F} \cdot \vec{n} \, ds = \oint_C M \, dy - N \, dx = \iint_R (M_x + N_y) \, dx \, dy \quad *^1$$

Outward flux Divergence integral

• the counterclockwise circulation of \vec{F} around C equals the double integral of $(\text{curl } \vec{F}) \cdot \vec{k}$ over R :

tangent form

$$\oint_C \vec{F} \cdot \vec{T} \, ds = \oint_C M \, dx + N \, dy = \iint_R (N_x - M_y) \, dx \, dy \quad *^2$$

Counterclockwise circulation Curl integral

Notes: • $*^1$ and $*^2$ are equivalent. That is, applying $*^1$ to the field $G^1 = N\vec{i} - M\vec{j}$ gives $*^2$ and applying $*^2$ to the field $G^2 = -N\vec{i} + M\vec{j}$ gives $*^1$.

• The simple closed curve C can be traversed in two directions:

① The curve C is traversed counterclockwise (and called positively oriented) if the region R enclosed is always to the left of an object as it moves along the path.

② Otherwise, C is traversed clockwise (and called negatively oriented).

Exp Verify both forms of Green's Theorem for the vector field $\vec{F} = -x^2y \vec{i} + xy^2 \vec{j}$ and the region R is the disk $x^2 + y^2 \leq 4$ bounded by the circle $C: \vec{r} = (2\cos t)\vec{i} + (2\sin t)\vec{j}, 0 \leq t \leq 2\pi$.

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• $x = 2\cos t$ and $y = 2\sin t \Rightarrow dx = -2\sin t dt$
 $dy = 2\cos t dt$

• $M = -x^2y = -8\cos^2 t \sin t$
 $N = xy^2 = 8\cos t \sin^2 t$

• $M_x = -2xy, M_y = -x^2, N_x = y^2, N_y = 2xy$

• Flux (form *1): $\oint_C Mdy - Ndx = \int_0^{2\pi} (-16\cos^3 t \sin t + 16\cos t \sin^3 t) dt$
 $= [4\cos^4 t + 4\sin^4 t]_0^{2\pi} = 0$

$\iint_R (M_x + N_y) dx dy = \iint_R (-2xy + 2xy) dx dy = 0$

• Circulation (form *2):

$\oint_C M dx + N dy = \int_0^{2\pi} (16\cos^2 t \sin^2 t + 16\cos^2 t \sin^2 t) dt$
 $= \int_0^{2\pi} 32\cos^2 t \sin^2 t dt = \int_0^{2\pi} 16\sin^2 2t dt$
 $= 4 \int_0^{4\pi} \sin^2 u du = 4 \left[\frac{u}{2} - \frac{\sin 2u}{4} \right]_0^{4\pi} = 8\pi$

$\iint_R (N_x - M_y) dx dy = \iint_R (y^2 + x^2) dx dy = \int_0^{2\pi} \int_0^2 r^2(r) dr d\theta$
 $= \int_0^{2\pi} 4 d\theta = 8\pi$

Exp Use Green's Theorem to find the counterclockwise circulation and outward flux for the vector field $\vec{F} = (x^2 + 4y)\vec{i} + (x + y^2)\vec{j}$ and the curve

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C : the square bounded by $x=0$, $x=1$, $y=0$, $y=1$.

• $M = x^2 + 4y \Rightarrow M_x = 2x$ and $M_y = 4$

$N = x + y^2 \Rightarrow N_x = 1$ and $N_y = 2y$

• Flux = $\iint_R (M_x + N_y) dx dy = \iint_R (2x + 2y) dx dy$
 $= \int_0^1 \int_0^1 (2x + 2y) dx dy = \int_0^1 (x^2 + 2xy) \Big|_0^1 dy = \int_0^1 (1 + 2y) dy = 2$

• Circulation = $\iint_R (N_x - M_y) dx dy = \iint_R (1 - 4) dx dy$
 $= \int_0^1 \int_0^1 -3 dx dy = -3$

Exp Evaluate the integral $\oint_C (3y dx + 2x dy)$

• Apply Green's Theorem form \ast^2

• $M = 3y \Rightarrow M_y = 3$

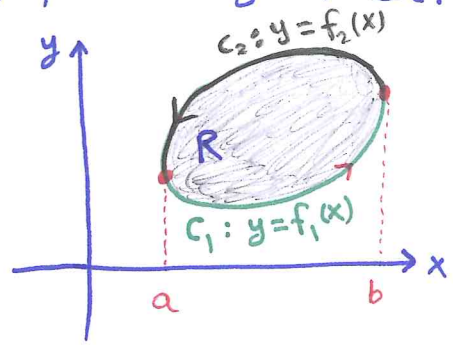
$N = 2x \Rightarrow N_x = 2$

• $\oint_C (3y dx + 2x dy) = \iint_R M dx + N dy = \iint_R (N_x - M_y) dx dy$
 $= \iint_R (2 - 3) dx dy$
 $= \int_0^\pi \int_0^{\sin x} (-1) dx dy$
 $= - \int_0^\pi \sin x dx = -2$

Proof of Green's Theorem for special Regions

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- Let C be smooth simple closed curve in xy -plane as given here:
- Let R be the region enclosed by C .
- Given $\vec{F} = M\vec{i} + N\vec{j}$ with M, N and their first partial derivatives are continuous at every point in some open region containing C and R .



- We need to prove the circulation-curl form \ast^2 :

$$\oint M dx + N dy = \iint_R (N_x - M_y) dx dy$$

- Note that the curve C consists of two directed parts:

$$C_1: y = f_1(x), \quad a \leq x \leq b \quad \text{and}$$

$$C_2: y = f_2(x), \quad a \leq x \leq b$$

- $\forall x \in [a, b] \Rightarrow \int_{f_1(x)}^{f_2(x)} M_y dy = M(x, y) \Big|_{y=f_1(x)}^{y=f_2(x)} = M(x, f_2(x)) - M(x, f_1(x))$

$$\Rightarrow \int_a^b \int_{f_1(x)}^{f_2(x)} M_y dy dx = \int_a^b [M(x, f_2(x)) - M(x, f_1(x))] dx$$

$$= - \int_b^a M(x, f_2(x)) dx - \int_a^b M(x, f_1(x)) dx$$

$$= - \int_{C_2} M dx - \int_{C_1} M dx = - \oint_C M dx$$

- Hence, $\oint_C M dx = \iint_R -M_y dx dy \dots \textcircled{1}$

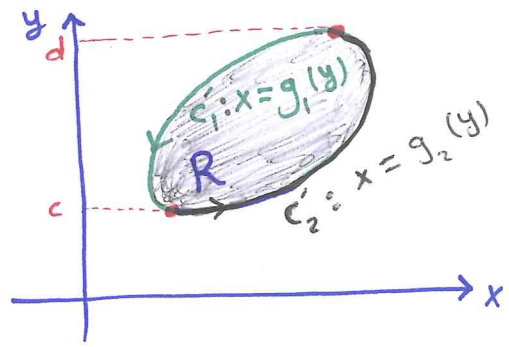
• Now we derive the other half by integrating N_x w.r.t x then w.r.t y .

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• Note that the curve C consists of two directed parts:

$$C_1: x = g_1(y), \quad c \leq y \leq d \quad \leftarrow$$

$$C_2: x = g_2(y), \quad c \leq y \leq d \quad \rightarrow$$



$$\forall y \in [c, d] \Rightarrow \int_{g_1(y)}^{g_2(y)} N_x dx = N(x, y) \Big|_{x=g_1(y)}^{x=g_2(y)} = N(g_2(y), y) - N(g_1(y), y)$$

$$\Rightarrow \int_c^d \int_{g_1(y)}^{g_2(y)} N_x dx dy = \int_c^d [N(g_2(y), y) - N(g_1(y), y)] dy$$

$$= \int_c^d N(g_2(y), y) dy + \int_d^c N(g_1(y), y) dy$$

$$= \int_{C_2} N dy + \int_{C_1} N dy = \oint_C N dy$$

• Hence, $\oint_C N dy = \iint_R N_x dx dy$ ----- (2)

• Thus, adding (1) + (2) gives:

$$\oint M dx + \oint N dy = \oint M dx + N dy$$

$$= \iint_R (N_x - M_y) dx dy$$