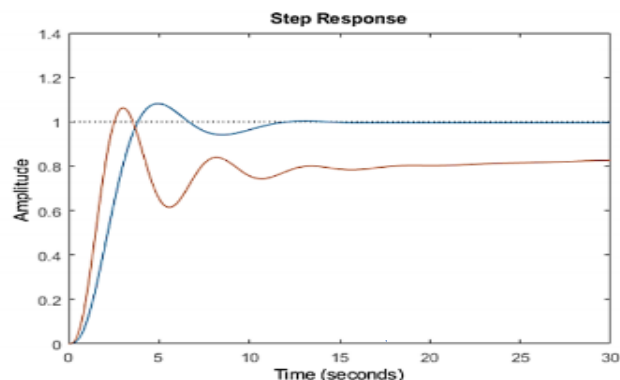


Design of a Servo System (Tracking System):

The tracking system is a control action aims to force the output response $y(t)$ to follow the desired input $r(t)$ with a required performance.



There are two cases for design the tracking system:

- Find the eigenvalues for the open loop system $|sI - A| = 0$
- Check if there is any eigenvalues at the origin or not i.e. find the Type number?
- Remember this:

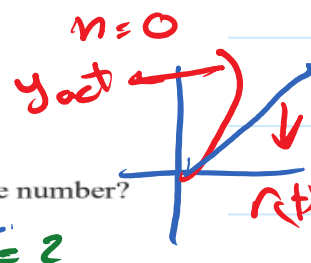


TABLE 7.2 Relationships between input, system type, static error constants, and steady-state errors

Input	Steady-state error formula	Type 0		Type 1		Type 2	
		Static error constant	Error	Static error constant	Error	Static error constant	Error
Step, $u(t)$	$\frac{1}{1+K_p}$	$K_p = \text{Constant}$	$\frac{1}{1+K_p}$	$K_p = \infty$	0	$K_p = \infty$	0
Ramp, $tu(t)$	$\frac{1}{K_v}$	$K_v = 0$	∞	$K_v = \text{Constant}$	$\frac{1}{K_v}$	$K_v = \infty$	0
Parabola, $\frac{1}{2}t^2u(t)$	$\frac{1}{K_a}$	$K_a = 0$	∞	$K_a = 0$	∞	$K_a = \text{Constant}$	$\frac{1}{K_a}$

If the steady state error is equal zero based on the Type number use the first case. Otherwise use the second case.

Type number is # of poles at origin (n)

$$G(s) = \frac{(s+3)}{s^2(s+1)} \quad n=2$$

$$(n) = 2$$

step

$$K_p = \lim_{s \rightarrow 0} G(s) = \lim_{s \rightarrow 0} \frac{1}{(s+2)(s+3)} = \frac{1}{(2)(3)}$$

$$e_{ss} = \frac{1}{1+K_p} = \frac{1}{1+\frac{1}{6}} = \frac{6}{7}$$

$$k_p = \lim_{s \rightarrow 0} G(s), \quad \text{ESS}(\infty) = \frac{1}{1+k_p}$$

$$k_v = \lim_{s \rightarrow 0} s G(s), \quad \text{ESS}(\infty) = \frac{1}{k_v}$$

$$k_a = \lim_{s \rightarrow 0} s^2 G(s), \quad \text{ESS}(\infty) = \frac{1}{k_a}$$

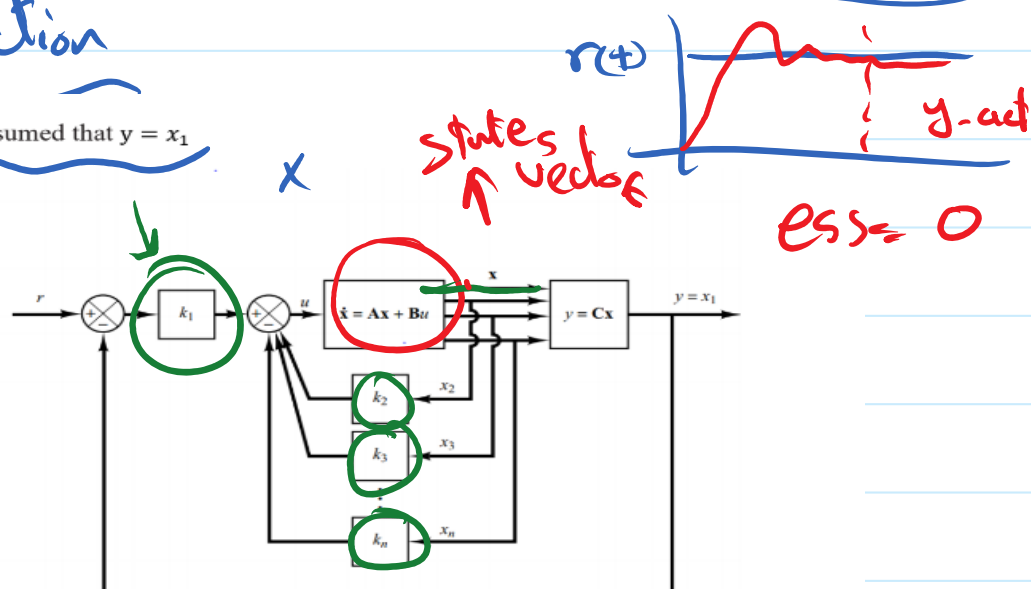
$$\begin{aligned} \dot{x} &= Ax + Bu & \text{--- (1)} \\ y &= Cx & \text{--- (2)} \end{aligned}$$

To Design the tracking Sys. there are two cases:-

Case 1 Design tracking Sys. without integral action

Here we assumed that $y = x_1$

$$y = x_1$$

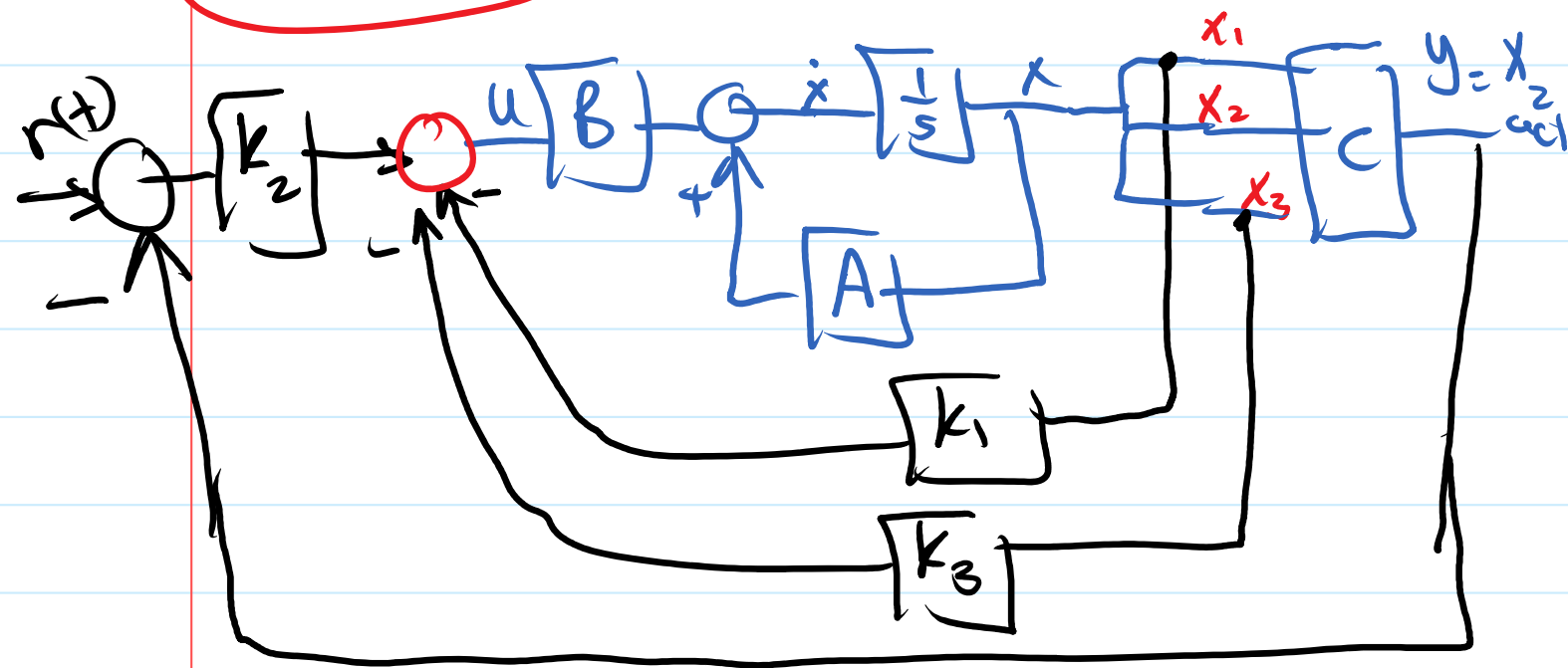


$$u = -k_1 x_1 - k_2(r - x_2) - k_3 x_3$$

$$= -[k_1 \dots k_3]x + k_2 r$$

number of state 3

$$y = x_2 = r(t)$$



* To determine which case is suitable you must check the following

* $|\lambda I - A| = 0$ — eigenvalue for open loop sys.

You can determine the type number (n) from Eq (4)

$r(t)$:- step input

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ 2 & 3 \end{bmatrix} x + \begin{bmatrix} 0 \\ 2 \end{bmatrix} u$$

$$y = \begin{bmatrix} 0 & 1 \end{bmatrix} x$$

char. Eq

$$|\lambda I - A| = 0 \Rightarrow \begin{vmatrix} \lambda & -1 \\ -2 & \lambda - 3 \end{vmatrix} = \lambda^2 - 3\lambda - 2 = 0$$

$$\lambda_1 = 3.56$$

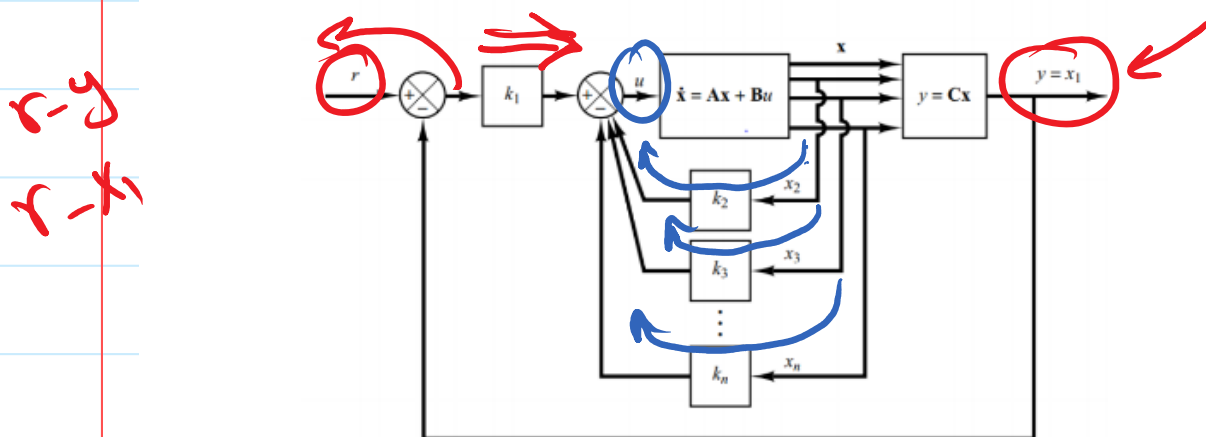
$$\lambda_2 = -0.56$$

$$n = 0$$

$r(t)$ = Step input , $n = 0$, $e_{ss}(t) = \text{Constant}$
 we must use Case (2)

Design tracking sys if $y = x_1 = r(t)$
act

Here we assumed that $y = x_1$



$$\begin{aligned}
 u &= -k_2 x_2 - k_3 x_3 - \dots - k_n x_n + k_1 (r - x_1) \\
 &= -k_1 x_1 - k_2 x_2 - \dots - k_n x_n + k_1 r \\
 &= -[k_1 \dots k_n] \begin{bmatrix} x_1 \\ \vdots \\ x_n \end{bmatrix} + k_1 r \\
 &= -KX + k_1 r \\
 K &= [k_1 \dots k_n], \quad X \text{ is state vector}
 \end{aligned}$$

$r(t)$ r \downarrow
step input

$$r(t) = r, \quad r(\infty) = r$$

$$\textcircled{1} \quad u = -kx + k_1 r \quad \text{(Control input)}$$

$$\dot{x} = Ax + Bu \quad \textcircled{2}$$

$$y = Cx$$

Sub Eq ① into Eq ②

$$\dot{x} = Ax + B(-kx + k_1 r)$$

closed loop
dynamic
at time

$$\rightarrow \dot{x} = (A - BK)x + Bk_1 r \quad \textcircled{3}$$

Note: To design sys. will be Asy stable
 $y(\infty)$ will approach constant value r ,
and $u(\infty)$ will approach zero, when
 r is step input

at $t = \infty$

$$\rightarrow \dot{x}(\infty) = (A - BK)x(\infty) + Bk_1 r(\infty) \quad \textcircled{4}$$

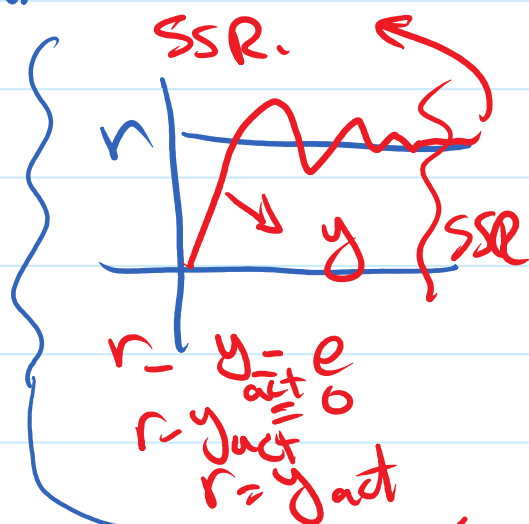
$$\textcircled{3} - \textcircled{4}$$

$$\dot{x}(t) - \dot{x}(\infty) = (A - BK)(x(t) - x(\infty)) + \cancel{Bk_1 r(t)} - \cancel{Bk_1 r(\infty)}$$

$$\dot{e}(t) = (A - BK)e(t)$$

$$e(t) :- x(t) - x(\infty)$$

$$\dot{e}(t) :- \dot{x}(t) - \dot{x}(\infty)$$

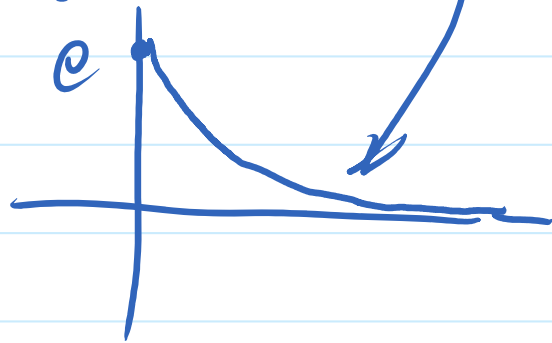


$$(A-BK) \quad x \quad \dot{x} = x$$

$$\dot{e}(t) = (A-BK)e(t) \quad \text{--- (5)}$$

This is similar to regulator equation

if the eigenvalues of $(A-BK)$ in the Left Side Plane (Asymptotically)



Therefore $e(t)$ will go to Zero

$$e(t) = [x(t) - x(\infty)]$$

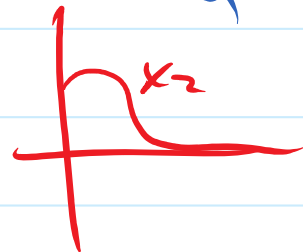
$$e = \begin{bmatrix} e_1 \\ e_2 \\ e_3 \end{bmatrix} = \begin{bmatrix} x_1(t) - x_1(\infty) \\ x_2(t) - x_2(\infty) \\ x_3(t) - x_3(\infty) \end{bmatrix}$$

Arrows point from the terms in the vector to their corresponding state variables: $x_1(t) \rightarrow r(t)$, $x_2(t) \rightarrow x_2$, and $x_3(t) \rightarrow \text{Zero}$.

$$e(t) = r(t) - y(t)$$

if we have then states

$$y_{act} = r(t) = x_1$$



Case 2:- Tracking Sys with an integral action

* This Case is used when the $ess(\infty)$ is Constant and we would like to improve the $ess(\infty)$ to Zero.

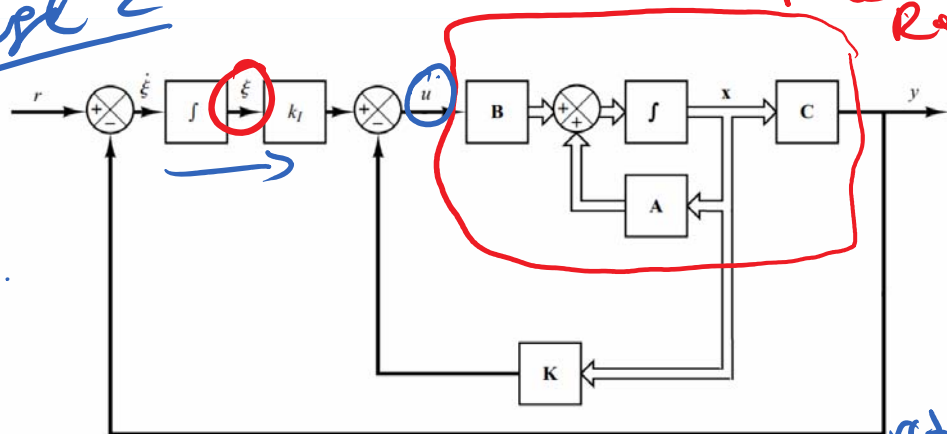
$$\underline{n=0} \quad r = \text{step input} \Rightarrow ess(\infty) = \text{constant}$$

$$\textcircled{n=1} \leftarrow ess(\infty) = \text{Zero}$$

* To determine which Case is required

$$|\lambda I - A| = 0 \rightarrow \text{1st (type number)}$$

Case 2

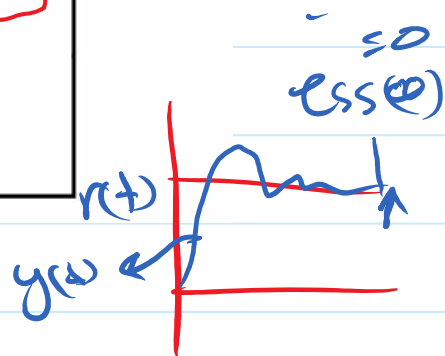


$$y = x = r(t)$$

$$\dot{x} = Ax + Bu \quad \text{--- (1)}$$

$$y = Cx \quad \text{--- (2)}$$

$$\rightarrow u = -Kx + k_i \int \text{--- (3)} \quad k_i = [k_1 \dots k_n]$$



k_i is gain integrator

$$\dot{x} = Ax + Bu \quad \text{--- (1)}$$

from the tracking Control Scheme

$$\dot{\xi} = r - y = r - Cx \quad \text{--- (4)}$$

$$\begin{bmatrix} \dot{x}(t) \\ \dot{\xi}(t) \end{bmatrix} = \begin{bmatrix} A & \vec{0} \\ -C & 0 \end{bmatrix} \begin{bmatrix} x(t) \\ \xi(t) \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} u(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} r(t) \quad \text{--- (5)}$$

$n \times n$ $n \times 1$ $n \times r$ $r(t)$
 $n \times n$ $p \times 1$

at $t \rightarrow \infty$

$$\begin{bmatrix} \dot{x}(\infty) \\ \dot{\xi}(\infty) \end{bmatrix} = \begin{bmatrix} A & \vec{0} \\ -C & 0 \end{bmatrix} \begin{bmatrix} x(\infty) \\ \xi(\infty) \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} u(\infty) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} r(\infty) \quad \text{--- (6)}$$

(5) - (6)

$$\begin{bmatrix} \dot{x}(t) - \dot{x}(\infty) \\ \dot{\xi}(t) - \dot{\xi}(\infty) \end{bmatrix} = \begin{bmatrix} A & \vec{0} \\ -C & 0 \end{bmatrix} \begin{bmatrix} x(t) - x(\infty) \\ \xi(t) - \xi(\infty) \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} u(t) - u(\infty) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \cancel{r(t) - r(\infty)}$$

at time $t \rightarrow \infty$ $r(t) = r(\infty) = r$
 $u(\infty) \rightarrow \text{Zero}$

$$\rightarrow \begin{bmatrix} \dot{\mathbf{x}}(t) - \dot{\mathbf{x}}(\infty) \\ \dot{\xi}(t) - \dot{\xi}(\infty) \end{bmatrix} = \begin{bmatrix} \mathbf{A} & \mathbf{0} \\ -\mathbf{C} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) - \mathbf{x}(\infty) \\ \xi(t) - \xi(\infty) \end{bmatrix} + \begin{bmatrix} \mathbf{B} \\ \mathbf{0} \end{bmatrix} [u(t) - u(\infty)] \quad 7$$

Define

 $P=1$

$$\mathbf{x}(t) - \mathbf{x}(\infty) = \mathbf{x}_e(t)$$

$$\xi(t) - \xi(\infty) = \xi_e(t)$$

$$u(t) - u(\infty) = u_e(t)$$

$$\rightarrow \begin{bmatrix} \dot{\mathbf{x}}_e(t) \\ \dot{\xi}_e(t) \end{bmatrix} = \begin{bmatrix} \mathbf{A} & \mathbf{0} \\ -\mathbf{C} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{x}_e(t) \\ \xi_e(t) \end{bmatrix} + \begin{bmatrix} \mathbf{B} \\ \mathbf{0} \end{bmatrix} u_e(t)$$

$e(t) = -(n+1) \times 1$

where $u_e(t) = -k x_e(t) + k_i \xi_e(t)$ — (9)

So will define a new $(n+P)$ th order of error vector

$$\mathbf{e}(t) = \begin{bmatrix} \mathbf{x}_e(t) \\ \xi_e(t) \end{bmatrix} = \begin{bmatrix} (n+P) \times 1 \end{bmatrix}$$

where:
 n # of states
 P # of outputs

$$\dot{\mathbf{e}}(t) = \underbrace{\begin{bmatrix} \mathbf{A} & \mathbf{0} \\ -\mathbf{C} & \mathbf{0} \end{bmatrix}}_{\hat{\mathbf{A}} \quad (n+1) \times (n+1)} \mathbf{e}(t) + \underbrace{\begin{bmatrix} \mathbf{B} \\ \mathbf{0} \end{bmatrix}}_{\hat{\mathbf{B}} \quad (n+1) \times 1} u_e(t) \quad (10)$$

when $P=1$ (output number)

$$u_e(t) = -k \underline{x}_e + \underline{\xi}_e k_i \quad (11)$$

$$u_e(t) = \begin{bmatrix} -k & k_i \end{bmatrix} \begin{bmatrix} x_e(t) \\ \xi_e(t) \end{bmatrix} \quad (11) \quad \mathbf{e}(t) = \begin{bmatrix} x_e(t) \\ \xi_e(t) \end{bmatrix}$$

$$e(t) = \begin{bmatrix} x_e(t) \\ \xi_e(t) \end{bmatrix}$$

$$u_e(t) = - \underbrace{[K \quad k_i]}_{\hat{K}} e(t) \quad (12)$$

$$u_e(t) = - \hat{K} e(t) \quad (13)$$

Sub Eq (13) into Eq. (10)

$$\dot{e}(t) = \begin{bmatrix} A & \vec{0} \\ -C & 0 \end{bmatrix} e(t) + \begin{bmatrix} B \\ 0 \end{bmatrix} \underline{u_e(t)} \quad (10)$$

$$\begin{aligned} \dot{e}(t) &= \hat{A} e(t) + \hat{B} u_e(t) \\ &= \hat{A} e(t) + \hat{B} (-\hat{K}) e(t) \end{aligned}$$

$$\dot{e}(t) = (\hat{A} - \hat{B} \hat{K}) e(t) \quad (14)$$

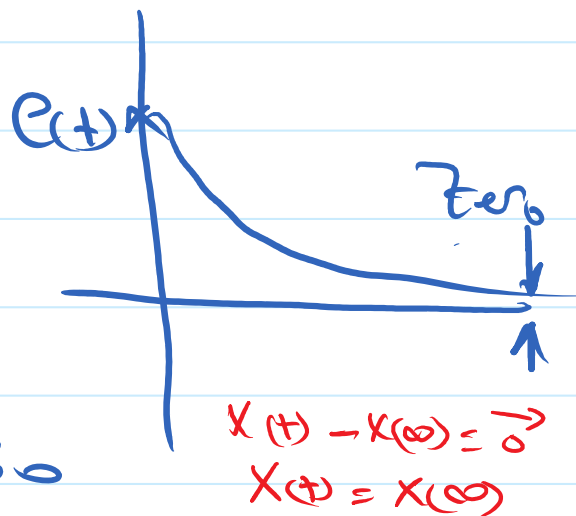
closed loop dynamics for Case 2 of tracking Sys

if the eigen values of $A_{cl} = \hat{A} - \hat{B} \hat{K}$ at left Side Plane. Then the Sys is Asy-stable. So the error goes to zero

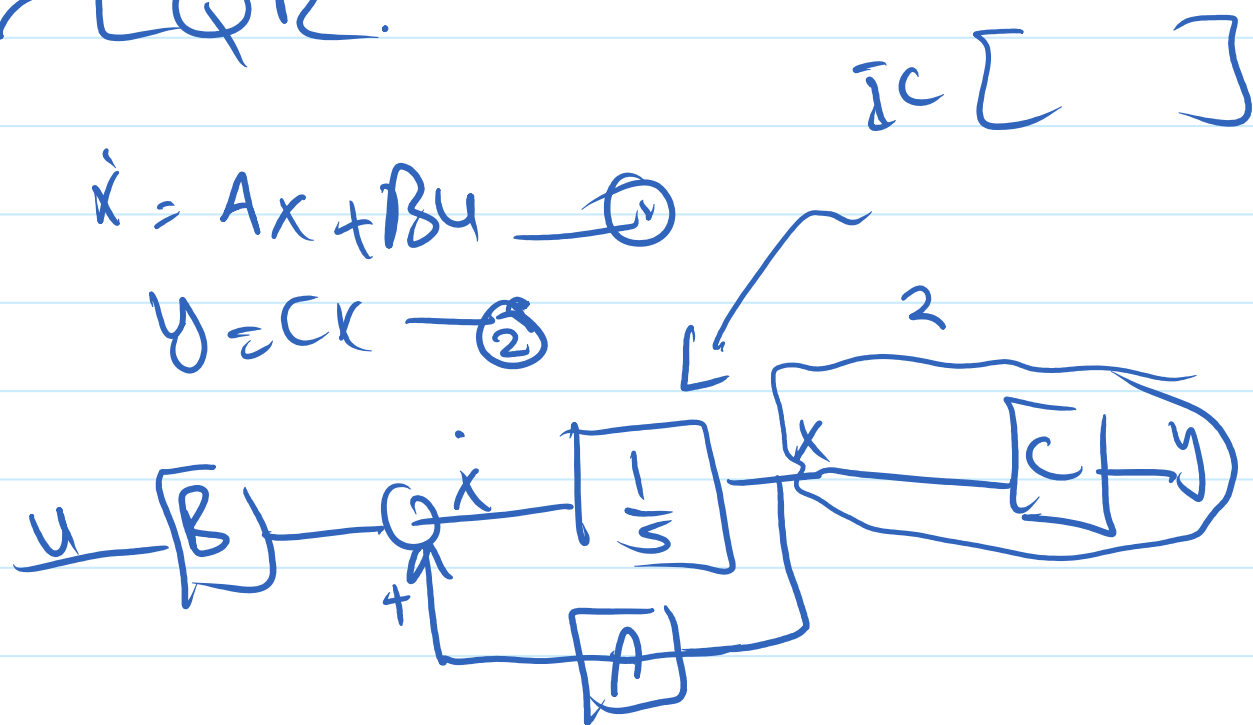
4 states

$$y_1 = x_1 = r(t)$$

$$e(t) = \begin{bmatrix} x_e(t) \\ \xi_e(t) \end{bmatrix} = \begin{bmatrix} x(t) - x(\infty) \\ \xi(t) - \xi(\infty) \end{bmatrix}$$



Now to design Asy. stable Sys. the eigenvalues of $\tilde{A} - \tilde{B}\tilde{K}$ must lie on the left side plane. You can do the previous step by pole placement or LQR.



Design Tracking Sys.

The required performance is $T_s = 1$ seconds and $\%OS = \%10$. Assume that the system configuration is the same as that shown in Figure below and the reference input r is a step function. Obtain the unit-step response of the designed system.

$$\dot{x} = \begin{bmatrix} 1 & 2 \\ 5 & 10 \end{bmatrix} x + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$y = [1 \ 0]$$

r : step input

$$\textcircled{1} |\lambda I - A| = \left| \begin{bmatrix} \lambda & 0 \\ 0 & \lambda \end{bmatrix} - \begin{bmatrix} 1 & 2 \\ 5 & 10 \end{bmatrix} \right| =$$

$$\textcircled{1} \begin{vmatrix} (\lambda - 1) & -2 \\ -5 & (\lambda - 10) \end{vmatrix} = (\lambda - 1)(\lambda - 10) - 10 = 0$$

$$\lambda^2 - 11\lambda + 10 - 10 = 0$$

$$\begin{aligned} a_1 = -11 \\ a_2 = 0 \end{aligned} \left\{ \begin{aligned} \lambda^2 - 11\lambda + 10 - 10 &= 0 \\ \lambda^2 - 11\lambda &= 0 \\ \lambda_1 = 0 & \quad \lambda_2 = 11 \end{aligned} \right. \Rightarrow \lambda(\lambda - 11) = 0$$

$$n = 1$$

$$\textcircled{2} M = [B \ AB] = \begin{bmatrix} 0 & 2 \\ 1 & 10 \end{bmatrix}$$

$$\det(M) = -2 \neq 0 \text{ Fully state Controllable}$$

$\textcircled{3}$ I will use Case 2 for Bass-Gura Approach because the sys is not in the form of the first canonical form

$$T = MW, \quad n=2 \quad W = \begin{bmatrix} a_1 & 1 \\ 1 & 0 \end{bmatrix} = \begin{bmatrix} -11 & 1 \\ 1 & 0 \end{bmatrix}$$

$$T = \begin{bmatrix} 0 & 2 \\ 1 & 10 \end{bmatrix} \begin{bmatrix} -11 & 1 \\ 1 & 0 \end{bmatrix}$$

$$= \begin{bmatrix} 2 & 0 \\ -1 & 1 \end{bmatrix}$$

$$T^{-1} = \begin{bmatrix} 0.5 & 0 \\ 0.5 & 1 \end{bmatrix}$$

④ $T_s = 1 \text{ sec}$ $\gamma_{OS} = \gamma_{10} = \xi = 0.59$ (under damped)

$$\omega_n = \frac{4}{T_s \xi} = \frac{4}{0.59 \times 1} = 6.78 \text{ rad/s}$$

$$M_{1,2} = -\xi \omega_n \pm \omega_n \sqrt{1 - \xi^2} j$$

$$M_{1,2} = -4 \pm 5.47 j \text{ (desired eigen values)}$$

$$(s - M_1)(s - M_2) = s^2 + 8s + 45.968$$

$$\alpha_1 = 8, \alpha_2 = 45.968$$

$$n=2$$

$$K = \begin{bmatrix} (\alpha_2 - a_2) & \vdots & (\alpha_1 - a_1) \end{bmatrix} T^{-1}$$

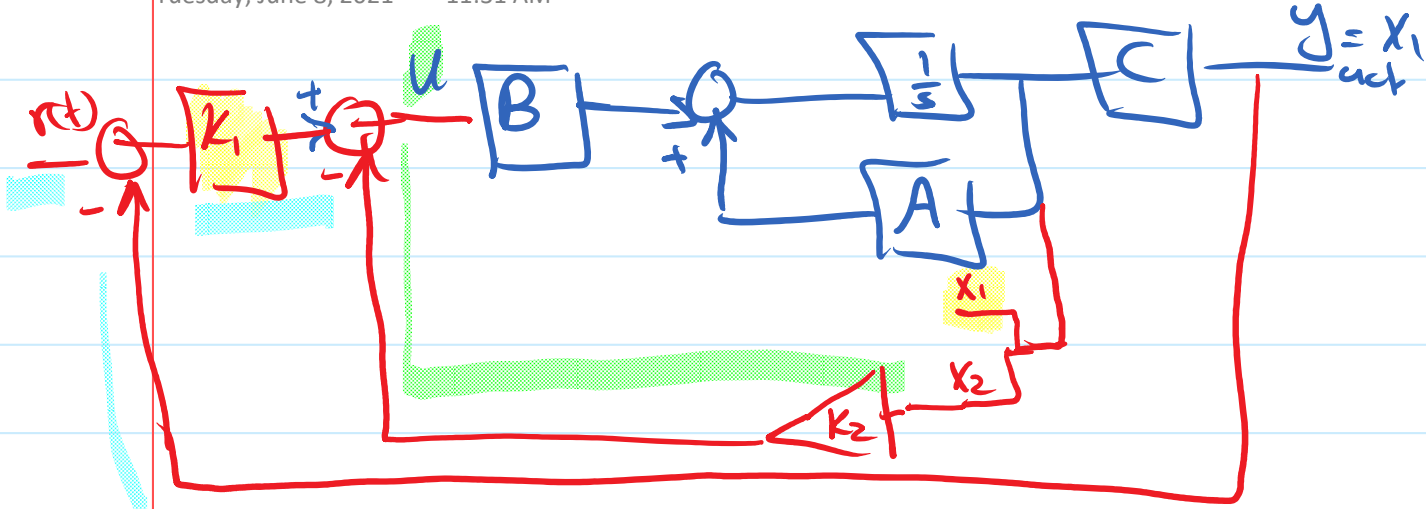
$$\begin{bmatrix} (45.968 - 0) & \vdots & (8 + 11) \end{bmatrix} \begin{bmatrix} 0.5 & 0 \\ 0.5 & 1 \end{bmatrix}$$

$$K = \begin{bmatrix} 32.48 & 19 \end{bmatrix}$$

$r = \text{step}$

$$y = x_1$$

$$y = CX + Du$$



$$u = -k_2 x_2 + k_1 (r - y) = -k_2 x_2 + k_1 r - k_1 x_1$$

$$= -\begin{bmatrix} k_1 & k_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + k_1 r$$

Example : Consider the system below:

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

Where:

$$A = \begin{bmatrix} 0 & 1 \\ 1 & 5 \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \quad C = [1 \quad 0]$$

- Study the stability for the system.
- Design a tracking system for the plant by using the pole-placement (**Bass-Gura Approach -second method**). The desired input for the control scheme is a step input and the controller must achieve the following requirements:
 - settling time (T_s) is one second.
 - critical damped (ζ).
 - the steady state error (ess) must be equal to zero.

Note: in the case you need to approximate the system to second order system use ($s_3 = -30$) if it is necessary.

$$\textcircled{1} |sI - A| = \begin{vmatrix} s & 0 \\ 0 & s \end{vmatrix} - \begin{vmatrix} 0 & 1 \\ 1 & 5 \end{vmatrix}$$

$$= \begin{vmatrix} s & -1 \\ -1 & s-5 \end{vmatrix} = s^2 - 5s - 1 = 0$$

internal stability

$s_1 = -0.19$
 $s_2 = 5.19$
 unstable

So we will use Case 2 for the tracking Sys.

$\text{type}/F = 0$

$$\hat{A} = \begin{bmatrix} A_{2 \times 2} & \vec{0} \\ -C & 0 \end{bmatrix}_{n+p \times n+p} = \begin{bmatrix} 0 & 1 & 0 \\ 1 & 5 & 0 \\ -1 & 0 & 0 \end{bmatrix}_{3 \times 3}$$

$$\hat{B} = \begin{bmatrix} 3 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}$$

$$(3) M = \begin{bmatrix} \hat{B} & \hat{A}\hat{B} & \hat{A}^2\hat{B} \end{bmatrix}$$

$$= \begin{bmatrix} 0 & 1 & 5 \\ 1 & 5 & 26 \\ 0 & 0 & -1 \end{bmatrix}, |M| = 1$$

fully state
Controllable.

$$\dot{\hat{x}} = \begin{bmatrix} 0 & 1 & 0 \\ 1 & 5 & 0 \\ -1 & 0 & 0 \end{bmatrix} \hat{x} + \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} \hat{u}$$

This Sys is not in the form of the first canonical form (Case 2 - Buss
gura-Approach)

$$|\lambda I - \hat{A}| = \begin{bmatrix} \lambda & 0 & 0 \\ 0 & \lambda & 0 \\ 0 & 0 & \lambda \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 1 & 5 & 0 \\ -1 & 0 & 0 \end{bmatrix}$$

$$s^3 - 5s^2 - s$$

$$a_1 = -5$$

$$a_2 = -1$$

$$a_3 = 0$$

$$T = M\omega, \quad \omega = \begin{bmatrix} a_2 & a_1 & 1 \\ a_1 & 1 & 0 \\ 1 & 0 & 0 \end{bmatrix} \quad n=3$$

$$\omega = \begin{bmatrix} -1 & -5 & 1 \\ -5 & 1 & 0 \\ 1 & 0 & 0 \end{bmatrix}$$

$$T = M\omega = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & 0 & 0 \end{bmatrix}$$

$$(4) T_s = 1 \text{ sec}$$

$$\zeta = 1 \quad \begin{array}{c} \times \\ -30 \\ \times \\ -4 \end{array} \quad \begin{array}{c} \times \\ -20 \\ \times \\ -4 \end{array}$$

$$\omega_n = \frac{4}{T_s \zeta} = 4 \text{ rad/s}$$

$$M_{1,2} = -\omega_n$$

$$M_{1,2} = -\omega_n \zeta \pm \omega_n \sqrt{1 - \zeta^2} j$$

$\zeta = 1$

$$M_{1,2} = -4$$

$$M_3 = -30$$

desired char. Eq.

$$(s - M_1)(s - M_2)(s - M_3)$$

$$(s + 4)(s + 4)(s + 30) =$$

desired
char.
Eq

$$= s^3 + 38.0s^2 + 256.0s + 480.0$$

$$= s^3 + \alpha_1 s^2 + \alpha_2 s + \alpha_3$$

$$\boxed{\alpha_1 = 38} \quad \boxed{\alpha_2 = 256} \quad \boxed{\alpha_3 = 480}$$

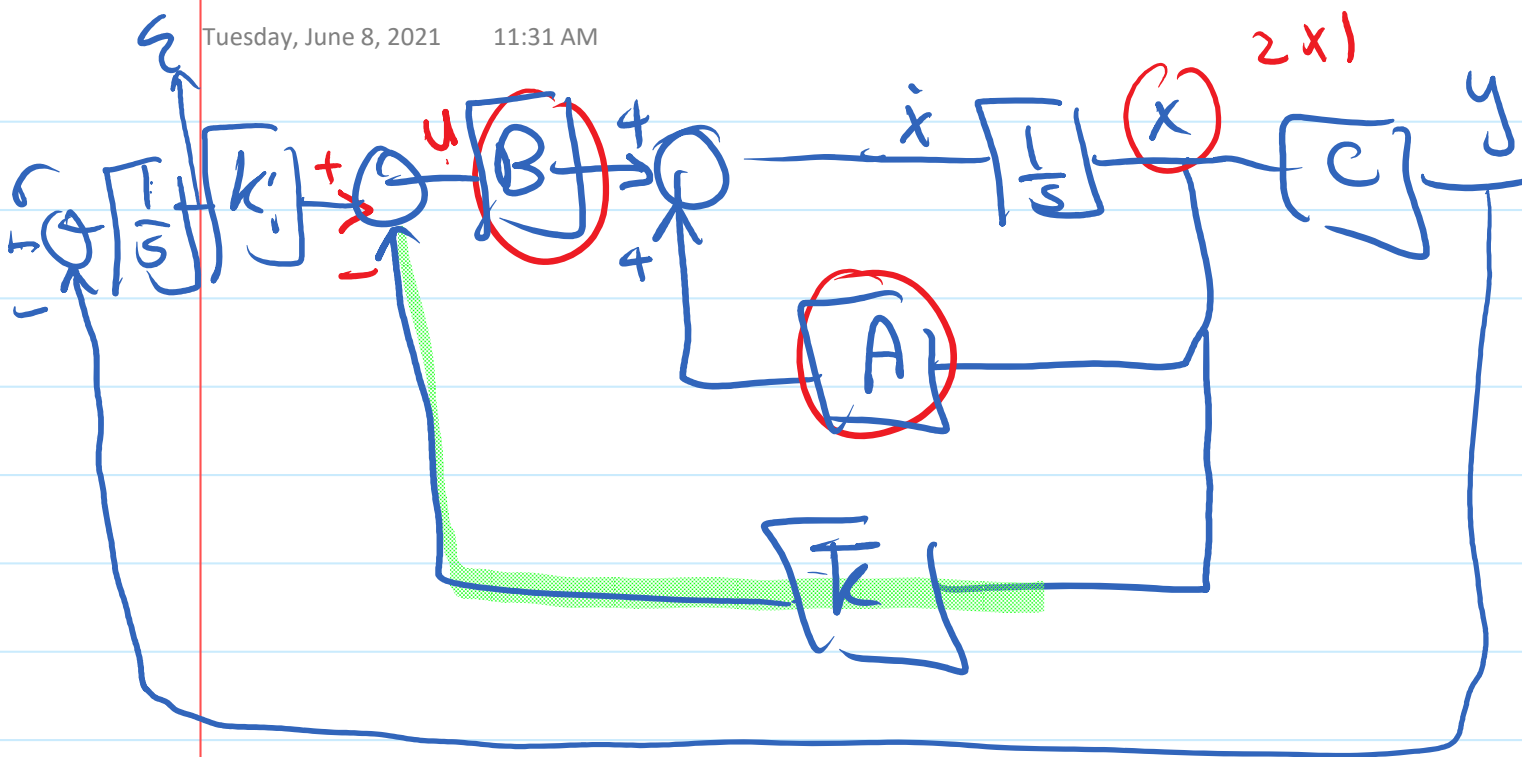
$$K = [(\alpha_n - a_n) \quad \dots \quad (\alpha_1 - a_1)] T^{-1}$$

$$[(\alpha_3 - a_3) \quad (\alpha_2 - a_2) \quad (\alpha_1 - a_1)] T^{-1}$$

$$[(480 - 0) \quad (256 - 1) \quad (38 - 5)] T^{-1}$$

$$= \begin{bmatrix} 257 & 43 & -480 \end{bmatrix}$$

$K_1 \quad K_2 \quad -K_i$



$$\bar{K} = [k_1 \quad k_2]$$

$$u = -\bar{K}x + k_i \xi$$

$$= -k_1 x_1 - k_2 x_2 + k_i \xi$$