## CHAPTER 17 EQUILIBRIUM: THE EXTENT OF CHEMICAL REACTIONS

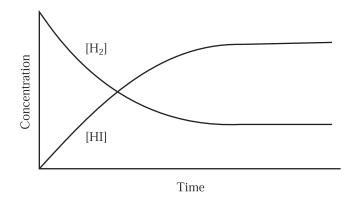
17.1 If the rate of the forward reaction exceeds the rate of reverse reaction, products are formed faster than they are consumed. The change in reaction conditions results in more products and less reactants. A change in reaction conditions can result from a change in concentration or a change in temperature. If concentration changes, product concentration increases while reactant concentration decreases, but the  $K_c$  remains unchanged because the *ratio* of products and reactants remains the same. If the increase in the forward rate is due to a change in temperature, the rate of the reverse reaction also increases. The equilibrium ratio of product concentration to reactant concentration is no longer the same. Since the rate of the forward reaction increases more than the rate of the reverse reaction,  $K_c$  increases (numerator, [products], is larger and denominator, [reactants], is smaller).

$$K_{\rm c} = \frac{[\text{products}]}{[\text{reactants}]}$$

- 17.2 The faster the rate and greater the yield, the more useful the reaction will be to the manufacturing process.
- 17.3 A system at equilibrium continues to be very dynamic at the molecular level. Reactant molecules continue to form products, but at the same rate that the products decompose to re-form the reactants.
- 17.4 If *K* is very large, the reaction goes nearly to completion. A large value of *K* means that the numerator is much larger than the denominator in the *K* expression. A large numerator, relative to the denominator, indicates that most of the reactants have reacted to become products. One cannot say with certainty whether the value of *K* for the phosphorus plus oxygen reaction is large or small (although it likely is large). However, it is certain that the reaction proceeds very fast.
- No, the value of Q is determined by the mass action expression with arbitrary concentrations for products and reactants. Thus, its value is not constant.
- 17.6 The equilibrium constant expression is  $K = [O_2]$ . If the temperature remains constant, K remains constant. If the initial amount of  $Li_2O_2$  present was sufficient to reach equilibrium, the amount of  $O_2$  obtained will be constant, regardless of how much  $Li_2O_2(s)$  is present.
- a) On the graph, the concentration of HI increases at twice the rate that H<sub>2</sub> decreases because the stoichiometric ratio in the balanced equation is 1 H<sub>2</sub>:2 HI.

Q for a reaction is the ratio of concentrations of products to concentrations of reactants. As the reaction progresses the concentration of reactants decrease and the concentration of products increase, which means that Q increases as a function of time.

$$H_2(g) + I_2(g) \leftrightarrows 2 \text{ HI}(g)$$
  $Q = \frac{\left[\text{HI}\right]^2}{\left[\text{H}_2\right]\left[\text{I}_2\right]}$ 



The value of Q increases as a function of time until it reaches the value of K.

b) No, Q would still increase with time because the  $[I_2]$  would decrease in exactly the same way as  $[H_2]$  decreases.

17.8 A homogeneous equilibrium reaction exists when **all** the components of the reaction are in the same phase (i.e., gas, liquid, solid, aqueous).

 $2 \text{ NO}(g) + O_2(g) \leftrightarrows 2 \text{ NO}_2(g)$ 

A heterogeneous equilibrium reaction exists when the components of the reaction are in different phases.

$$Ca(HCO_3)_2(aq) \leftrightarrows CaCO_3(s) + H_2O(l) + CO_2(g)$$

17.9  $1/2 N_2(g) + 1/2 O_2(g) \leftrightarrows NO(g)$ 

$$Q_{\text{c(form)}} = \frac{[\text{NO}]}{[\text{N}_2]^{\frac{1}{2}}[\text{O}_2]^{\frac{1}{2}}}$$

 $NO(g) \leftrightarrows 1/2 N_2(g) + 1/2 O_2(g)$ 

$$Q_{\text{c(decomp)}} = \frac{\left[N_2\right]^{\frac{1}{2}}\left[O_2\right]^{\frac{1}{2}}}{\left[\text{NO}\right]}$$

 $Q_{\text{c(decomp)}} = 1/Q_{\text{c(form)}}$ , so the constants do differ (they are the reciprocal of each other).

17.10 Yes, the Q values for the two reactions do differ. The balanced equation for the first reaction is

 $3/2 H_2(g) + 1/2 N_2(g) \leftrightarrows NH_3(g)$  (1)

The coefficient in front of  $NH_3$  is fixed at 1 mole according to the description. In the second reaction, the coefficient in front of  $N_2$  is fixed at 1 mole.

$$3 H_2(g) + N_2(g) \leftrightarrows 2 NH_3(g)$$
 (2)

The reaction quotients for the two equations and their relationship are:

$$Q_1 = \frac{\left[ \text{NH}_3 \right]}{\left[ \text{H}_2 \right]^{3/2} \left[ \text{N}_2 \right]^{1/2}}$$

$$Q_2 = \frac{\left[ \text{NH}_3 \right]^2}{\left[ \text{H}_2 \right]^3 \left[ \text{N}_2 \right]}$$

$$Q_2 = Q_1^2$$

17.11 Check that correct coefficients from balanced equation are included as exponents in the mass action expression. a)  $4 \text{ NO}(g) + \text{O}_2(g) \leftrightarrows 2 \text{ N}_2\text{O}_3(g)$ 

$$Q_{c} = \frac{\left[N_{2}O_{3}\right]^{2}}{\left[NO\right]^{4}\left[O_{2}\right]}$$

b)  $SF_6(g) + 2 SO_3(g) \leftrightarrows 3 SO_2F_2(g)$ 

$$Q_{c} = \frac{\left[SO_{2}F_{2}\right]^{3}}{\left[SF_{6} ISO_{3}\right]^{2}}$$

c) 2 SCIF<sub>5</sub>(g) + H<sub>2</sub>(g) 
$$\leftrightarrows$$
 S<sub>2</sub>F<sub>10</sub>(g) + 2 HCl(g)
$$Q_{c} = \frac{\left[S_{2}F_{10}\right]\left[HCl\right]^{2}}{\left[SCIF_{5}\right]^{2}\left[H_{2}\right]}$$

17.12 a) 
$$2 C_2H_6(g) + 7 O_2(g) \leftrightarrows 4 CO_2(g) + 6 H_2O(g)$$

$$Q_c = \frac{[CO_2]^4 [H_2O]^6}{[C_2H_6]^2 [O_2]^7}$$
b)  $CH_4(g) + 4 F_2(g) \leftrightarrows CF_4(g) + 4 HF(g)$ 

$$Q_c = \frac{[CF_4][HF]^4}{[CH_4][F_2]^4}$$
c)  $2 SO_3(g) \leftrightarrows 2 SO_2(g) + O_2(g)$ 

$$Q_c = \frac{[SO_2]^2 [O_2]}{[SO_3]^2}$$

17.13 The Q for the original reaction is 
$$Q_{\text{ref}} = \frac{\left[H_2\right]^2 \left[S_2\right]}{\left[H_2S\right]^2}$$

a) The given reaction 1/2  $S_2(g) + H_2(g) \leftrightarrows H_2S(g)$  is the reverse reaction of the original reaction multiplied by a factor of 1/2. The equilibrium constant for the reverse reaction is the inverse of the original constant. When a reaction is multiplied by a factor, K for the new equation is equal to the K of the original equilibrium raised to a power equal to the factor. For the reaction given in part a), take  $(1/K)^{1/2}$ .

$$Q_{\rm a} = (1/Q_{\rm ref})^{1/2} = \frac{\left[{\rm H_2S}\right]}{\left[{\rm S_2}\right]^{1/2} \left[{\rm H_2}\right]}$$
$$K = (1/1.6 \times 10^{-2})^{1/2} = 7.90569 = 7.9$$

b) The given reaction  $5 \text{ H}_2\text{S}(g) \leftrightarrows 5 \text{ H}_2(g) + 5/2 \text{ S}_2(g)$  is the original reaction multiplied by 5/2. Take the original K to the 5/2 power to find K of given reaction.

$$Q_{\rm a} = (Q_{\rm ref})^{5/2} = \frac{\left[{\rm H}_2\right]^5 \left[{\rm S}_2\right]^{5/2}}{\left[{\rm H}_2{\rm S}\right]^5}$$

$$K = (1.6 \times 10^{-2})^{5/2} = 3.23817 \times 10^{-5} = 3.2 \times 10^{-5}$$

17.14 
$$Q_{c(ref)} = \frac{\left[N_{2}\right]\left[H_{2}O\right]^{2}}{\left[NO\right]^{2}\left[H_{2}\right]^{2}}$$
a)  $Q_{c} = \left[Q_{c(ref)}\right]^{1/2} = \frac{\left[N_{2}\right]^{\frac{1}{2}}\left[H_{2}O\right]}{\left[NO\right]\left[H_{2}\right]}$ 
Thus,  $K_{c} = \left[K_{c(ref)}\right]^{1/2} = (6.5 \times 10^{2})^{1/2} = 25.495 = 25$ 
b)  $Q_{c} = \left[Q_{c(ref)}\right]^{-2} = \frac{\left[NO\right]^{4}\left[H_{2}\right]^{4}}{\left[N_{2}\right]^{2}\left[H_{2}O\right]^{4}}$ 

$$K_{c} = \left[K_{c(ref)}\right]^{-2} = (6.5 \times 10^{2})^{-2} = 2.36686 \times 10^{-6} = 2.4 \times 10^{-6}$$

- 17.15 The concentration of solids and pure liquids do not change, so their concentration terms are not written in the reaction quotient expression.
  - a)  $2 \text{ Na}_2\text{O}_2(s) + 2 \text{ CO}_2(g) \leftrightarrows 2 \text{ Na}_2\text{CO}_3(s) + \text{O}_2(g)$

$$Q_{c} = \frac{\left[O_{2}\right]}{\left[CO_{2}\right]^{2}}$$

- b)  $H_2O(l) \leftrightarrows H_2O(g)$ 
  - $Q_c = [H_2O(g)]$ Only the gaseous water is used. The "(g)" is for emphasis.
- c)  $NH_4Cl(s) \leftrightarrows NH_3(g) + HCl(g)$

$$Q_c = [NH_3][HC1]$$

17.16 a)  $H_2O(l) + SO_3(g) \leftrightarrows H_2SO_4(aq)$ 

$$Q_{c} = \frac{\left[H_{2}SO_{4}\right]}{\left[SO_{3}\right]}$$

b) 2 KNO<sub>3</sub>(s)  $\leftrightarrows$  2 KNO<sub>2</sub>(s) + O<sub>2</sub>(g)

$$Q_{\rm c} = [{\rm O}_2]$$

 $Q_c = [O_2]$ c)  $S_8(s) + 24 F_2(g) \leftrightarrows 8 SF_6(g)$ 

$$Q_{c} = \frac{\left[SF_{6}\right]^{8}}{\left[F_{2}\right]^{24}}$$

- Write balanced chemical equations for each reaction, and then write the appropriate equilibrium expression. 17.17
  - a)  $4 \operatorname{HCl}(g) + O_2(g) \leftrightarrows 2 \operatorname{Cl}_2(g) + 2 \operatorname{H}_2O(g)$

$$Q_{c} = \frac{\left[\text{Cl}_{2}\right]^{2} \left[\text{H}_{2}\text{O}\right]^{2}}{\left[\text{HCl}\right]^{4} \left[\text{O}_{2}\right]}$$

b)  $2 \text{ As}_2\text{O}_3(s) + 10 \text{ F}_2(g) \leftrightarrows 4 \text{ As}_{5}(l) + 3 \text{ O}_2(g)$ 

$$Q_{c} = \frac{\left[O_{2}\right]^{3}}{\left[F_{2}\right]^{10}}$$

c)  $SF_4(g) + 2 H_2O(l) \leftrightarrows SO_2(g) + 4 HF(g)$ 

$$Q_{c} = \frac{\left[SO_{2}\right]\left[HF\right]^{4}}{\left[SF_{4}\right]}$$

d)  $2 \text{ MoO}_3(s) + 6 \text{ XeF}_2(g) \leftrightarrows 2 \text{ MoF}_6(l) + 2 \text{ Xe}(g) + 3 \text{ O}_2(g)$ 

$$Q_{c} = \frac{\left[\text{Xe}\right]^{6} \left[\text{O}_{2}\right]^{3}}{\left[\text{XeF}_{2}\right]^{6}}$$

17.18 a) The balanced equations and corresponding reaction quotients are given below. Note the second equation must occur twice to get the appropriate overall equation.

$$(1) \operatorname{Cl}_{2}(g) + \operatorname{F}_{2}(g) \leftrightarrows 2 \operatorname{ClF}(g)$$

$$Q_{1} = \frac{\left[\operatorname{ClF}\right]^{2}}{\left[\operatorname{Cl}_{2}\right]\left[\operatorname{F}_{2}\right]}$$

$$(2) \operatorname{ClF}(g) + \operatorname{F}_{2}(g) \leftrightarrows \operatorname{ClF}_{3}(g)$$

$$Q_{2} = \frac{\left[\operatorname{ClF}_{3}\right]}{\left[\operatorname{ClF}\right]\left[\operatorname{F}_{2}\right]}$$

$$((3) \operatorname{ClF}(g) + \operatorname{F}_{2}(g) \leftrightarrows \operatorname{ClF}_{3}(g)$$

$$Q_{2} = \frac{\left[\operatorname{ClF}_{3}\right]}{\left[\operatorname{ClF}\right]\left[\operatorname{F}_{2}\right]}$$

$$Q_{1} = \frac{\left[\operatorname{ClF}_{3}\right]}{\left[\operatorname{ClF}\right]\left[\operatorname{F}_{2}\right]}$$

$$Q_{2} = \frac{\left[\operatorname{ClF}_{3}\right]}{\left[\operatorname{ClF}\right]\left[\operatorname{F}_{2}\right]}$$

$$Q_{2} = \frac{\left[\operatorname{ClF}_{3}\right]^{2}}{\left[\operatorname{ClF}\right]\left[\operatorname{F}_{2}\right]}$$

- Overall:  $\operatorname{Cl}_2(g) + 3 \operatorname{F}_2(g) \leftrightarrows 2 \operatorname{ClF}_3(g)$   $Q_{\operatorname{overall}} = \frac{\left[\operatorname{ClF}_3\right]^2}{\left[\operatorname{Cl}_2\right]\left[\operatorname{F}_2\right]^3}$
- b) The second equation occurs twice, thus it could simply be multiplied by two and its reaction quotient squared. The reaction quotient for the overall reaction,  $Q_{\text{overall}}$ , determined from the reaction is:

$$Q_{\text{overall}} = \frac{\left[\text{ClF}_{3}\right]^{2}}{\left[\text{Cl}_{2}\right]\left[\text{F}_{2}\right]^{3}}$$

$$Q_{\text{overall}} = Q_{1}Q_{2}^{2} = Q_{1}Q_{2}Q_{2} = \frac{\left[\text{ClF}\right]^{2}}{\left[\text{Cl}_{3}\right]\left[\text{F}_{2}\right]} \times \frac{\left[\text{ClF}_{3}\right]}{\left[\text{ClF}\right]\left[\text{F}_{2}\right]} \times \frac{\left[\text{ClF}_{3}\right]}{\left[\text{ClF}\right]\left[\text{F}_{2}\right]} = \frac{\left[\text{ClF}_{3}\right]^{2}}{\left[\text{Cl}_{3}\right]\left[\text{F}_{2}\right]^{3}}$$

- 17.19 According to the Ideal Gas Equation, PV = nRT. Concentration and pressure of gas are directly proportional as long as the temperature is constant: C = n/V = P/RT.
- 17.20  $K_c$  and  $K_p$  are related by the equation  $K_p = K_c(RT)^{\Delta n}$ , where  $\Delta n$  represents the change in the number of moles of gas in the reaction (moles gaseous products moles gaseous reactants). When  $\Delta n$  is zero (no change in number of moles of gas), the term  $(RT)^{\Delta n}$  equals 1 and  $K_c = K_p$ . When  $\Delta n$  is not zero, meaning that there is a change in the number of moles of gas in the reaction, then  $K_c \neq K_p$ .
- a) K<sub>p</sub> = K<sub>c</sub>(RT)<sup>Δn</sup>. Since Δn = number of moles gaseous products number of moles gaseous reactants, Δn is a positive integer. If Δn is a positive integer, then (RT)<sup>Δn</sup> is greater than 1. Thus, K<sub>c</sub> is multiplied by a number that is greater than 1 to give K<sub>p</sub>. K<sub>c</sub> is smaller than K<sub>p</sub>.
  b) Assuming that RT > 1 (which occurs when T > 12.2 K, because 0.0821 (R) x 12.2 = 1), K<sub>p</sub> > K<sub>c</sub> if the number of moles of gaseous products exceeds the number of moles of gaseous reactants. K<sub>p</sub> < K<sub>c</sub> when the number of moles of gaseous reactants exceeds the number of moles of gaseous product.
- 17.22 a) Number of moles of gaseous reactants = 0; Number of moles of gaseous products = 3;  $\Delta n = 3 0 = 3$  b) Number of moles of gaseous reactants = 1; Number of moles of gaseous products = 0;  $\Delta n = 0 1 = -1$ 
  - c) Number of moles of gaseous reactants = 0; Number of moles of gaseous products = 3;  $\Delta n = 3 0 = 3$
- 17.23 a)  $\Delta n_{gas} = 1$  b)  $\Delta n_{gas} = -3$  c)  $\Delta n_{gas} = 1$
- 17.24 First, determine  $\Delta n$  for the reaction and then calculate  $K_c$  using  $K_p = K_c(RT)^{\Delta n}$ .
  - a)  $\Delta n = \text{Number of product gas moles} \text{Number of reactant gas moles} = 1 2 = -1$

$$K_{\rm c} = \frac{K_{\rm p}}{({\rm RT})^{\Delta n}} = \frac{3.9 \times 10^{-2}}{[(0.0821)(1000.)]^{-1}} = 3.2019 = 3.2$$

b)  $\Delta n =$  Number of product gas moles – Number of reactant gas moles = 1 – 1 = 0

$$K_{\rm c} = \frac{K_{\rm p}}{({\rm RT})^{\Delta n}} = \frac{28.5}{[(0.0821)(500.)]^0} = 28.5$$

First, determine  $\Delta n$  for the reaction and then calculate  $K_c$  using  $K_p = K_c(RT)^{\Delta n}$ .

a)  $\Delta n = \text{Number of product gas moles} - \text{Number of reactant gas moles} = 2 - 2 = 0$ 

$$K_{\rm c} = K_{\rm p} / ({\rm RT})^{\Delta n} = (49)/[(0.0821) (730.)]^0 = 49$$

- b)  $\Delta n = \text{Number of product gas moles} \text{Number of reactant gas moles} = 2 3 = -1$  $K_c = K_p / (\text{RT})^{\Delta n} = (2.5 \text{ x } 10^{10})/[(0.0821) (500.)]^{-1} = 1.02625 \text{ x } 10^{12} = \textbf{1.0 x } \textbf{10}^{12}$
- 17.26 When Q < K, the reaction proceeds to the **right** to form more products. The reaction quotient and equilibrium constant are determined by [products]/[reactants]. For Q to increase and reach the value of K, the concentration of products (numerator) must increase in relation to the concentration of reactants (denominator).
- 17.27 a) The reaction is  $2D \leftrightarrow E$  and  $K_c = \frac{[E]}{[D]^2}$

Concentration of D = Concentration of E = 
$$(3 \text{ spheres}) \left( \frac{0.0100 \text{ mol}}{1 \text{ sphere}} \right) \left( \frac{1}{1.00 \text{ L}} \right) = 0.0300 \text{ M}$$

$$K_c = \frac{[E]}{[D]^2} = \frac{[0.0300]}{[0.0300]^2} = 33.3333 = 33.3$$

b) In Scene B the concentrations of D and E are both 0.0300 mol/0.500 L = 0.0600 M

$$Q_c = \frac{[E]}{[D]^2} = \frac{[0.0600]}{[0.0600]^2} = 16.66666 = 16.7$$

B is **not at equilibrium**. Since  $Q_c \le K_c$ , the reaction will proceed to the **right**.

In Scene C, the concentration of D is still 0.0600 M and the concentration of E is 0.0600 mol/0.500 L = 0.120 M

$$Q_c = \frac{[E]}{[D]^2} = \frac{[0.0600]}{[0.120]^2} = 4.16667 = 4.17$$

C is **not at equilibrium**. Since  $Q_c \le K_c$ , the reaction will proceed to the **right**.

17.28 To decide if the reaction is at equilibrium, calculate  $Q_p$  and compare it to  $K_p$ . If  $Q_p = K_p$ , then the reaction is at equilibrium. If  $Q_p > K_p$ , then the reaction proceeds to the left to produce more reactants. If  $Q_p < K_p$ , then the reaction proceeds to the right to produce more products.

$$Q_{\rm p} = \frac{{\rm P}_{\rm H_2} {\rm P}_{\rm Br_2}}{{\rm P}_{\rm HBr}^2} = \frac{(0.010)(0.010)}{(0.20)^2} = 2.5 \times 10^{-3} > K_{\rm p} = 4.18 \times 10^{-9}$$

 $Q_p > K_p$ , thus, the reaction is **not** at equilibrium and will proceed to the **left** (toward the reactants). Thus, the numerator will decrease in size as products are consumed and the denominator will increase in size as more reactant is produced.  $Q_p$  will decrease until  $Q_p = K_p$ .

17.29 
$$Q_{\rm p} = \frac{P_{\rm NO}^2 P_{\rm Br_2}}{P_{\rm NOR}^2} = \frac{(0.10)^2 (0.10)}{(0.10)^2} = 0.10 < K_{\rm p} = 60.6$$

 $Q_p \le K_p$  Thus, the reaction is **not** at equilibrium and will proceed to the **right** (toward the products).

17.30 There is insufficient information to calculate the partial pressures of each gas (T is not given). There is sufficient information to determine the concentrations and hence  $Q_c$ . Convert the  $K_p$  given to  $K_c$  using  $K_p = K_c (RT)^{\Delta n}$ . Compare the  $Q_c$  to the  $K_c$  just calculated and make a prediction.

 $\Delta n$  = Number of product gas moles – Number of reactant gas moles = 2 – 2 = 0

Since  $\Delta n = 0$ ,  $K_p = K_c = 2.7$  (note if  $\Delta n$  had any other value, we could not finish the calculation without the temperature).

$$Q_{c} = \frac{[\text{CO}_{2}][\text{H}_{2}]}{[\text{CO}][\text{H}_{2}\text{O}]} = \frac{[0.62/2.0][0.43/2.0]}{[0.13/2.0][0.56/2.0]} = 3.662 \text{ (unrounded)} > K_{c} = 2.7$$

 $Q_c > K_c$  Thus, the reaction is **not** at equilibrium and will proceed to the **left** (towards the reactants).

- 17.31 When x mol of CH<sub>4</sub> reacts, 2x mol of H<sub>2</sub>O also reacts to form x mol of CO<sub>2</sub> and 4x mol of H<sub>2</sub>. The final (equilibrium) concentration of each reactant is the initial concentration minus the amount that reacts. The final (equilibrium) concentration of each product is the initial concentration plus the amount that forms.
- 17.32 a) The approximation applies when the change in concentration from initial to equilibrium is so small that it is insignificant. This occurs when K is small and initial concentration is large. b) This approximation will not work when the change in concentration is greater than 5%. This can occur when [reactant] $_{initial}$  is very small, or when [reactant] $_{change}$  is relatively large due to a large K.
- Since all equilibrium concentrations are given in molarities and the reaction is balanced, construct an equilibrium 17.33 expression and substitute the equilibrium concentrations to find  $K_c$ .

$$K_{\rm c} = \frac{\left[{\rm HI}\right]^2}{\left[{\rm H}_2\right]\left[{\rm I}_2\right]} = \frac{\left[1.87 \text{ x} 10^{-3}\right]^2}{\left[6.50 \text{ x} 10^{-5}\right]\left[1.06 \text{ x} 10^{-3}\right]} = 50.753 =$$
**50.8**

17.34 
$$K_{c} = \frac{\left[N_{2}\right]\left[H_{2}\right]^{3}}{\left[NH_{3}\right]^{2}} = \frac{\left[0.114\right]\left[0.342\right]^{3}}{\left[0.0225\right]^{2}} = 9.0077875 = 9.01$$

The reaction table requires that the initial [PCl<sub>5</sub>] be calculated: [PCl<sub>5</sub>] = 0.15 mol/2.0 L = 0.075 M 17.35 Since there is a 1:1:1 mole ratio in this reaction:

 $x = [PCl_5]$  reacting (-x), and the amount of PCl<sub>3</sub> and of Cl<sub>2</sub> forming (+x).

Concentration $(M)$	$PCl_5(g)$	≒	$PCl_3(g)$	-	+	$\operatorname{Cl}_2(g)$
Initial	0.075		0			0
Change	-x		$+_{\rm X}$			$+_{\mathbf{X}}$
Equilibrium	0.075 - x		X			X

17.36 The reaction table requires that the initial  $[H_2]$  and  $[F_2]$  be calculated:  $[H_2] = 0.10 \text{ mol}/0.50 \text{ L} = 0.20 \text{ M}$ ;  $[F_2] = 0.050 \text{ mol}/0.50 \text{ L} = 0.10 M$ 

$$x = [H_2] = [F_2]$$
 reacting  $(-x)$ ;  $2x = [HF]$  forming  $(+2x)$   
Concentration  $(M)$   $H_2(g)$  +  $F_2(g)$   $\leftrightarrows$  2HF

Concentration (*M*) 
$$H_2(g) + F_2(g) \leftrightarrows 2HF($$
  
Initial 0.20 0.10 0  
Change  $-x -x +2x$   
Equilibrium 0.20  $-x 0.10 -x 2x$ 

Two of the three equilibrium pressures are known. Construct an equilibrium expression and solve for  $P_{\text{NOCI}}$ . 17.37

$$K_{\rm p} = 6.5 \text{ x } 10^4 = \frac{P_{\rm NOCl}^2}{P_{\rm NO}^2 P_{\rm Cl_2}}$$

$$6.5 \times 10^4 = \frac{P_{\text{NOCI}}^2}{(0.35)^2 (0.10)}$$

$$P_{\text{NOCl}} = \sqrt{\left(6.5 \times 10^4\right) \left(0.35\right)^2 \left(0.10\right)} = 28.2179 = 28 \text{ atm}$$

A high pressure for NOCl is expected because the large value of  $K_p$  indicates that the reaction proceeds largely to the right, i.e., to the formation of products.

17.38 
$$C(s) + 2 H_2(g) \leftrightarrows CH_4(g)$$

$$K_{\rm p} = \frac{P_{\rm CH_4}}{P_{\rm H_2}^2} = 0.262$$

$$P_{\text{CH}_4} = K_{\text{p}} P_{\text{H}_2}^2 = (0.262) (1.22)^2 = 0.38996 =$$
**0.390 atm**

17.39 The ammonium hydrogen sulfide will decompose to produce hydrogen sulfide and ammonia gas until  $K_p = 0.11$ : NH<sub>4</sub>HS(s)  $\rightleftharpoons$  H<sub>2</sub>S(g) + NH<sub>3</sub>(g)

 $x = [NH_4HS]$  reacting (-x), and the amount of  $H_2S$  and of  $NH_3$  forming (+x) since there is a 1:1:1 mole ratio between the reactant and products.

(It is not necessary to calculate the molarity of NH<sub>4</sub>HS since, as a solid, it is not included in the equilibrium expression.)

Concentration (M) 
$$NH_4HS(s)$$
  $\Rightarrow$   $H_2S(g)$  +  $NH_3(g)$  Initial  $-$  0 0  $Change$   $-x$   $+x$   $+x$  Equilibrium  $x$   $x$ 

$$K_{\rm p} = 0.11 = (P_{\rm H_2S})(P_{\rm NH_3})$$
 (The solid NH<sub>4</sub>HS is not included.)  
 $0.11 = (x)(x)$   
 $x = P_{\rm NH_3} = 0.33166 =$ **0.33 atm**

17.40  $2 H_2S(g) = 2 H_2(g) + S_2(g)$ 

$$[H_2S] = 0.45 \text{ mol} / 3.0 \text{ L} = 0.15 M$$

$$K_{c} = 9.30 \times 10^{-8} = \frac{\left[H_{2}\right]^{2} \left[S_{2}\right]}{\left[H_{2}S\right]^{2}} = \frac{\left[2x\right]^{2} \left[x\right]}{\left[0.15 - 2x\right]^{2}}$$

Assuming  $0.15 M - 2 x \approx 0.15 M$ 

9.30 x 10<sup>-8</sup> = 
$$\frac{[2x]^2[x]}{[0.15]^2}$$
 =  $\frac{4x^3}{0.15^2}$ 

 $x = 8.0575 \times 10^{-4} M$  (unrounded)

$$[H_2] = 2 x = 2 (8.0575 \times 10^{-4} M) = 1.6115 \times 10^{-3} = 1.6 \times 10^{-3} M$$

(Since  $(1.6 \times 10^{-3})/(0.15) < 0.05$ , the assumption is OK.)

17.41 The initial concentrations of  $N_2$  and  $O_2$  are (0.20 mol/1.0 L) = 0.20 M and (0.15 mol/1.0 L) = 0.15 M, respectively.

 $N_2(g) + O_2(g) \leftrightarrows 2 \text{ NO}(g)$  There is a 1:1:2 mole ratio between reactants and products. Concentration (M)  $N_2(g)$   $O_2(g) \leftrightarrows 2 \text{ NO}(g)$  Initial 0.20 0.15 0 Change -x -x +2x (1:1:2 mole ratio) Equilibrium 0.20-x 0.15-x 2x

$$K_{\rm c} = 4.10 \text{ x } 10^{-4} = \frac{\left[\text{NO}\right]^2}{\left[\text{N}_2\right]\left[\text{O}_2\right]} = \frac{\left[2x\right]^2}{\left[0.20 - x\right]\left[0.15 - x\right]}$$

Assume  $0.20 M - x \approx 0.20 M$  and  $0.15 M - x \approx 0.15 M$ 

$$4.10 \times 10^{-4} = \frac{4x^2}{[0.20][0.15]}$$

 $x = 1.753568 \times 10^{-3} M$  (unrounded)

[NO] =  $2x = 2 (1.753568 \times 10^{-3} M) = 3.507136 \times 10^{-3} = 3.5 \times 10^{-3} M$ 

(Since  $(1.8 \times 10^{-3})/(0.15) < 0.05$ , the assumption is OK.)

17.42 
$$2 \text{ NO}_2(g) \leftrightarrows 2 \text{ NO}(g) + \text{O}_2(g)$$

Pressure (atm) 
$$2 \text{ NO}_2(g) \Rightarrow 2 \text{ NO}(g) \text{ O}_2(g)$$
Initial  $0.75 \Rightarrow 0 \Rightarrow 0$ 
Change  $-2x \Rightarrow +2x \Rightarrow +x$ 
Equilibrium  $0.75-2x \Rightarrow 2x \Rightarrow x$ 

$$K_{\rm p} = 4.48 \times 10^{-13} = \frac{P_{\rm NO}^2 P_{\rm O_2}}{P_{\rm NO_2}^2} = \frac{\left(2x\right)^2 \left(x\right)}{\left(0.75 - 2x\right)^2}$$

Assume  $0.75 \text{ atm} - 2x \approx 0.75 \text{ atm}$ 

$$4.48 \times 10^{-13} = \frac{\left(4x^2\right)(x)}{\left(0.75\right)^2} = \frac{\left(4x^3\right)}{\left(0.75\right)^2}$$

$$x = 3.979 \text{ x } 10^{-5} \text{ atm} = 4.0 \text{ x } 10^{-5} \text{ atm } O_2$$

$$x = 3.979 \text{ x } 10^{-5} \text{ atm} = 4.0 \text{ x } 10^{-5} \text{ atm } O_2$$
  
 $P_{\text{NO}} = 2x = 2(3.979 \text{ x } 10^{-5} \text{ atm}) = 7.958 \text{ x } 10^{-5} = 8.0 \text{ x } 10^{-5} \text{ atm NO}$ 

17.43 Construct a reaction table, using [ICl]<sub>init</sub> = (0.500 mol/ 5.00 L) = 0.100 M, and substitute the equilibrium concentrations into the equilibrium expression. There is a 2:1:1 mole ratio between reactant and products:

Concentration (M) 2 ICl(g) 
$$\Rightarrow$$
 I<sub>2</sub>(g) + Cl<sub>2</sub>(g)  
Initial 0.100 0 0  
Change  $-2x$   $+x$   $+x$  (2:1:1 mole ratio)  
Equilibrium  $0.100-2x$   $x$ 

$$K_{\rm c} = 0.110 = \frac{[I_2][CI_2]}{[ICI]^2} = \frac{[x][x]}{[0.100 - 2x]^2}$$

$$0.110 = \frac{\left[x\right]^2}{\left[0.100 - 2x\right]^2}$$

Take the square root of each side:

$$0.331662 = \frac{[x]}{[0.100 - 2x]}$$

$$x = 0.0331662 - 0.663324x$$

$$1.663324x = 0.0331662$$

$$x = 0.0199397$$

$$[I_2]_{eq} = [Cl_2]_{eq} = 0.0200 M$$

$$[ICI]_{eq} = 0.100 - 2x = 0.601206 = 0.060 M ICI$$

17.44 Concentration (M)  $S(CH_2CH_2Cl)_2(g)$ Initial

Change 
$$-x$$
  $-2x$   $+x$  Equilibrium  $0.675 - x$   $0.973 - 2x$ 

$$[S(CH_2CH_2CI)_2]_{eq} = x = 0.350 M$$

$$[SCl_2]_{eq} = 0.675 - x = 0.675 - 0.350 = 0.325 M$$

$$[C_2H_4]_{eq} = 0.973 - 2x = 0.973 - 2(0.350) = 0.273 M$$

$$[SCl_{2}]_{eq} = 0.675 - x = 0.675 - 0.350 M$$

$$[C_{2}H_{4}]_{eq} = 0.973 - 2x = 0.973 - 2(0.350) = 0.273 M$$

$$K_{c} = \frac{[S(CH_{2}CH_{2}Cl)_{2}]}{[SCl_{2}][C_{2}H_{4}]^{2}} = \frac{[0.350]}{[0.325][0.273]^{2}} = 14.4497 \text{ (unrounded)}$$

$$K_p = K_c (RT)^{\Delta n}$$
  $\Delta n = 1 \text{ mol} - 3 \text{ mol} = -2$ 

$$K_p = (14.4497) \lceil (0.0821) (273.2 + 20.0) \rceil^{-2} = 0.0249370 = \mathbf{0.0249}$$

17.45  $4 \text{ NH}_3(g) + 3 \text{ O}_2(g) \leftrightarrows 2 \text{ N}_2(g) + 6 \text{ H}_2\text{O}(g)$ 

> To find the equilibrium constant, determine the equilibrium concentrations of each reactant and product and insert into the equilibrium expression. Since  $[N_2]$  increases from 0 to 1.96 x  $10^{-3}$  M, the concentration of  $H_2O$  gas will increase by 3 times as much (stoichiometric ratio is 6 H<sub>2</sub>O: 2 N<sub>2</sub>) and the concentration of reactants will decrease by a factor equivalent to the stoichiometric ratio (2 for NH<sub>3</sub> and 3/2 for O<sub>2</sub>). Since the volume is 1.00 L, the concentrations are equal to the number of moles present

concentrations are equal to the number of moles present.							
Concentration (M)	$4 \text{ NH}_3(g)$	+	$3 O_2(g)$	≒	$2 N_2(g)$	+	$6 H_2O(g)$
Initial	0.0150		0.0150		0		0
Change	-4x		-3x		+2x		+6x
Equilibrium	0.0150 - 4x		0.0150 - 3x		+2x		+6x

All intermediate concentration values are unrounded.

$$[N_2]_{eq} = 2x = 1.96 \times 10^{-3} M$$

$$[H_2O]_{eq} = (6 \text{ mol } H_2O/2 \text{ mol } N_2) (1.96 \text{ x } 10^{-3}) = 5.8800 \text{ x } 10^{-3} M$$

$$[H_2O]_{eq} = (6 \text{ mol } H_2O/2 \text{ mol } N_2) (1.96 \times 10^{-3}) = 5.8800 \times 10^{-3} M$$

$$[NH_3]_{eq} = (0.0150 \text{ mol } NH_3/1.00 \text{ L}) - (4 \text{ mol } NH_3/2 \text{ mol } N_2) (1.96 \times 10^{-3}) = 1.1080 \times 10^{-2} M$$

$$[O_2]_{eq} = (0.0150 \text{ mol } O_2/1.00 \text{ L}) - (3 \text{ mol } O_2/2 \text{ mol } N_2) (1.96 \times 10^{-3}) = 1.2060 \times 10^{-2} M$$

$$[O_2]_{eq} = (0.0150 \text{ mol } O_2/1.00 \text{ L}) - (3 \text{ mol } O_2/2 \text{ mol } N_2) (1.96 \text{ x } 10^{-3}) = 1.2060 \text{ x } 10^{-2} M$$

$$K_{c} = \frac{\left[N_{2}\right]^{2} \left[H_{2}O\right]^{6}}{\left[NH_{3}\right]^{4} \left[O_{2}\right]^{3}} = \frac{\left[1.96 \times 10^{-3}\right]^{2} \left[5.8800 \times 10^{-3}\right]^{6}}{\left[1.1080 \times 10^{-2}\right]^{4} \left[1.2060 \times 10^{-2}\right]^{3}} = 6.005859 \times 10^{-6} = 6.01 \times 10^{-6}$$

If values for concentrations were rounded to calculate  $K_c$ , the answer is 5.90 x  $10^{-6}$ .

17.46 Pressure (atm) FeO(s) + CO(g)Initial Change Equilibrium

$$K_{\rm p} = \frac{P_{\rm CO_2}}{P_{\rm CO}} = 0.403 = \frac{x}{1.00 - x}$$

$$x = 0.28724 = 0.287$$
 atm CO<sub>2</sub>

$$1.00 - x = 1.00 - 0.28724 = 0.71276 =$$
**0.71 atm CO**

- 17.47 Equilibrium position refers to the specific concentrations or pressures of reactants and products that exist at equilibrium, whereas equilibrium constant refers to the overall ratio of equilibrium concentrations and not to specific concentrations. Reactant concentration changes cause changes in the specific equilibrium concentrations of reactants and products (equilibrium position), but not in the equilibrium constant.
- 17.48 A positive  $\Delta H_{\text{rxn}}$  indicates that the reaction is endothermic, and that heat is consumed in the reaction:  $NH_4Cl(s) + heat = NH_3(g) + HCl(g)$ 
  - a) The addition of heat (high temperature) causes the reaction to proceed to the right to counterbalance the effect of the added heat. Therefore, more products form at a higher temperature and container (B) with the largest number of product molecules best represents the mixture.
  - b) When heat is removed (low temperature), the reaction shifts to the left to offset that disturbance. Therefore, NH<sub>3</sub> and HCl molecules combine to form more reactant and container (A) with the smallest number of product gas molecules best represents the mixture.
- 17.49 Equilibrium component concentration values may change but the mass action expression of these concentrations is a constant as long as temperature remains constant. Changes in component amounts, pressures (volumes), or addition of a catalyst will not change the value of the equilibrium constant.
- a) Rate<sub>f</sub> =  $k_f$  [Reactants]<sup>x</sup>. An increase in reactant concentration shifts the equilibrium to the right by increasing 17.50 the initial forward rate. Since  $K_{eq} = k_f/k_r$  and  $k_f$  and  $k_r$  are not changed by changes in concentration,  $K_{eq}$  remains
  - b) A decrease in volume causes an increase in concentrations of gases. The reaction rate for the formation of fewer moles of gases is increased to a greater extent. Again, the  $k_{\rm f}$  and  $k_{\rm r}$  values are unchanged.
  - c) An increase in temperature increases  $k_r$  to a greater extent for an exothermic reaction and thus lowers the  $K_{eq}$ value.

- 17.51 An endothermic reaction can be written as: reactants + heat  $\leftrightarrows$  products. A rise in temperature (increase in heat) favors the forward direction of the reaction, i.e., the formation of products and consumption of reactants. Since K = [products]/[reactants], the addition of heat increases the numerator and decreases the denominator, making  $K_2$  larger than  $K_1$ .
- 17.52  $XY(s) \Rightarrow X(g) + Y(s)$  Since Product Y is a solid substance, addition of solid Y has no effect on the equilibrium position (as long as some Y is present). **Scene A** best represents the system at equilibrium after the addition of two formula units of Y. More Y is present but the amounts of X and XY do not change.
- 17.53 a) Equilibrium position shifts **toward products**. Adding a reactant (CO) causes production of more products as the system will act to reduce the increase in reactant by proceeding toward the product side, thereby consuming additional CO.
  - b) Equilibrium position shifts **toward products**. Removing a product (CO<sub>2</sub>) causes production of more products as the system acts to replace the removed product.
  - c) Equilibrium position **does not shift**. The amount of a solid reactant or product does not impact the equilibrium as long as there is some solid present.
  - d) Equilibrium position shifts **toward reactants**. When product is added, the system will act to reduce the increase in product by proceeding toward the reactant side, thereby consuming additional CO<sub>2</sub>; dry ice is solid carbon dioxide that sublimes to carbon dioxide gas. At very low temperatures, CO<sub>2</sub> solid will not sublime, but since the reaction lists carbon dioxide as a gas, the assumption that sublimation takes place is reasonable.
- 17.54 a) **no change**

- b) no change
- c) shifts toward the products
- d) shifts toward the reactants
- 17.55 An increase in container volume results in a decrease in pressure (Boyle's Law). Le Châtelier's principle states that the equilibrium will shift in the direction that forms more moles of gas to offset the decrease in pressure.
  - a) More F forms (2 moles of gas) and less  $\mathbf{F}_2$  (1 mole of gas) is present as the reaction shifts toward the right.
  - b) More  $C_2H_2$  and  $H_2$  form (4 moles of gas) and less  $CH_4$  (2 moles of gas) is present as the reaction shifts toward the right.
- 17.56 a) more CO<sub>2</sub> and H<sub>2</sub>O; less C<sub>3</sub>H<sub>8</sub> and O<sub>2</sub>
  - b) more NH<sub>3</sub> and O<sub>2</sub>; less N<sub>2</sub> and H<sub>2</sub>O
- 17.57 The purpose of adjusting the volume is to cause a shift in equilibrium.
  - a) Because the number of reactant gaseous moles (4 H<sub>2</sub>) equals the product gaseous moles (4 H<sub>2</sub>O), a change in volume will have **no effect** on the yield.
  - b) The moles of gaseous product (2 CO) exceed the moles of gaseous reactant (1  $O_2$ ). A decrease in pressure favors the reaction direction that forms more moles of gas, so **increase** the reaction vessel volume.
- 17.58 a) increase volume b) decrease volume
- 17.59 An increase in temperature (addition of heat) causes a shift in the equilibrium <u>away</u> from the side of the reaction with heat.

a) 
$$CO(g) + 2H_2(g) = CH_3OH(g) + heat$$
  $\Delta H_{rxn} = -90.7 \text{ kJ}$ 

A negative  $\Delta H_{\text{rxn}}$  indicates an exothermic reaction. The equilibrium shifts to the left, away from heat, toward the reactants, so amount of product **decreases**.

b) 
$$C(s) + H_2O(g) + heat = CO(g) + H_2(g)$$
  $\Delta H_{rxn} = 131 \text{ kJ}$ 

A positive  $\Delta H_{\text{rxn}}$  indicates an endothermic reaction. The equilibrium shifts to the right, away from heat, toward the products, so amounts of products **increase**.

c) 
$$2NO_2(g) + heat = 2NO(g) + O_2(g)$$

The reaction is endothermic. The equilibrium shifts to the right, away from heat, toward the product, so amounts of products **increase**.

d) 
$$2C(s) + O_2(g) = 2CO(g) + heat$$

The reaction is exothermic. The equilibrium shifts to the left, away from heat, toward the reactants; amount of product **decreases**.

- 17.60 a) decrease b) decrease c) decrease d) increase
- $4 \text{ Fe}_3\text{O}_4(s) + \text{O}_2(g) \leftrightarrows 6 \text{ Fe}_2\text{O}_3(s)$   $K_p = 2.5 \text{ x } 10^{87} \text{ at } 298 \text{ K}$ 17.61 a)  $K_p = \frac{1}{P_{O_2}} = 2.5 \times 10^{87}$  $P_{02} = 4.0 \times 10^{-88} \text{ atm}$ 
  - b)  $Q_p = \frac{1}{P_{O_2}} = 1/(0.21) = 4.7619$  (unrounded)

shift in equilibrium to the side with the fewer moles of gas.

- $K_{\rm p} > Q_{\rm p}$  thus, the reaction will proceed to the **right**. c)  $K_{\rm p} = K_{\rm c} (RT)^{\Delta n}$  $K_c = K_p/((RT)^{\Delta n})$   $\Delta n = 0 - 1 = -1$   $K_c = (2.5 \times 10^{87})/[(0.0821) (298)]^{-1} = 6.11645 \times 10^{88} =$ **6.1 \times 10^{88}**
- a)  $SO_2(g) + \frac{1}{2}O_2(g) \leftrightarrows SO_3(g) + heat$ 17.62 The forward reaction is exothermic ( $\Delta H_{\text{IND}}$  is negative), so it is favored by **lower temperatures**. Lower temperatures will cause a shift to the right, the heat side of the reaction. There are fewer moles of gas as products  $(1 \text{ SO}_3)$  than as reactants  $(1 \text{ SO}_2 + \frac{1}{2} \text{ O}_2)$ , so products are favored by **higher pressure**. High pressure will cause a
  - b) Addition of O<sub>2</sub> would **decrease**  $Q(Q = \frac{[SO_3]}{[SO_2][O_2]^{1/2}})$  and have **no impact on** K.
  - c) To enhance yield of SO<sub>3</sub>, a low temperature is used. Reaction rates are slower at lower temperatures, so a catalyst is used to speed up the reaction.

17.63 a) 
$$Q_c = \frac{[XY]^2}{[X_2][Y_2]}$$

b) Scene A: 
$$Q_c = \frac{[0]^2}{[0.4][0.4]} = \mathbf{0}$$

Scene B: 
$$Q_c = \frac{[0.4]^2}{[0.2][0.2]} = 4$$

Scenes C-E: 
$$Q_c = \frac{[0.6]^2}{[0.1][0.1]} = 36 = 4 \times 10^1$$

- c) **left-to-right**. Frame A must be the earliest time.
- d)  $K = 4 \times 10^{1}$
- e) Scene B, at higher temperatures, the reaction shifts to the left (forming more X<sub>2</sub> and Y<sub>2</sub>).
- f) None, volume (pressure) has no effect on the position of the equilibrium.
- 17.64 Calculate  $K_c$

$$K_{\rm c} = \frac{[{\rm CO}_2][{\rm H}_2]}{[{\rm CO}][{\rm H}_2{\rm O}]} = \frac{[0.40][0.10]}{[0.10][0.10]} = 4.0$$

Calculate new concentrations

New H<sub>2</sub> = 0.10 M + (0.60 mol / 2.0 L) = 0.40 M

Concentration (M) 
$$CO(g) + H_2O(g) \leftrightarrows CO_2(g) + H_2(g)$$
  
Initial 0.10 0.10 0.40 0.40  
Change  $+x + x -x -x -x$   
Equilibrium 0.10 + x 0.10 + x 0.40 - x 0.40 - x

$$K_{c} = \frac{\left[\text{CO}_{2}\right]\left[\text{H}_{2}\right]}{\left[\text{CO}\right]\left[\text{H}_{2}\text{O}\right]} = \frac{\left[0.40 - x\right]\left[0.40 - x\right]}{\left[0.10 + x\right]\left[0.10 + x\right]} = \frac{\left[0.40 - x\right]^{2}}{\left[0.10 + x\right]^{2}} = 4.0$$

$$\frac{\left[0.40 - x\right]}{\left[0.10 + x\right]} = 2.0$$

$$x = 0.066667 \text{ (unrounded)}$$

$$\left[\text{CO}\right] = \left[\text{H}_{2}\text{O}\right] = 0.10 + x = 0.10 + 0.066667 = 0.166667 = 0.17 M$$

$$\left[\text{CO}_{2}\right] = \left[\text{H}_{2}\right] = 0.40 - x = 0.40 - 0.066667 = 0.333333 = 0.33 M$$

17.65 a) You are given a value of  $K_c$  but the amounts of reactant and product is given in units of pressure. Convert  $K_c$  to  $K_p$ .

 $K_p = K_c (RT)^{\Delta n}$   $\Delta n = 1 - 2 = -1$  (1 mol of product,  $C_2H_5OH$  and 2 mol of reactants,  $C_2H_4 + H_2O$ )  $K_p = K_c (RT)^{-1} = (9 \times 10^3)[(0.0821 \text{ L*atm/mol*K}) (600. \text{ K})]^{-1} = 1.8270 \times 10^2 \text{ (unrounded)}$ Substitute the given values into the equilibrium expression and solve for  $P_{C_2H_4}$ .

$$K_{\rm p} = \frac{P_{\rm C_2H_5OH}}{P_{\rm C_2H_4}P_{\rm H_2O}} = \frac{200.}{P_{\rm C_2H_4} (400.)} = 1.8270 \text{ x } 10^2$$

$$P_{\rm C_2H_4} = 2.7367 \text{ x } 10^{-3} = 3 \text{ x } 10^{-3} \text{ atm}$$

- b) The forward direction, towards the production of ethanol, produces the least number of moles of gas and is favored by **high pressure**. A **low temperature** favors an exothermic reaction.
- c) No, condensing the  $C_2H_5OH$  would not increase the yield. Ethanol has a lower boiling point (78.5°C) than water (100°C). Decreasing the temperature to condense the ethanol would also condense the water, so moles of gas from each side of the reaction are removed. The direction of equilibrium (yield) is unaffected when there is no net change in the number of moles of gas.

17.66 
$$n/V = M = P / RT = \frac{(2.0 \text{ atm})}{\left(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}\right) \left(\left(273.2 + 25.0\right) \text{K}\right)} = 0.0816919 M \text{ each gas (unrounded)}$$

$$\frac{\text{H}_2(g) + \text{CO}_2(g)}{0.0816919 - x + 0.0816919 - x + x} + \frac{\text{CO}(g)}{x}$$

$$K_c = \frac{\left[\text{H}_2\text{O}\right]\left[\text{CO}\right]}{\left[\text{H}_2\right]\left[\text{CO}_2\right]} = 0.534 = \frac{\left[x\right]\left[x\right]}{\left[0.0816919 - x\right]\left[0.0816919 - x\right]} = \frac{\left[x\right]^2}{\left[0.0816919 - x\right]^2}$$

$$(0.534)^{1/2} = 0.730753 = \frac{\left[x\right]}{\left[0.0816919 - x\right]}$$

$$x = 0.03449 \text{ (unrounded)}$$

 $Mass \; H_2 \; [(0.0816919 - 0.03449) \; mol/L] \\ (1.00 \; L) \; (2.016 \; g \; H_2/mol) = 0.095159 \\ = \textbf{0.095} \; \textbf{g} \; \textbf{H}_2 \\ (0.0816919 - 0.03449) \; mol/L] \\ (0.08169 - 0.03449) \; mol/L] \\ (0.0816919 - 0.03449) \; mol/L] \\ (0.08169 - 0$ 

To get the two equations to sum to the desired equation, the first equation must be reversed and doubled. This will result in squaring the reciprocal of its  $K_c$  value. The other equation does not need to be changed. Adding the two equations means the new  $K_c$  value will be the product of the individual  $K_c$  values.

$$\frac{2 \text{ NO}(g)}{2 \text{ NO}(g)} \leftrightarrows \text{ N}_2(g) + \text{O}_2(g) \qquad K_1 = (K_c)^{-2} = 4.340 \text{ x } 10^{18} = K_2 \text{ (unrounded)}$$

$$\frac{2 \text{ NO}_2(g)}{2 \text{ NO}_2(g)} \leftrightarrows \frac{2 \text{ NO}(g)}{2 \text{ NO}_2(g)} + \text{O}_2(g) \qquad K_2 = K_c = 1.1 \text{ x } 10^{-5}$$
Overall:  $2 \text{ NO}_2(g) \leftrightarrows \text{N}_2(g) + 2 \text{ O}_2(g) \qquad K_c \text{ (overall)} = K_1 K_2 = 4.774 \text{ x } 10^{13} = \textbf{4.8 x } \textbf{10}^{13} M$ 

17.68 
$$M_2(g) + N_2(g) \iff \text{tuc}(g)$$
  $K_c = \frac{[MN]^2}{[M_2][N_2]}$ 

Scene A: Concentrations:  $[M_2] = [N_2] = 0.20 M$ ; [MN] = 0.40 M

$$K_{\rm c} = \frac{\left[0.40\right]^2}{\left[0.20\right]\left[0.20\right]} = 4.0$$

Scene B:

Concentration (M) 
$$M_2(g) + N_2(g) = 2MN(g)$$
  
Initial 0.60 0.30 0  
Change  $-x - x + 2x$   
Equilibrium 0.60  $-x = 0.30 - x = 2x$ 

$$K_{\rm c} = 4.0 = \frac{\left[2x\right]^2}{\left[0.60 - x\right]\left[0.30 - x\right]}$$

$$4.0 = \frac{4x^2}{0.18 - 0.90x + x^2}$$
$$4x^2 = 0.72 - 3.6x + 4x^2$$

$$3.6x = 0.72$$

$$x = 0.20 \text{ M}$$

$$[M_2] = 0.60 - x = 0.60 - 0.20 = 0.40 M$$

$$[N_2] = 0.30 - x = 0.30 - 0.20 = 0.10 M$$

$$[MN] = 2x = 2(0.20 \text{ M}) = 0.40 M$$

17.69 a) You are given a value of  $K_c$  but the amounts of reactant and product is given in units of pressure. Convert  $K_c$  to  $K_p$ .

$$K_{\rm p} = K_{\rm c}({\rm RT})^{\Delta n}$$
  $\Delta n = 2 - 3 = -1$  (2 mol of product, SO<sub>3</sub> and 3 mol of reactants, 2 SO<sub>2</sub> + O<sub>2</sub>)  
 $K_{\rm p} = K_{\rm c}({\rm RT})^{\Delta n} = K_{\rm c}({\rm RT})^{-1} = (1.7 \times 10^8)[(0.0821 \text{ L} \cdot \text{atm/mol} \cdot \text{K}) (600. \text{ K})]^{-1} = 3.451 \times 10^6 \text{ (unrounded)}$ 

$$K_{\rm p} = \frac{P_{\rm SO_3}^2}{P_{\rm SO_2}^2 P_{\rm O_2}} = \frac{\left(300.\right)^2}{P_{\rm SO_2}^2 \left(100.\right)} = 3.451 \times 10^6$$

$$P_{SO_2} = 0.016149 = 0.016$$
 atm

b) Create a reaction table that describes the reaction conditions. Since the volume is  $1.0\,L$ , the moles equals the molarity. Note the 2:1:2 mole ratio between  $SO_2:O_2:SO_3$ 

x = 0.0010, therefore:

$$[SO_2] = 0.0040 - 2(0.0010) = 0.0020 M$$

$$[O_2] = 0.0028 - 0.0010 = 0.0018 M$$

$$[SO_3] = 2(0.0010) = 0.0020 M$$

Substitute equilibrium concentrations into the equilibrium expression and solve for  $K_c$ .

$$K_{\rm c} = \frac{\left[\text{SO}_3\right]^2}{\left[\text{SO}_2\right]^2 \left[\text{O}_2\right]} = \frac{\left[0.0020\right]^2}{\left[0.0020\right]^2 \left[0.0018\right]} = 555.5556 = 5.6 x 10^2$$

The pressure of  $SO_2$  is estimated using the concentration of  $SO_2$  and the ideal gas law (although the ideal gas law is not well behaved at high pressures and temperatures).

$$P_{SO_2} = \frac{nRT}{V} = \frac{(0.0020 \text{ mol}) \left(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}\right) (1000. \text{ K})}{(1.0 \text{ L})} = 0.1642 = \textbf{0.16} \text{ atm}$$

The equilibrium constant for the reaction is  $K_p = P_{CO_2} = 0.220$  atm.

The amount of calcium carbonate solid in the container at the first equilibrium equals the original amount, 0.100 mol, minus the amount reacted to form 0.220 atm of carbon dioxide. The moles of CaCO<sub>3</sub> reacted is equal to the number of moles of carbon dioxide produced. Use the pressure of CO2 and the Ideal Gas Equation to calculate the moles of CaCO<sub>3</sub> reacted:

Moles  $CaCO_3 = moles CO_2 = n = PV/RT$ 

$$n = \frac{(0.220 \text{ atm})(10.0 \text{ L})}{\left(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}\right) (385 \text{ K})} = 0.06960 \text{ mol CaCO}_3 \text{ lost (unrounded)}$$

 $0.100 \text{ mol } \text{CaCO}_3 - 0.06960 \text{ mol } \text{CaCO}_3 = 0.0304 \text{ mol } \text{CaCO}_3 \text{ at first equilibrium}$ 

As more carbon dioxide gas is added, the system returns to equilibrium by shifting to the left to convert the added carbon dioxide to calcium carbonate to maintain the partial pressure of carbon dioxide at 0.220 atm  $(K_p)$ . Convert the added 0.300 atm of CO<sub>2</sub> to moles using the Ideal Gas Equation. The moles of CO<sub>2</sub> reacted equals the moles of CaCO<sub>3</sub> formed.

Moles CaCO<sub>3</sub> = moles CO<sub>2</sub> = 
$$n = PV/RT$$
  

$$n = \frac{(0.300 \text{ atm})(10.0 \text{ L})}{\left(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}\right)(385 \text{ K})} = 0.09491 \text{ mol CaCO}_3 \text{ formed (unrounded)}$$

Add the moles of CaCO<sub>3</sub> formed in the second equilibrium to the moles of CaCO<sub>3</sub> at the first equilibrium position and convert to grams.

Mass 
$$CaCO_3 = \left(\frac{0.0304 \text{ mol} + 0.09491 \text{ mol } CaCO_3}{1 \text{ mol } CaCO_3}\right) \left(\frac{100.09 \text{ g } CaCO_3}{1 \text{ mol } CaCO_3}\right) = 12.542 = 12.5 \text{ g } CaCO_3$$

17.71 a) 
$$C_2H_4(g) + 3 O_2(g) \leftrightarrows 2 CO_2(g) + 2 H_2O(g)$$
  
b)  $4 NO_2(g) + 6 H_2O(g) \leftrightarrows 4 NH_3(g) + 7 O_2(g)$ 

17.72 The first equation is in the correct form, but the second equation must be reversed. Reversing the equation leads to the reciprocal of the K value.

a) Calculate the partial pressures of oxygen and carbon dioxide because volumes are proportional to moles of gas, 17.73 so volume fraction equals mole fraction. Assume that the amount of carbon monoxide gas is small relative to the other gases, so the total volume of gases equals  $V_{\text{CO}_2} + V_{\text{O}_2} + V_{\text{N}_2} = 10.0 + 1.00 + 50.0 = 61.0$ 

$$P_{\text{CO}_2} = \left(\frac{10.0 \text{ mol CO}_2}{61.0 \text{ mol gas}}\right) (4.0 \text{ atm}) = 0.6557377 \text{ atm (unrounded)}$$

$$P_{\rm O_2} = \left(\frac{1.00 \text{ mol O}_2}{61.0 \text{ mol gas}}\right) (4.0 \text{ atm}) = 0.06557377 \text{ atm (unrounded)}$$

Use the partial pressures and given  $K_p$  to find  $P_{CO}$ .

$$2 \operatorname{CO}_2(g) \leftrightarrows 2 \operatorname{CO}(g) + \operatorname{O}_2(g)$$

$$K_{\rm p} = \frac{P_{\rm CO}^2 P_{\rm O_2}}{P_{\rm CO_2}^2} = \frac{P_{\rm CO}^2 \left(0.06557377\right)}{\left(0.6557377\right)^2} = 1.4 \times 10^{-28}$$

$$P_{\rm CO} = 3.0299 \times 10^{-14} = 3.0 \times 10^{-14} \text{ atm}$$

$$P_{\rm CO} = 3.0299 \times 10^{-14} = 3.0 \times 10^{-14} \text{ atm}$$

b) Convert partial pressure to moles per liter using the ideal gas equation, and then convert moles of CO to grams.

$$n_{\text{CO}}/V = P/RT = \frac{\left(3.0299 \times 10^{-14} \text{ atm}\right)}{\left(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}\right) \left(800 \text{ K}\right)} = 4.6131 \times 10^{-16} \text{ mol/L (unrounded)}$$

$$\left(\frac{4.6131 \times 10^{-16} \text{ mol CO}}{\text{L}}\right) \left(\frac{28.01 \text{ g CO}}{1 \text{ mol CO}}\right) \left(\frac{1 \text{ pg}}{10^{-12} \text{ g}}\right) = 0.01292 = \textbf{0.013 pg CO/L}$$

17.74 a) 
$$Fe^{2+} + 2 Fe^{3+}$$

b)  $(0.050 \text{ mol H}_2\text{O})/(1.0 \text{ L}) = 0.050 \text{ M} \text{H}_2\text{O}$ 

$$K_{\rm c} = \frac{\left[{\rm H}_2\right]^4}{\left[{\rm H}_2{\rm O}\right]^4} = 5.1 = \frac{\left[4x\right]^4}{\left[0.050 - 4x\right]^4}$$

1.50277 = 
$$\frac{[4x]}{[0.050 - 4x]}$$
 (unrounded)

$$x = (7.50553 \times 10^{-3} \text{ mol/L}) (1.0 \text{ L}) = 7.50553 \times 10^{-3} \text{ mol Fe}_3\text{O}_4 \text{ reacting (unrounded)}$$
  
Mass Fe<sub>3</sub>O<sub>4</sub> =  $(7.50553 \times 10^{-3}) (231.55 \text{ g Fe}_3\text{O}_4/1 \text{ mol Fe}_3\text{O}_4) = 1.7494 = 1.7 \text{ g Fe}_3\text{O}_4$ 

- 17.75 Although the yield is favored by low temperature, the rate of formation is not. In fact, ammonia forms so slowly at low temperatures that the process becomes uneconomical. In practice, a compromise is achieved that optimizes yield and rate (high pressure, continual removal of NH<sub>3</sub>, increasing the temperature).
- a) Write a reaction table given that  $P_{\text{CH}_4}$  (init) =  $P_{\text{CO}_2}$  (init) = 10.0 atm, substitute equilibrium values into the 17.76 equilibrium expression, and solve for  $P_{\rm H_2}$ .

Pressure (atm) 
$$CH_4(g) + CO_2(g) \leftrightarrows 2CO(g) + 2H_2(g)$$
  
Initial 10.0 10.0 0 0 0  
Change  $-x - x + 2x + 2x$   
Equilibrium  $10.0 - x = 10.0 - x = 2x = 2x$   
 $K_p = \frac{P_{CO}^2 P_{H_2}^2}{P_{CH_4} P_{CO_2}} = \frac{(2x)^2 (2x)^2}{(10.0 - x)(10.0 - x)} = \frac{(2x)^4}{(10.0 - x)^2} = 3.548 \times 10^6 \text{ (take square root of each side)}$   
 $\frac{(2x)^2}{(10.0 - x)} = 1.8836135 \times 10^3$ 

A quadratic is necessary:

$$4x^2 + (1.8836135 \times 10^3 x) - 1.8836135 \times 10^4 = 0$$
 (unrounded)  
a = 4 b = 1.8836135 x 10<sup>3</sup> c = -1.8836135 x 10<sup>4</sup>

$$a = 4$$
  $b = 1.8836135 \times 10^3$   $c = -1.8836135 \times 10^4$ 

$$x = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

$$x = \frac{-1.8836135 \times 10^3 \pm \sqrt{\left(1.8836135 \times 10^3\right)^2 - 4(4)\left(-1.8836135 \times 10^4\right)}}{2(4)}$$

x = 9.796209 (unrounded)

 $P ext{ (hydrogen)} = 2x = 2 (9.796209) = 19.592418 atm (unrounded)$ 

If the reaction proceeded entirely to completion, the partial pressure of H<sub>2</sub> would be 20.0 atm (pressure is proportional to moles, and twice as many moles of H<sub>2</sub> form for each mole of CH<sub>4</sub> or CO<sub>2</sub> that reacts).

The percent yield is 
$$\frac{19.592418 \text{ atm}}{20.0 \text{ atm}} (100\%) = 97.96209 = 98.0\%.$$

b) Repeat the calculations for part (a) with the new  $K_p$  value. The reaction table is the same.

$$K_{\rm p} = \frac{P_{\rm CO}^2 P_{\rm H_2}^2}{P_{\rm CH_4} P_{\rm CO_2}} = \frac{(2x)^2 (2x)^2}{(10.0 - x)(10.0 - x)} = \frac{(2x)^4}{(10.0 - x)^2} = 2.626 \times 10^7$$

$$\frac{(2x)^2}{(10.0 - x)} = 5.124451 \times 10^3$$

A quadratic is needed:

$$x = \frac{-5.124451 \times 10^{3} - 5.124451 \times 10^{4} = 0 \text{ (unrounded)}}{2(4)}$$

$$x = \frac{-5.124451 \times 10^{3} \pm \sqrt{(5.124451 \times 10^{3})^{2} - 4(4)(-5.124451 \times 10^{4})}}{2(4)}$$

x = 9.923138 (unrounded)

 $P ext{ (hydrogen)} = 2x = 2 ext{ (9.923138)} = 19.846276 atm ext{ (unrounded)}$ 

If the reaction proceeded entirely to completion, the partial pressure of H<sub>2</sub> would be 20.0 atm (pressure is proportional to moles, and twice as many moles of H2 form for each mole of CH4 or CO2 that reacts).

The percent yield is 
$$\frac{19.846276 \text{ atm}}{20.0 \text{ atm}} (100\%) = 99.23138 = 99.0\%.$$

a) Multiply the second equation by 2 to cancel the moles of CO produced in the first reaction.  $K_p$  for the second 17.77 reaction is then  $(K_p)^2$ .

$$2 \text{ CH}_4(g) + O_2(g) + 2 \text{ H}_2O(g) \leftrightarrows 2 \text{ CO}_2(g) + 6 \text{ H}_2(g)$$

- $2 \text{ CH}_4(g) + O_2(g) + 2 \text{ H}_2O(g) \leftrightarrows 2 \text{ CO}_2(g) + 6 \text{ H}_2(g)$ b)  $K_p = (9.34 \times 10^{28}) (1.888) = 1.76339 \times 10^{29} =$ **1.76 \times 10^{29}**
- c)  $\Delta n = 8 5 = 3$  (8 moles of product gas 5 moles of reactant gas)

$$K_{\rm c} = \frac{K_{\rm p}}{[RT]^{\Delta n}}$$

$$K_{\rm c} = \frac{1.76339 \times 10^{29}}{[(0.0821 \text{ atm} \cdot \text{L/mol} \cdot \text{K})(1000)]^3} = 3.18654 \times 10^{23} = 3.19 \times 10^{23}$$

d) The initial total pressure is given as 30. atm. To find the final pressure use relationship between pressure and number of moles of gas:  $n_{\text{initial}}/P_{\text{initial}} = n_{\text{final}}/P_{\text{final}}$ 

Total mol of gas initial =  $2.0 \text{ mol CH}_4 + 1.0 \text{ mol O}_2 + 2.0 \text{ mol H}_2\text{O} = 5.0 \text{ mol}$ 

Total mol of gas final =  $2.0 \text{ mol } CO_2 + 6.0 \text{ mol } H_2 = 8.0 \text{ mol}$ 

$$P_{\text{final}} = \frac{30. \text{ atm reactants}}{5 \text{ mol products}} = 48 \text{ atm}$$

a) Careful reading of the problem indicates that the given  $K_p$  occurs at 1000. K and that the initial pressure of  $N_2$  is 200. atm. Log  $K_p = -43.10$ ;  $K_p = 10^{-43.10} = 7.94328 \times 10^{-44}$  Pressure (atm)  $N_2(g) \rightleftharpoons 2N(g)$  Initial 200.

Pressure (atm) 
$$N_2(g) \implies 2N(g)$$
Initial 200. 0
Change  $-x +2x$ 
Equilibrium  $200-x 2x$ 

$$K_p = \frac{(P_N)^2}{(P_{N_2})} = 7.94328 \times 10^{-44}$$

$$\frac{(2x)^2}{(200-x)} = 7.94328 \times 10^{-44}$$
 Assume  $200.-x \approx 200.$ 

$$P_{\rm N} = 2x = \sqrt{(200.)(7.94328 \times 10^{-44})} = 3.985795 \times 10^{-21} = \textbf{4.0} \times \textbf{10}^{-21}$$
b) Log  $K_{\rm p} = -17.30$ ;  $K_{\rm p} = 10^{-17.30} = 5.01187 \times 10^{-18}$ 
Pressure (atm)  $H_2(g) \leftrightarrows 2H(g)$ 
Initial  $600.$  0
Change  $-x + 2x$ 
Equilibrium  $600 - x + 2x$ 

$$K_{\rm p} = \frac{(P_{\rm H})^2}{(P_{\rm H_2})} = 5.01187 \times 10^{-18}$$

$$\frac{(2x)^2}{(600. - x)} = 5.01187 \times 10^{-18} \qquad \text{Assume } 600. - x \cong 600.$$

$$P_{\rm H} = 2x = \sqrt{(600.)(5.01187 \times 10^{-18})} = 5.48372 \times 10^{-8} = \textbf{5.5} \times \textbf{10}^{-8}$$

c) Convert pressures to moles using the ideal gas law. PV = nRT. Convert moles to atoms using Avogadro's number.

Moles 
$$N/V = P/RT = \frac{\left(3.985795 \times 10^{-21} \text{atm}\right)}{\left(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}\right) \left(1000.\text{K}\right)} \left(\frac{6.022 \times 10^{23} \text{ atoms}}{\text{mol}}\right)$$

$$= 29.2356 = \mathbf{29 \text{ N atoms/L}}$$
Moles  $H/V = P/RT = \frac{\left(5.48372 \times 10^{-8} \text{ atm}\right)}{\left(0.0821 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}\right) \left(1000.\text{ K}\right)} \left(\frac{6.022 \times 10^{23} \text{ atoms}}{\text{mol}}\right)$ 

$$= 4.022 \times 10^{14} = 4.0 \times 10^{14} \text{ H atoms/L}$$

d) The more reasonable step is  $N_2(g) + H(g) \rightarrow NH(g) + N(g)$ . With only 29 N atoms in 1.0 L, the first reaction would produce virtually no NH(g) molecules. There are orders of magnitude more  $N_2$  molecules than N atoms, so the second reaction is the more reasonable step.

17.79 a) 
$$3 H_2(g) + N_2(g) \iff 2 NH_3(g)$$
 The mole ratio  $H_2/N_2 = 3/1$ ; if  $N_2 = x$ ,  $H_2 = 3x$   $P_{NH_3} = 50$ . atm 
$$K_p = \frac{\left(P_{NH_3}\right)^2}{\left(P_{N_2}\right)\left(P_{H_2}\right)^3} = 1.00 \times 10^{-4}$$

$$K_p = \frac{\left(50.\right)^2}{\left(x\right)\left(3\,x\right)^3} = 1.00 \times 10^{-4}$$

$$x = 31.02016 = 31 \text{ atm } N_2$$

$$3x = 3 (31.02016) = 93.06048 = 93 \text{ atm } H_2$$

$$P_{total} = P_{nitrogen} + P_{hydrogen} + P_{ammonia} = (31.02016 \text{ atm}) + (93.06048 \text{ atm}) + (50. \text{ atm})$$

$$= 174.08064 = 174 \text{ atm total}$$
b)  $K_p = \frac{\left(50.\right)^2}{\left(x\right)\left(6x\right)^3} = 1.00 \times 10^{-4}$   $N_2 = x \text{ and } H_2 = 6x$ 

$$x = 18.44 = 18 \text{ atm } N_2$$

$$6x = 6 (18.44) = 110.64 = 111 \text{ atm } H_2$$

$$P_{total} = P_{nitrogen} + P_{hydrogen} + P_{ammonia} = (18.44 \text{ atm}) + (110.64 \text{ atm}) + (50. \text{ atm})$$

$$= 179.09 = 179 \text{ atm total}$$

This is not a valid argument. The total pressure in (b) is greater than in (a) to produce the same amount of NH<sub>3</sub>.

17.80 a) Equilibrium partial pressures for the reactants, nitrogen and oxygen, can be assumed to equal their initial partial pressures because the equilibrium constant is so small that very little nitrogen and oxygen will react to form nitrogen monoxide. After calculating the equilibrium partial pressure of nitrogen monoxide, test this assumption by comparing the partial pressure of nitrogen monoxide with that of nitrogen and oxygen.

Pressure (atm) 
$$N_2(g) + O_2(g) \Rightarrow 2NO(g)$$
  
Initial  $0.780 \quad 0.210 \quad 0$   
Change  $-x \quad -x \quad +2x$   
Equilibrium  $0.780 - x \quad 0.210 - x \quad 2x$   
 $K_p = \frac{(P_{NO})^2}{(P_{N_2})(P_{O_2})} = 4.35 \times 10^{-31}$ 

$$\frac{(2x)^2}{(0.780 - x)(0.210 - x)} = 4.35 \times 10^{-31}$$
 Assume *x* is small because *K* is small.

$$\frac{\left(2x\right)^2}{\left(0.780\right)\left(0.210\right)} = 4.35 \times 10^{-31}$$

$$x = 1.33466 \times 10^{-16}$$
 (unrounded)

Based on the small amount of nitrogen monoxide formed, the assumption that the partial pressures of nitrogen and oxygen change to an insignificant degree holds.

P<sub>nitrogen</sub> (equilibrium) = 
$$(0.780 - 1.33466 \times 10^{-16})$$
 atm = **0.780 atm N**<sub>2</sub>  
P<sub>oxygen</sub> (equilibrium) =  $(0.210 - 1.33466 \times 10^{-16})$  atm = **0.210 atm O**<sub>2</sub>  
P<sub>NO</sub> (equilibrium) =  $2(1.33466 \times 10^{-16})$  atm =  $2.66932 \times 10^{-16}$  = **2.67 x 10<sup>-16</sup> atm NO**

$$P_{\text{NO}}$$
 (equilibrium) = 2 (1.33466 x 10<sup>-16</sup>) atm = 2.66932 x 10<sup>-16</sup> = **2.67** x **10<sup>-16</sup> atm NO**

b) The total pressure is the sum of the three partial pressures:

$$0.780 \text{ atm} + 0.210 \text{ atm} + 2.67 \times 10^{-16} \text{ atm} = 0.990 \text{ atm}$$

0.780 atm + 0.210 atm + 2.67 x 
$$10^{-16}$$
 atm = **0.990 atm** c)  $K_p = K_c(RT)^{\Delta n}$   $\Delta n = 2$  mol NO product  $-2$  mol reactant  $(1 \text{ N}_2 + 1 \text{ O}_2) = 0$   $K = K(RT)^0$ 

 $K_p = K_c(RT)^0$   $K_c = K_p = 4.35 \times 10^{-31}$  because there is no net increase or decrease in the number of moles of gas in the course of the reaction.

17.81 a) Scenes B and D represent equilibrium.

b) C, A, 
$$B = D$$

c) [Y] = 
$$(4 \text{ spheres}) \left( \frac{0.025 \text{ mol}}{1 \text{ sphere}} \right) \left( \frac{1}{0.40 \text{ L}} \right) = 0.25 \text{ M}$$

[Z] = 
$$(8 \text{ spheres}) \left( \frac{0.025 \text{ mol}}{1 \text{ sphere}} \right) \left( \frac{1}{0.40 \text{ L}} \right) = 0.50 \text{ M}$$

$$K_{\rm c} = \frac{[Z]^2}{[Y]} = \frac{[0.50]^2}{[0.25]} = 1.0$$

17.82  $C_5H_{11}OH + CH_3COOH \leftrightarrows CH_3COOC_5H_{11} + H_2O$ 

> Removing water should help to increase the yield of banana oil. Both isopentyl alcohol and acetic acid are more soluble in water than isopentyl acetate. Thus, removing water will increase the concentration of both reactants and cause a shift in equilibrium toward the products.

17.83 The K is very small, thus the reaction will shift to the right to reach equilibrium. To simplify the calculations, assume the equilibrium shifts entirely to the left, and then a little material reacts to reach equilibrium. Shifting entirely to the left gives  $[H_2S] = 0.600$ , and  $[H_2] = [S_2] = 0$ .

	$H_2S(g)$	$\Rightarrow$ 2 H <sub>2</sub> (g)	+ $S_2(g)$
Initial	0.600  M	0 M	0 M
Change	-2x	+2x	$+\chi$
Equilibrium	0.600 - 2x	+2x	$+\chi$

$$K_{\rm c} = \frac{\left[{\rm H_2}\right]^2 \left[{\rm S_2}\right]}{\left[{\rm H_2S}\right]^2} = 9.0 \text{ x } 10^{-8}$$

$$\frac{[2x]^2[x]}{[0.600 - 2x]^2} = 9.0 \times 10^{-8}$$
 Assume 2x is small compared to 0.600 M.

$$\frac{\left[2x\right]^2 \left[x\right]}{\left[0.600\right]^2} = 9.0 \times 10^{-8}$$

 $x = 2.008 \times 10^{-3}$  (unrounded) assumption justified

$$[H_2S] = 0.600 - 2x = 0.600 - 2 (2.008 \times 10^{-3}) = 0.595984 = 0.596 M H_2S$$
  
 $[H_2] = 2x = 2 (2.008 \times 10^{-3}) = 4.016 \times 10^{-3} = 4.0 \times 10^{-3} M H_2$ 

$$[H_2] = 2x = 2 (2.008 \times 10^{-3}) = 4.016 \times 10^{-3} = 4.0 \times 10^{-3} M H_2$$

$$[S_2] = x = 2.008 \times 10^{-3} = 2.0 \times 10^{-3} M S_2$$

17.84 a) 
$$K_p = (P_{H,O})^{10} = 4.08 \times 10^{-25}$$
  
 $P_{H,O} = \sqrt[10]{4.08 \times 10^{-25}} = 3.6397 \times 10^{-3} = 3.64 \times 10^{-3} \text{ atm}$ 

- b) (1) Adding more Na<sub>2</sub>SO<sub>4</sub>(s) will decrease the ratio of hydrated form/anhydrous form merely because you are increasing the value of the denominator, not because the equilibrium shifts.
  - (2) Reducing the container size will increase the pressure (concentration) of the water vapor, which will shift the equilibrium to the reactant side. The ratio of hydrated form/anhydrous form will increase.
  - (3) Adding more water vapor will increase the concentration of the water vapor, which will shift the equilibrium to the reactant side. The ratio of hydrated form/anhydrous form will increase.
  - (4) Adding N<sub>2</sub> gas will not change the partial pressure of the water vapor, so the ratio of hydrated form/anhydrous form will not change.
- The reaction is:  $CO(g) + H_2O(g) \leftrightarrows CO_2(g) + H_2(g)$ 17.85
  - a) Set up a table with the initial CO and initial  $H_2 = 0.100 \text{ mol}/20.00 \text{ L} = 0.00500 \text{ M}$ .

[CO]<sub>equilibrium</sub> = 
$$0.00500 - x = 2.24 \times 10^{-3} M = [H_2O]$$
 (given in problem)

$$x = 0.00276 M = [CO_2] = [H_2]$$

$$K_c = \frac{[CO_2][H_2]}{[CO][H_2O]} = \frac{[0.00276][0.00276]}{[0.00224][0.00224]} = 1.518176 = 1.52$$

b) 
$$M_{\text{total}} = [\text{CO}] + [\text{H}_2\text{O}] + [\text{CO}_2] + [\text{H}_2] = (0.00224 \text{ M}) + (0.00224 \text{ M}) + (0.00276 \text{ M}) + (0.00276 \text{ M}) + (0.00276 \text{ M})$$
  
= 0.01000 M

$$P_{\text{total}} = n_{\text{total}} RT/V = \frac{\left(0.2000 \,\text{mol}\right) \left(0.08206 \frac{\text{L} \cdot \text{atm}}{\text{mol} \cdot \text{K}}\right) \left(\left(273 + 900.\right) \text{K}\right)}{\left(20.00 \,\text{L}\right)} = 0.9625638 = \textbf{0.9626} \,\text{atm}$$

- c) Initially, an equal number of moles must be added = 0.2000 mol CO
- d) Set up a table with the initial concentrations equal to the final concentrations from part (a), and then add 0.2000 mol CO/20.00 L = 0.01000 M to compensate for the added CO.

Initial 0.00224 M 0.00224 M 0.00276 M 0.00276 M

Added CO 0.01000 M

Change 
$$-x$$
  $-x$   $+x$   $+x$ 

Equilibrium  $0.01224 - x$   $0.00224 - x$   $0.00276 + x$   $0.00276 + x$ 

$$K_c = \frac{\left[\text{CO}_2\right]\left[\text{H}_2\right]}{\left[\text{CO}\right]\left[\text{H}_2\text{O}\right]} = \frac{\left[0.00276 + x\right]\left[0.00224 - x\right]}{\left[0.01224 - x\right]\left[0.00224 - x\right]} = 0.9625638$$

$$\frac{\left[7.6176 \times 10^{-6} + 5.52 \times 10^{-3} x + x^{2}\right]}{2.74176 \times 10^{-5} - 1.448 \times 10^{-2} x + x^{2}} = 0.9625638$$

$$7.6176 \times 10^{-6} + 5.52 \times 10^{-3} x + x^{2} = (0.9625638) (2.74176 \times 10^{-5} - 1.1448 \times 10^{-2} x + x^{2})$$

$$7.6176 \times 10^{-6} + 5.52 \times 10^{-3} x + x^{2} = 2.6391189 \times 10^{-5} - 1.3937923 \times 10^{-2} x + 0.9625638 x^{2}$$

$$0.0374362 x^{2} + 1.9457923 \times 10^{-2} x - 1.8773589 \times 10^{-5} = 0$$

$$a = 0.0374362 \quad b = 1.9457923 \times 10^{-2} \quad c = -1.8773589 \times 10^{-5}$$

$$x = \frac{-b \pm \sqrt{b^{2} - 4ac}}{2a}$$

$$x = \frac{-(1.9457923 \times 10^{-2}) \pm \sqrt{\left(1.9457923 \times 10^{-2}\right)^{2} - 4\left(0.0374362\right)\left(-1.8773589 \times 10^{-5}\right)}}{2\left(0.0374362\right)}$$

$$x = 9.6304567 \times 10^{-4} \text{ (unrounded)}$$

$$[CO] = 0.01224 - x = 0.01224 - (9.6304567 \times 10^{-4}) = 0.011276954 = 0.01128 M$$

17.86 
$$Q(g) \leftrightarrows R(g)$$
  $K = \frac{[R]}{[Q]}$ 

For Scene A at equilibrium:

$$K = \frac{[R]}{[Q]} = \frac{[2]}{[6]} = 0.33$$

For Scene B:

$$Q(g) \implies R(g)$$
Initial 10 2
$$\frac{\text{Change} -x}{\text{Equilibrium}} 10 - x 2 + x$$

$$0.33 = \frac{[2+x]}{[10-x]}$$

$$x = 0.977 = 1$$

$$Q = 10 - x = 10 - 1 = 9$$

$$R = 2 + x = 2 + 1 = 3$$