السير ، والتقدم والسبق إلى الله سبحانه انما هو بالهمم وصدق الرغبة والعزيمة ، فيتقدم صاحب الهمة ، مع سكونه ، صاحب العمل الكثير بمراحل) (١)

pole- zero placement method

geometric Interpretation pole / Zero location 8-

$$H(z)$$
 in Pole | $\overline{\text{Tero}}$ form $H(z) = \frac{b_0}{\alpha_0} \frac{M}{m} (1 - C_K \overline{z}^T)$
 $\overline{T} (1 - d_K \overline{z}^T)$
 $K = 0$

Stable system means that the ROC of H(Z) includes Z=1.

The frequency Response
$$H(\dot{e}^{i\omega}) = H(z) = \frac{b_0}{a_0} \frac{\chi^{ij}}{\chi^{ij}} (1 - c_k e^{-i\omega})$$

$$z = e^{i\omega} \frac{\chi^{ij}}{\chi^{ij}} (1 - c_k e^{-i\omega})$$

$$|H(\dot{\delta}^{\omega})| = \frac{|bol|}{|aol|} = \frac{|\dot{\delta}^{\omega}(M-N)|}{|\dot{\delta}^{\omega}(M-N)|}$$

Note the the magnitude | H(èw) | depends on term | e-al



| H(è) | = | bo |
$$\frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo | \frac{\pi}{|\pi|} (\frac{\partial w}{\partial w} - C_k) = | bo |$$

* when e close to a zero, | H(e)w) | is "small".

* when e close to a pole, | H(ein) | is "large"

Example 8- let
$$H(z) = \frac{1}{1-3z^{-1}}$$
, sketch $|W(\dot{e}^{i\omega})|$, Evaluate $|H(\dot{e}^{i\omega})|$ at $w=0$, $T/\sqrt{1-3z^{-1}}$, $T/\sqrt{1-3z^{-1}}$.

$$H(\overline{z}) = \frac{\overline{z}}{\overline{z} - 3}$$
, \overline{z} eros = o
 $\overline{z} - \frac{3}{4}$ Poles = $\frac{3}{4}$

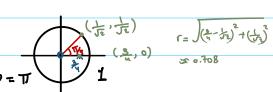
I at w =0



* magnitude from e to the poke

* the distance between 1 and 3 is 1/4

distance from w=o to Zero = 1



$$|H(\dot{z}^{i\omega})| = Distance from \dot{z}^{i\omega}$$
 to zero = $\frac{1}{z} = 52 = 1.4$
Distance from $\dot{z}^{i\omega}$ to poleo $\approx J_z$



$$|H(\dot{e^{i\omega}})| = \frac{1}{z_i} = \frac{4}{7} = 0.57$$

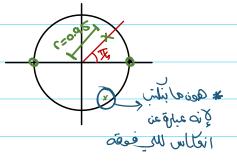
$$|H(\dot{e^{i\omega}})|$$

$$|H(\dot{e^{i\omega}})|$$

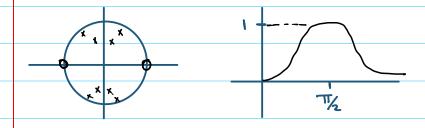
Example: $H(z) = \frac{1-\overline{z}^2}{(1-0.95e^{\frac{i\pi}{4}})(1-0.95e^{-\frac{i\pi}{4}})}$ Find $|H(e^{i\omega})|$ at w=0

Zeros - Z= FI

Poles -> Z = 0.95e , Z = 0.95e



Example 8- Infor filter charectaristics from poke | Zero.



filters design by poles zero placement

- when a Zero is placed at a given point on the Z-plane, the frequency Response will be Zero at the Corresponding point.
- A pole in the other hand produces a peak at the Corresponding frequency point.

* الأقطاد القريبة جدًا من الدائة الوحدية ب تنتج
قمم كبيرة في استجابة المهدد.

* الأمهنار القريبة أو العوجوة على الدائة الوحدية
تنتج انخفاضات أو قيمان في استجابة المهدد.

* Zeros به مكان الفلتر " يخنف " أو يقتل الإشارة في هذا البتحد تحديدًا * على الفلتر " يضخم " أو يقدّ على الفلتر " يضخم " أو يقدّ على البتد .

- العدف من المتيار أعان الأقطاب والأصفار ب نقير نصم فلن
 - كل فلتر بيختلف عن الناخي بوجود أمانن الأهمفار والأقطاب

A Narrowband Bandpass Filter "Resonator".

- In general: allows frequencies with in a Certain Range (band) to pass and Blocks frequencies and side this Range.
- A Marrow band Pass Filter: works the Same way, but the allowed Range is very narrow. in other words, instead of allowing a wide Range of frequencies, it selects a small slice of frequencies and blocks all the Rest.

Features:

- · passes only the Frequencies Very close to a Central frequency fo
- . Blocks frequencies for from fo, whether they are higher or lower.
- . Has high Selectivity due the The narrow band width.

On the Graph:

if you plot the Frequency Response s

- · you will see a peak of for (the Center Frequency).
- . the width at half of the peak (Band width) is very Small.
- . The shape books like a thin mountain or spike in the middle of the axis

In pole-zero placement

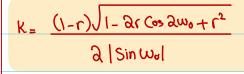
To design a Narrow BPF 3-

- place poles close to the unite circle at the desired frequency bo, so they boost only the Region around it.
- a place Zeros on or near the unit Circle at other locations to Cancel unwanted frequencies
- 3) the closer poles are to the unit Circle, the narrower and taller the peak becomes Resulling in a narrower band width filter.

كآم تلىن بافظتيم

$$H(\mathcal{Z}) = \frac{K(\mathcal{Z}_{-1})(\mathcal{Z}_{+1})}{(\mathcal{Z}_{-1}e^{\partial w_{o}})(\mathcal{Z}_{-1}e^{\partial w_{o}})} = \frac{K(\mathcal{Z}_{-1})}{(\mathcal{Z}_{-1}e^{\partial w_{o}})(\mathcal{Z}_{-1}e^{\partial w_{o}})}$$

يتحكم في عوف الطلفان bond حصل الملاقة المالة من القرينا عن فلتر فهي المثالة المالة ال



K: is the gain factor

Examples Design a Second_order band pass filter using the pole-Zero placement method and Satisfying the following specifications: Sampling Rate = 8000 Hz 3-dB band width = 200 HZ Passband Center frequency = 1000 Hz Zero gain at Zero and 4000 Hz. * eleas and aloss. I il أصلا عارفين إنه والع يلون في ١٥٥٥ عند ١٦,٥ Ans :- $F_5 = 8000$, $\Delta f = 200$, $f_0 = 1000$ $W = \frac{2Tf_0}{F_5} = \frac{2T(1000)}{48000} = T/y$ $K = (1-r) \sqrt{1-2r(0samo+r^2)} = (1-0.9214) \sqrt{1-(2)(0.9214)(0s72+(0.9214))}$ a Sin wo 2 Sin (T/4) K= (0.0786) (1.359) = 0.0755 0.3535

A narrowband Band Stop filter

-> Also, called Notch filter (Band Reject).

Definition: -

- . Notch filter: is a type of narrowband band Stop filter.
- . it Removes or greatly attenuates one specific frequency (or avery narrow Range around it) while allowing all other frequencies to pass almost unaffected.

Frequency Response:

- the frequency Response is flat (high gain) for most frequencies.
- At the notch frequency to . There is a sharp dip to very low gain (ideally Zero).
- This "V-shaped" dip is very narrow for a nallow band notch filter.

Design in Digital Filters:

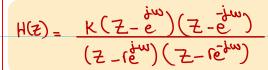
1. place Zeros on the unit Circle at the angle Corresponding to

- a) Place Poles just inside the unit Circle at the same angle
 - . the Zeros Completly Remove To.
 - . The poles Control the band width of the notch
 - . poles closer to the unit Circle -> narrower notch.
 - . Poles further away wider notch.

ج كورة النم بيرة Poles كمين بشيا -

م بن احما بدنا العلم عاياخن مل فقط فعشان نقلل

Zero's 11 in Tiguences de Zeros 11 mil -1



without poles!

يتحكم في عرف الطلاء الله Band حمد القريبا عن فلتر في الناق

معطيان في الامتحان المش حفظ "

$$K = \frac{1 - 2r(os w_0 + r^2)}{2|1 - (os w_0)|}$$

K: is the gain factor.

Examples Obtain the Pole-Zero placement method,

1 the transfer function of a sample digital Noteh filter

Notch Srequency 8-50HZ.

3dB width of the blotch = 75HZ = 10HZ

Sampling frequency: 500 Hz

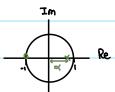
$$0 H(z) = \frac{K(z-iw)(z-iw)}{(z-reiw)(z-eiw)}, w_0 = \frac{2\pi(50)}{5} = \pi/5$$

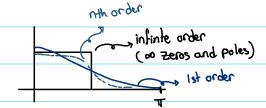
$$K = \frac{1 - 2(\cos w_0 + r^2)}{2|1 - \cos w_0|} = \frac{1 - 2(0.937)(\cos(\sqrt{s}) + (0.937)^2)}{2|1 - (\cos \sqrt{s})|} = \frac{4.08 \times 10^3}{1.2 \times 10^4} = 34$$

Example: Design a Second-order Notch Filter using pole-zero placement method :-Fs = 8000 HZ 3dB_BW = 100 HZ _ DF = 100 HZ من بك رصقه لعون السنفهاء Stop Band Center freq. To = 1500 HZ. ثم لم يتعرك بقوة $W = \frac{2\pi f_0}{F_S} = \frac{2\pi (1500)}{8000} = 1.178$ وصف رعبية لإملاع لنفس e Japles Neco $N(z) = \frac{K(z-e^{\frac{31.178}{1.178}})(z-e^{-\frac{11.178}{1.178}})}{(z-e^{\frac{31.178}{1.178}})(z-e^{-\frac{11.178}{1.178}})}$ Uik, vi6, vi6 av je € $C = 1 - \frac{100}{8000}$ IT = 0.9607 $K = \frac{1-2(0.9607)(05(1.178) + (0.9607)^2}{2} = -806.78$ 2/1-(05(1.178))

first order low pass filter

- · A wide Band filter.
- . Pass frequency Components from 0 to Fc (culaff frequency).
- Place a Zero on the unit Circle at Z = −1.
- place a pole on the Real axis and inside the unit Circle





$$H(z) = \frac{K(Z+1)}{(Z-\alpha)}$$

$$\alpha = \int_{-1-a\pi(\frac{F_c}{F_s})} \int_{-F_c} F_c < \frac{F_s}{4}$$

$$\pi_{-1-a\pi(\frac{F_c}{F_s})} \int_{-F_c} F_c > \frac{F_s}{4}$$

Example 8 Design a first order low pass lilter using the pole_Zero placement method and Satisfying the following specifications: Sampling Rate = 8000 Hz 3-dB cut of frequency = 100 Hz.

Zero gain at 4000 HZ

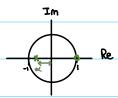
$$H(z) = \frac{K(Z+1)}{(Z-\alpha)} = \frac{0.039(Z+1)}{(Z-0.921)}$$

$$\frac{F_5}{4} = \frac{8000}{4} = 2000 \implies 100 < 2000 \implies 0$$

$$C = 1 - 2\pi \left[\frac{(00)}{8000} = 0.921 \right]$$
 $C = 1 - 0.921 = 0.039$

First Order High pass filter

- · A wide Band Filter.
- . Suppress frequency Components from 0 to Fc the Cut off frequency.
- . place a Zero on the unit circle at Z=1
- . place a pole on the Real axis and inside the unit circle.



$$H(z) = \frac{k(z-1)}{z+\alpha}$$

$$\alpha = \int_{-2\pi}^{\pi} \left(\frac{F_c}{F_s}\right), F_c < \left(\frac{F_s}{Y}\right)$$

$$\pi_{-1} - 2\pi \left(\frac{F_c}{F_s}\right), F_c > \frac{F_s}{Y}$$

Example: Design a first_order highpass filter using the pole Zero placement method and satisfying the following specifications &

Sampling Rate = 8000 Hz

3-dB whaff frequency = 3800 Hz

Zero gain all Zero HZ.

$$K = \frac{1 - 0.842}{2} = 6.078$$
 .. $K = \frac{1 - 0.842}{2}$