

(L1)

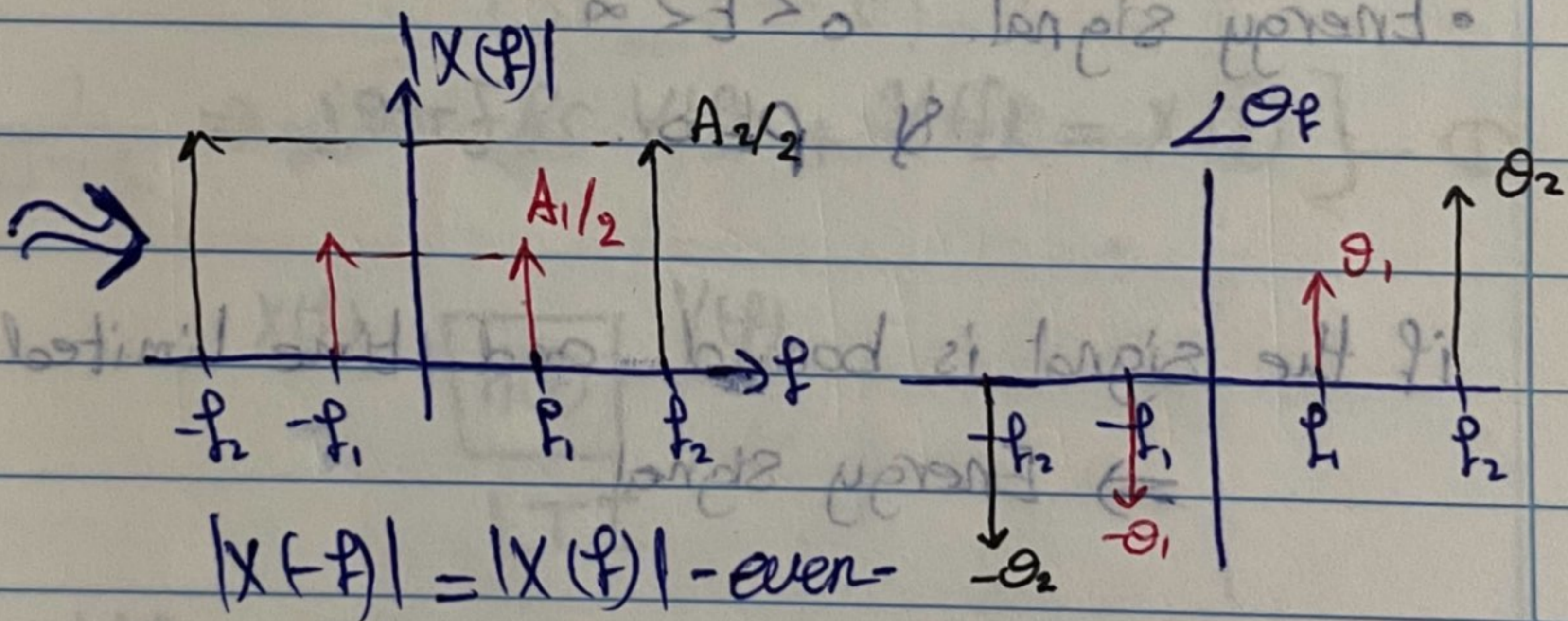
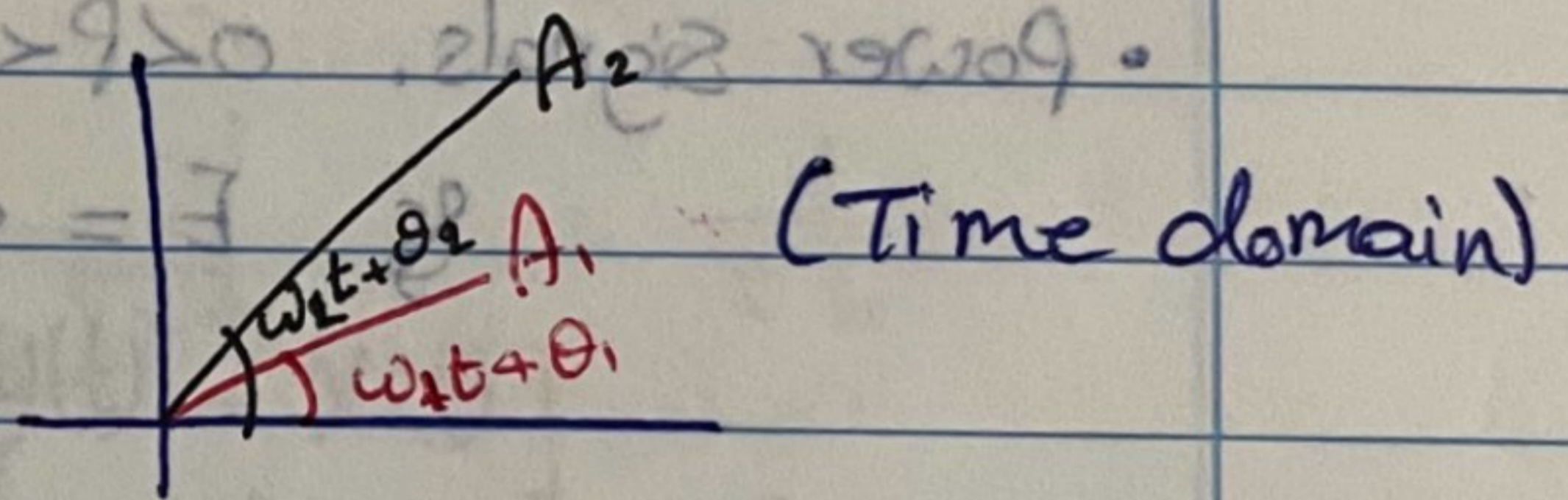
- signals part -

Review.

• signals → function $\begin{cases} \rightarrow 1D \\ \rightarrow 2D \\ \rightarrow 3D. \end{cases}$

• Types of signals $\begin{cases} \rightarrow \text{step function} \\ \rightarrow \text{ramp function} \\ \rightarrow \text{pulse function} \\ \rightarrow \text{impulse function} \end{cases}$

$$X(t) = \text{Re}\{Ae^{j\theta} e^{j\omega t}\} = A \cos(\omega t + \theta)$$



$|X(-f)| = |X(f)|$ - even -

$\angle \phi = -\angle \phi$ - odd -

• To evaluate power.

In Time domain:- $X(t) = A \cos(\omega t + \theta)$

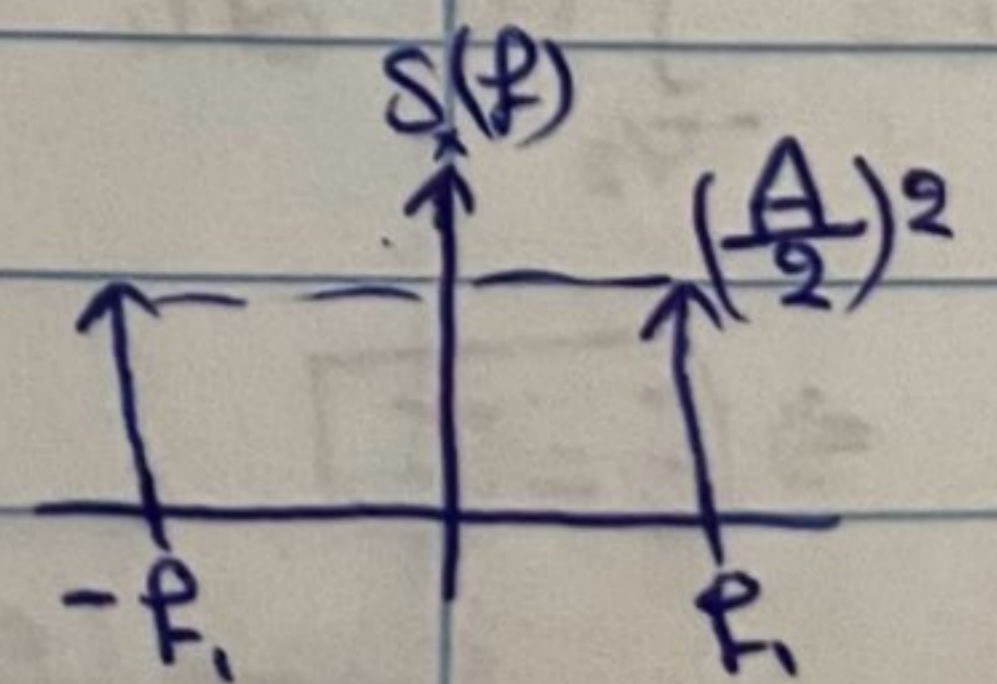
$$P_{avg} = \frac{A^2}{2}$$

In freq domain:-

- power spectral density (PSD).

$$S_x(f) = \left(\frac{A}{2}\right)^2 \delta(f - f_1) + \left(\frac{A}{2}\right)^2 \delta(f + f_1)$$

$$P = \int \left(\frac{A}{2}\right)^2 \rightarrow \boxed{P = \frac{A^2}{2}}$$



Power & Energy Signals

$$E = \int_{T_0}^{\infty} |X(t)|^2 dt$$

$$P = \lim_{T_0 \rightarrow \infty} \frac{1}{2T_0} \int_{-T_0}^{T_0} |X(t)|^2 dt$$

$$P = \lim_{T_0 \rightarrow \infty} \frac{1}{T_0} \int_0^{T_0} |X(t)|^2 dt$$

$$RMS = \sqrt{P_{avg}}$$

• Power signals. $0 < P < \infty$

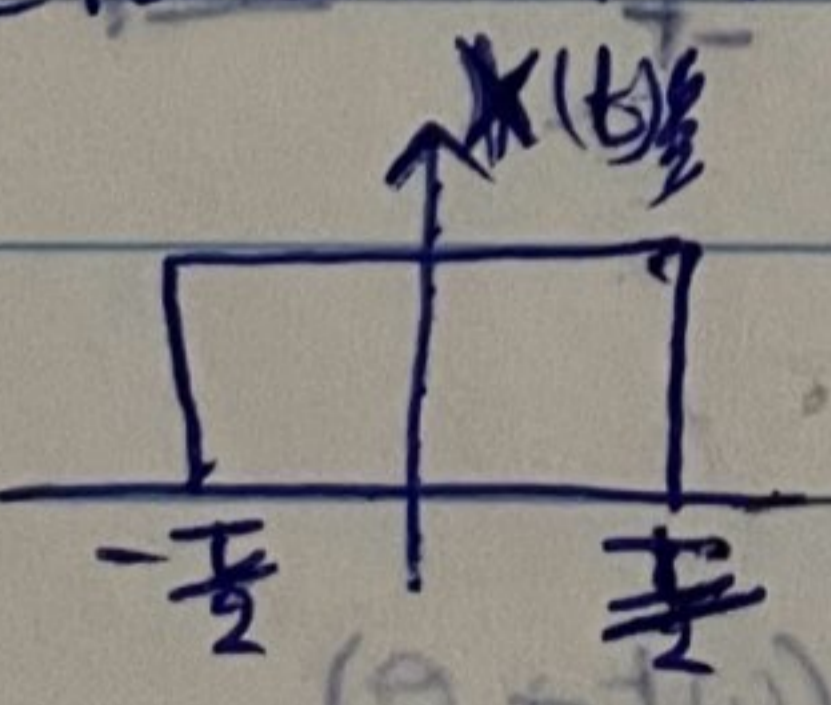
& $E = \infty$

• Energy signal. $0 < E < \infty$

& $P = 0$

if the signal is bound and time limited
 \Rightarrow Energy signal.

check if $X(t)$ is power or energy signal.



$$P = \lim_{T_0 \rightarrow \infty} \frac{1}{2T_0} \int_{-T_0}^{T_0} |X(t)|^2 dt$$

$$E = \int_{-T/2}^{T/2} (1)^2 dt$$

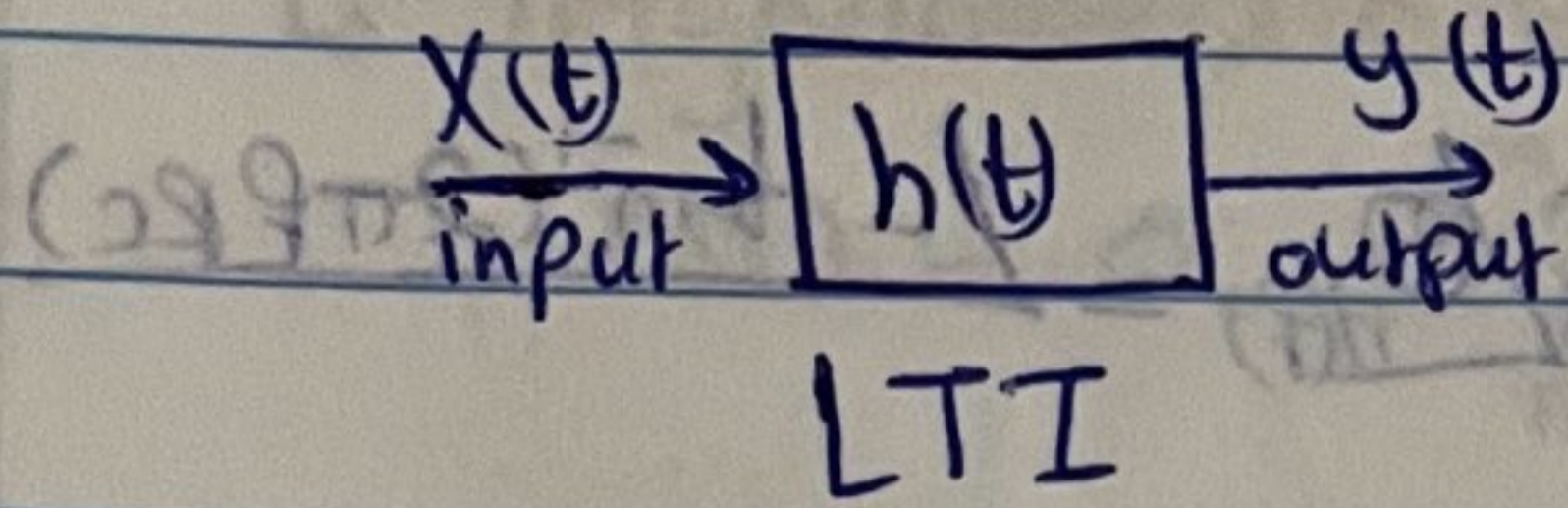
$$\Rightarrow E = T$$

\Rightarrow Energy signal.

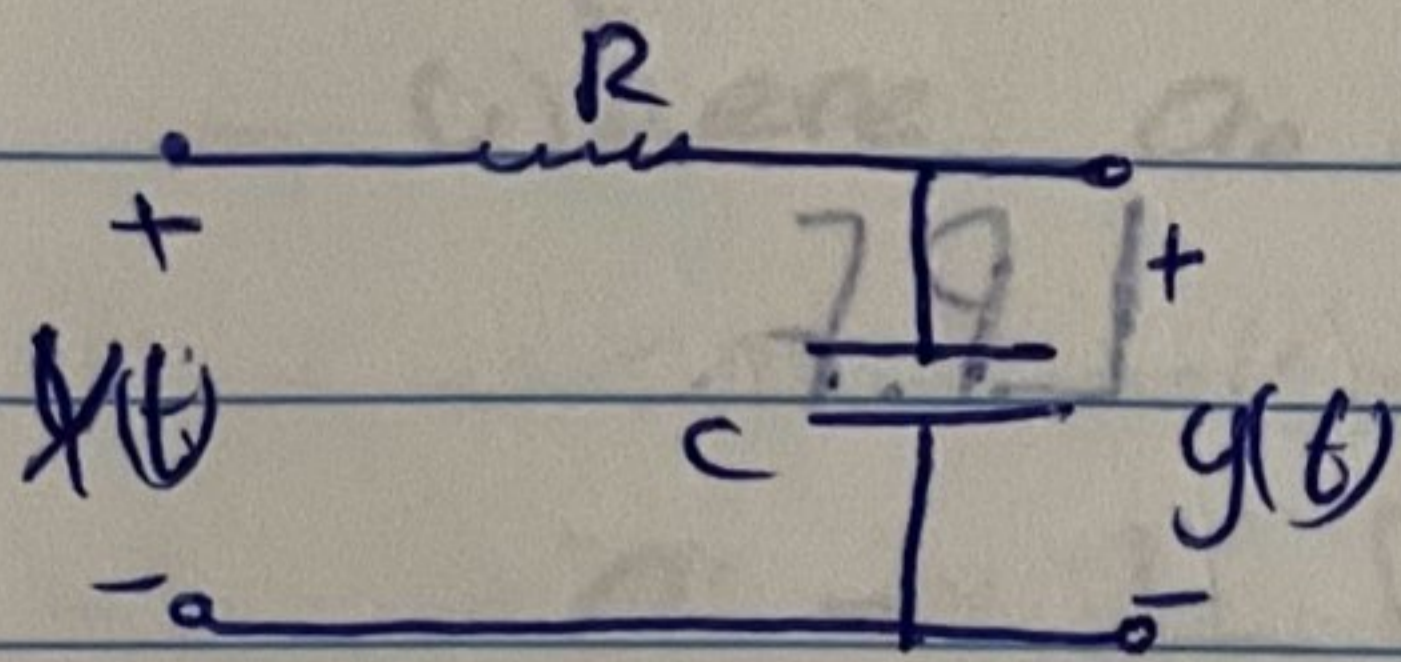
$$= \lim_{T_0 \rightarrow \infty} \frac{1}{2T_0} \left[\int_{-T_0}^{-T/2} (0)^2 dt + \int_{-T/2}^{T/2} (1)^2 dt + \int_{T/2}^{T_0} (0)^2 dt \right]$$

$\Rightarrow P = 0$

• Systems.



$$y(t) = x(t) * h(t)$$



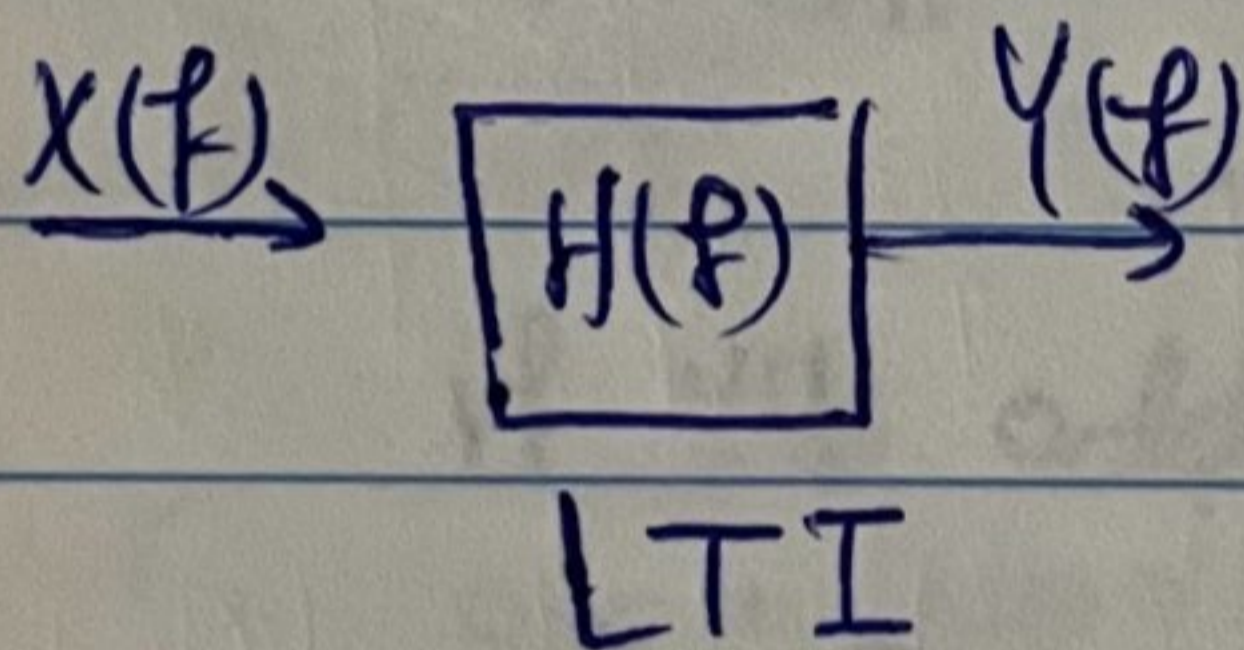
$$RC \frac{dy(t)}{dt} + y(t) = x(t)$$

$$\Rightarrow y(t) = \frac{1}{RC} e^{-t/RC} u(t)$$

In freq. domain.

$$\mathcal{F} \left[RC \frac{dy(t)}{dt} + y(t) = x(t) \right]$$

$$\Rightarrow j2\pi f RC Y(f) + Y(f) = X(f) \quad \text{--- (1)}$$



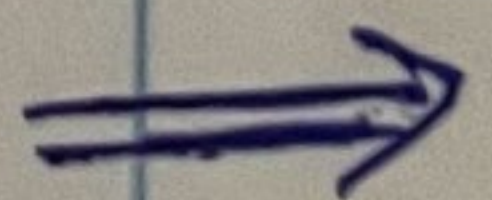
$$Y(f) = X(f)H(f) \Rightarrow H(f) = \frac{Y(f)}{X(f)}$$

From Eq (1) :-

$$[1 + j2\pi f RC] Y(f) = X(f)$$

$$\Rightarrow H(f) = \frac{1}{1 + j2\pi f RC}$$

$$= \frac{1 \angle 0}{\sqrt{1^2 + (2\pi f RC)^2} \angle \tan^{-1}(2\pi f RC)}$$

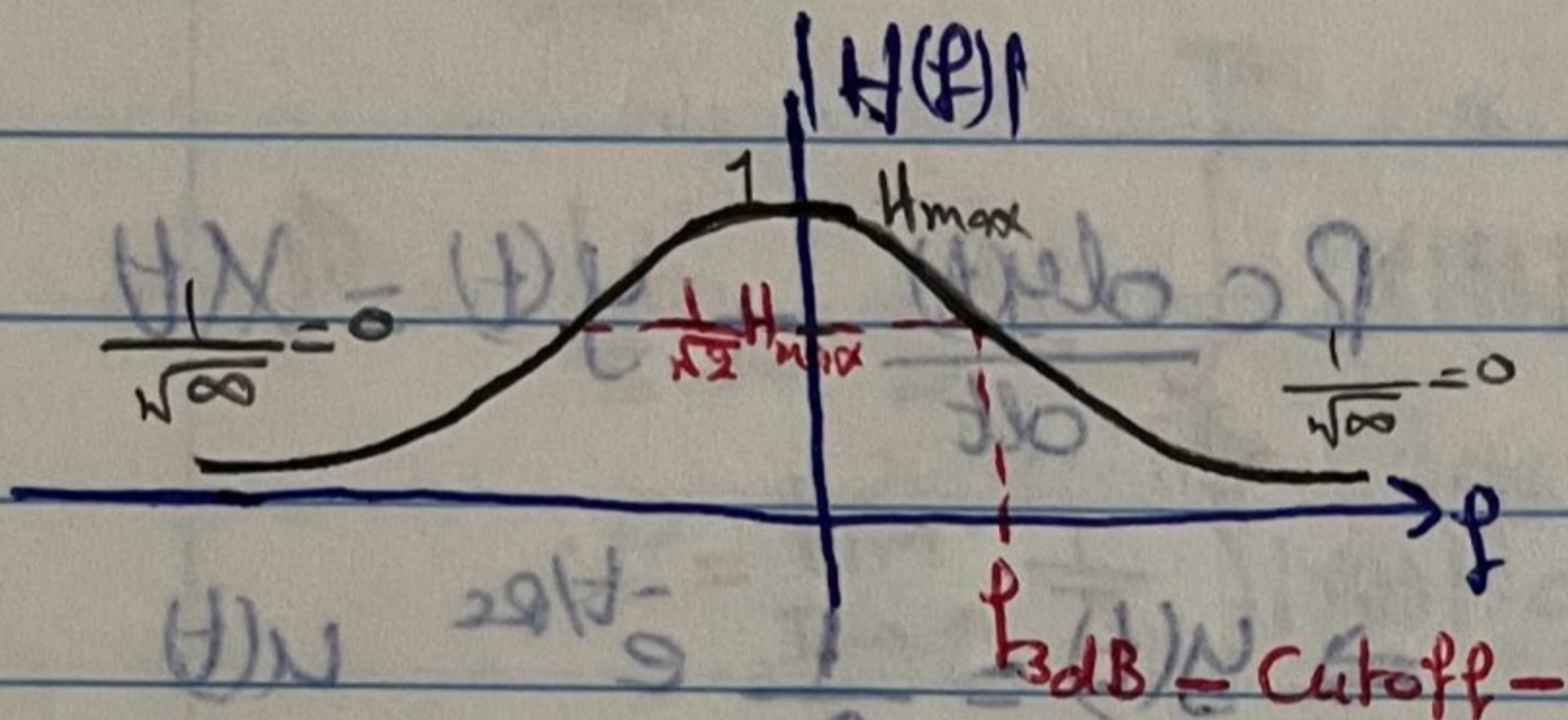




$$H(f) = |H(f)| \angle \theta_{H(f)}$$

$$|H(f)| = \frac{1}{\sqrt{1 + (2\pi f R_c)^2}}$$

$$\angle \theta_{H(f)} = -\tan^{-1}(2\pi f R_c)$$



L.P.F.

$$\frac{1}{\sqrt{2}} = \frac{1}{\sqrt{1 + (2\pi f_{3dB} R_c)^2}}$$

$$2 = 1 + (2\pi f_{3dB} R_c)^2$$

$$1 = 2\pi f_{3dB} R_c \Rightarrow f_{3dB} = \frac{1}{2\pi R_c}$$

(L 2)

≡ Fourier Series

↳ Trigonometric Fourier Series

$$X(t) = a_0 + \sum_{n=1}^{\infty} a_n \cos(n\omega_0 t) + \sum_{n=1}^{\infty} b_n \sin(n\omega_0 t)$$

where a_0, a_n, b_n Trigonometric Coefficients Fourier Series.

$$a_0 = \frac{1}{T_0} \int_{T_0} X(t) dt = \text{average Value or DC Value}$$

$$a_n = \frac{2}{T_0} \int_{T_0} X(t) \cos(n\omega_0 t) dt$$

$$b_n = \frac{2}{T_0} \int_{T_0} X(t) \sin(n\omega_0 t) dt$$

Note: if $X(t)$ even function.

$$\Rightarrow b_n = 0, a_n \checkmark$$

if $X(t)$ odd function.

$$\Rightarrow a_n = 0, b_n \checkmark$$

→ $X(t) = \sum_{n=-\infty}^{\infty} X_n e^{jn\omega_0 t}$ - Complex Exponential Fourier Series
where X_n : Complex Exponential Coefficient Fourier Series.

$$X_n = \frac{1}{T_0} \int_{T_0} X(t) e^{-jn\omega_0 t} dt$$

Note 2 For Complex Exponential Fourier Series

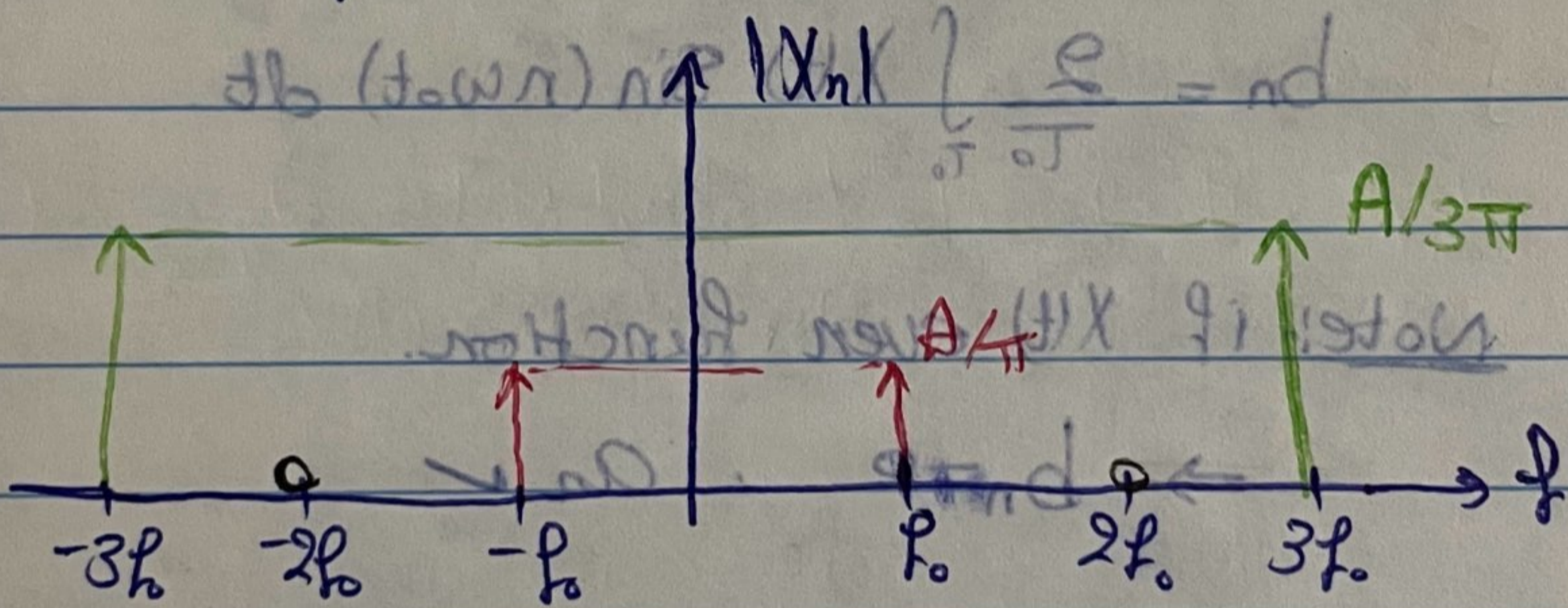
• if $X(t)$ even $\Rightarrow X_n = \text{real}$

• if $X(t)$ odd $\Rightarrow X_n = \text{Imaginary}$

In general

$$X_n = \begin{cases} \frac{1}{2}(a_n - jb_n), & n > 0 \\ \frac{1}{2}(a_n + jb_n), & n < 0 \\ a_0, & n = 0 \end{cases}$$

Line Spectra



$$X_n = \begin{cases} \frac{A}{j\pi n}, & n(\text{odd}), n > 0 \\ -\frac{A}{j\pi n}, & n(\text{odd}), n < 0 \\ 0, & n = 0 \end{cases}$$

≡ Parseval's Theorem.

$$P_{avg} = \sum_{n=-\infty}^{\infty} |X_n|^2$$

Since $|X_{-n}| = |X_n|$

$$\Rightarrow P_{avg} = X_0^2 + 2 \sum_{n=1}^{\infty} |X_n|^2$$

- We can write expression for PSD.

$$S_x(f) = \sum_{n=-\infty}^{\infty} |X_n|^2 \delta(f - nf_0)$$

≡ Fourier Transform

$$X(f) = \int_{-\infty}^{\infty} x(t) e^{-j2\pi ft} dt$$

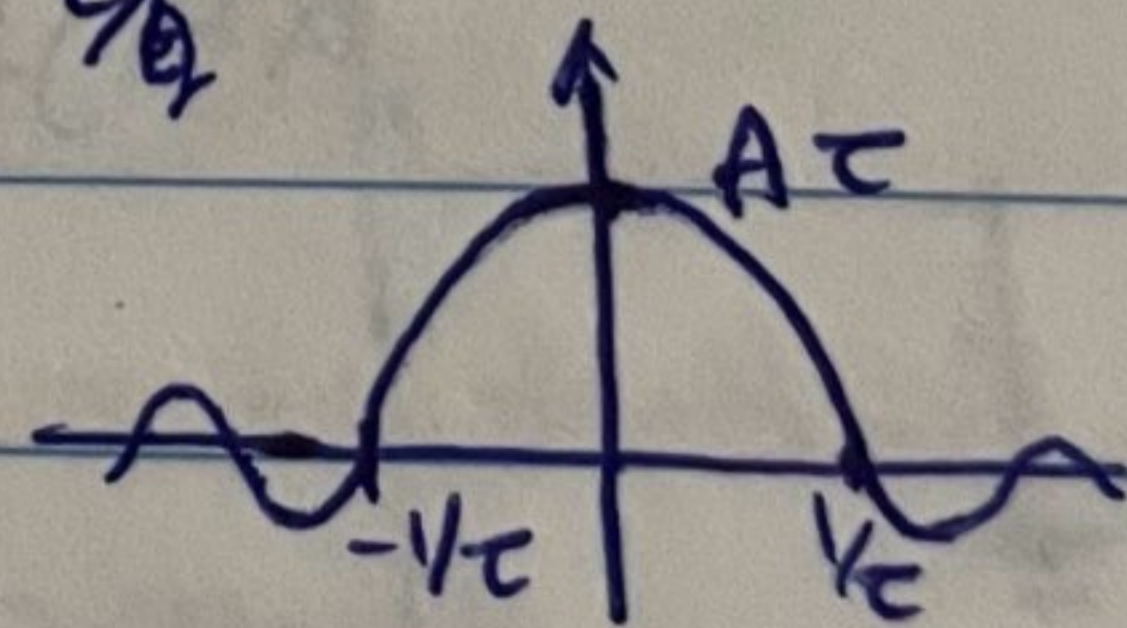
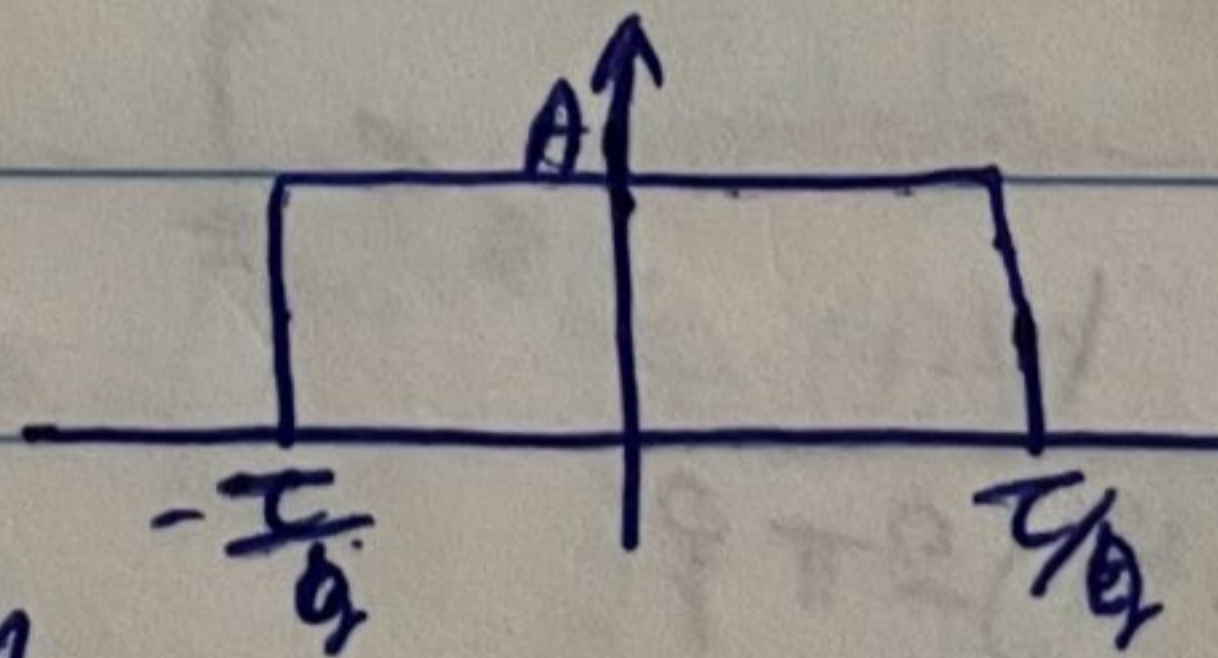
$$x(t) = \int_{-\infty}^{\infty} X(f) e^{j2\pi ft} df$$

Time domain.

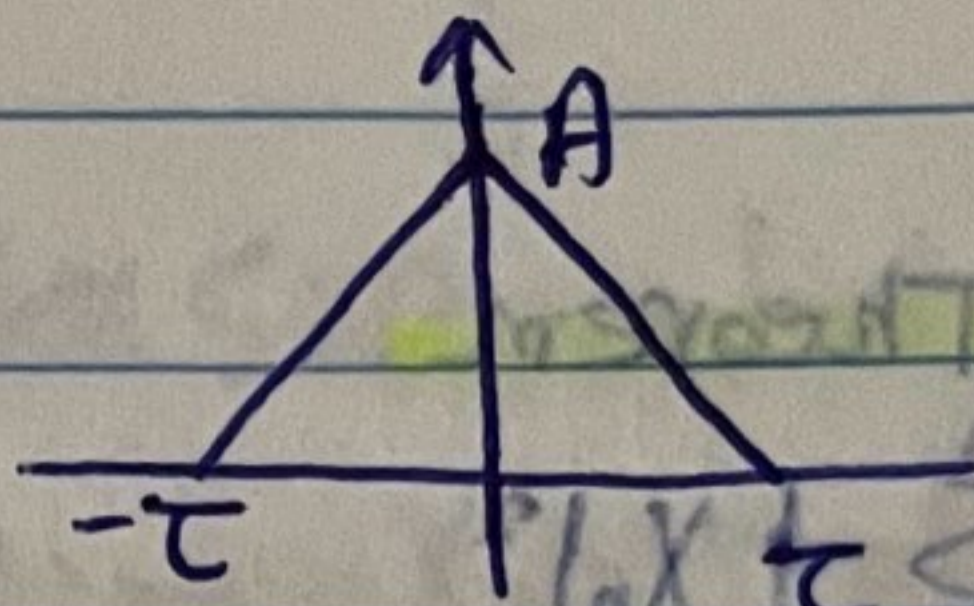
$$\square x(t) = A \Pi\left(\frac{t}{\tau}\right)$$

↳ Freq domain.

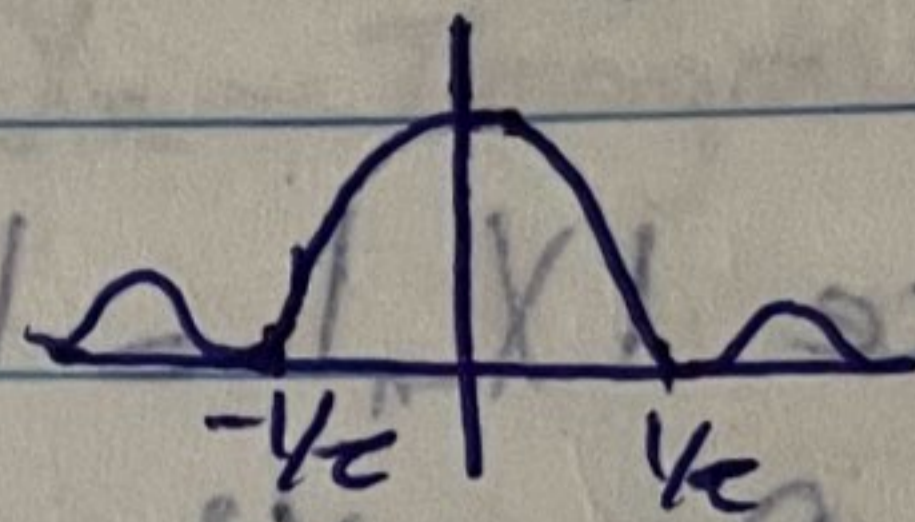
$$X(f) = A\tau \text{sinc}(\tau f)$$



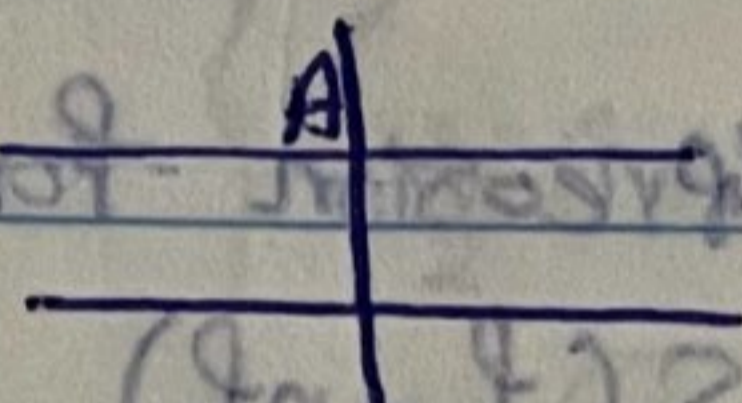
(Time domain) $X_2(t) = A \wedge \left(\frac{t}{\tau}\right)$



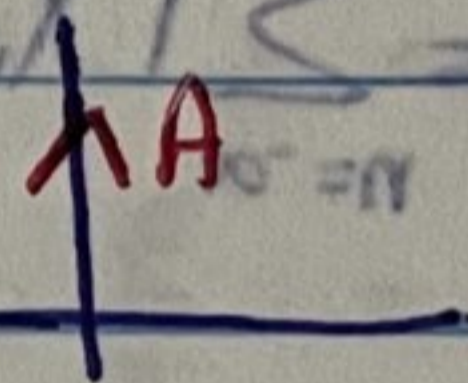
(Freq. domain) $X_2(f) = A\tau \text{sinc}^2(\tau f)$



(Time domain) $X_3(t) = A$



(Freq. domain) $X_3(f) = A \delta(f)$



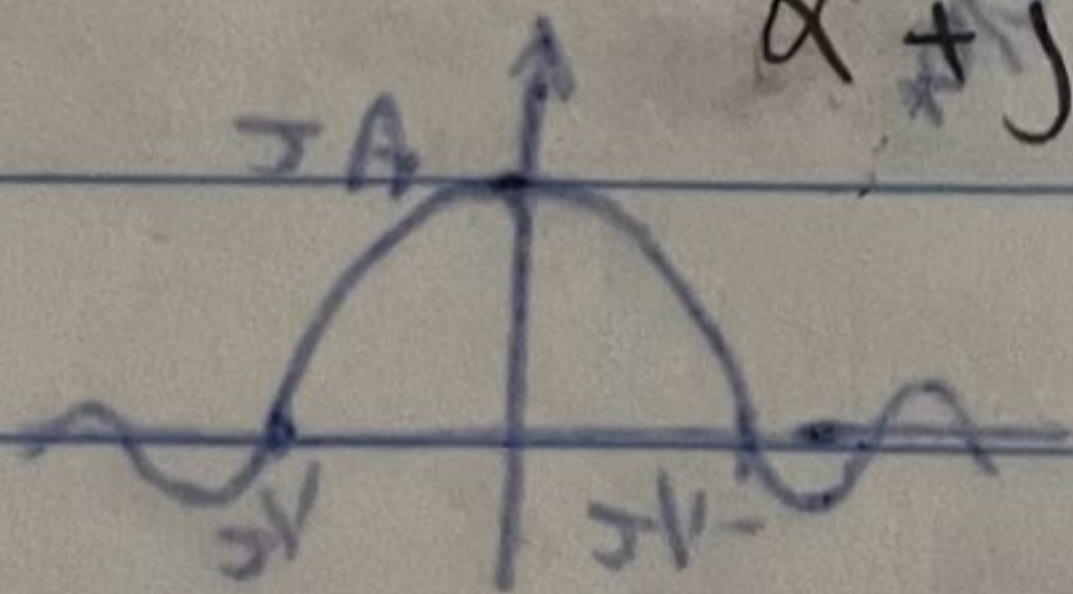
Example Evaluate FT of the following signal.

$X(t) = e^{-\alpha t} u(t)$

$$X(f) = \int_{-\infty}^{\infty} x(t) e^{-j2\pi ft} dt$$

$$= \int_0^{\infty} e^{-\alpha t} e^{-j2\pi ft} dt = \int_0^{\infty} e^{-(\alpha + j2\pi f)t} dt$$

$$= \frac{1}{\alpha + j2\pi f}$$



FT Theorems

1- Linearity:-

$$\begin{aligned} \mathcal{F}[X_1(t) + X_2(t)] &= \mathcal{F}[X_1(t)] + \mathcal{F}[X_2(t)] \\ &= X_1(f) + X_2(f) \end{aligned}$$

EX Evaluate FT. for the following signal.

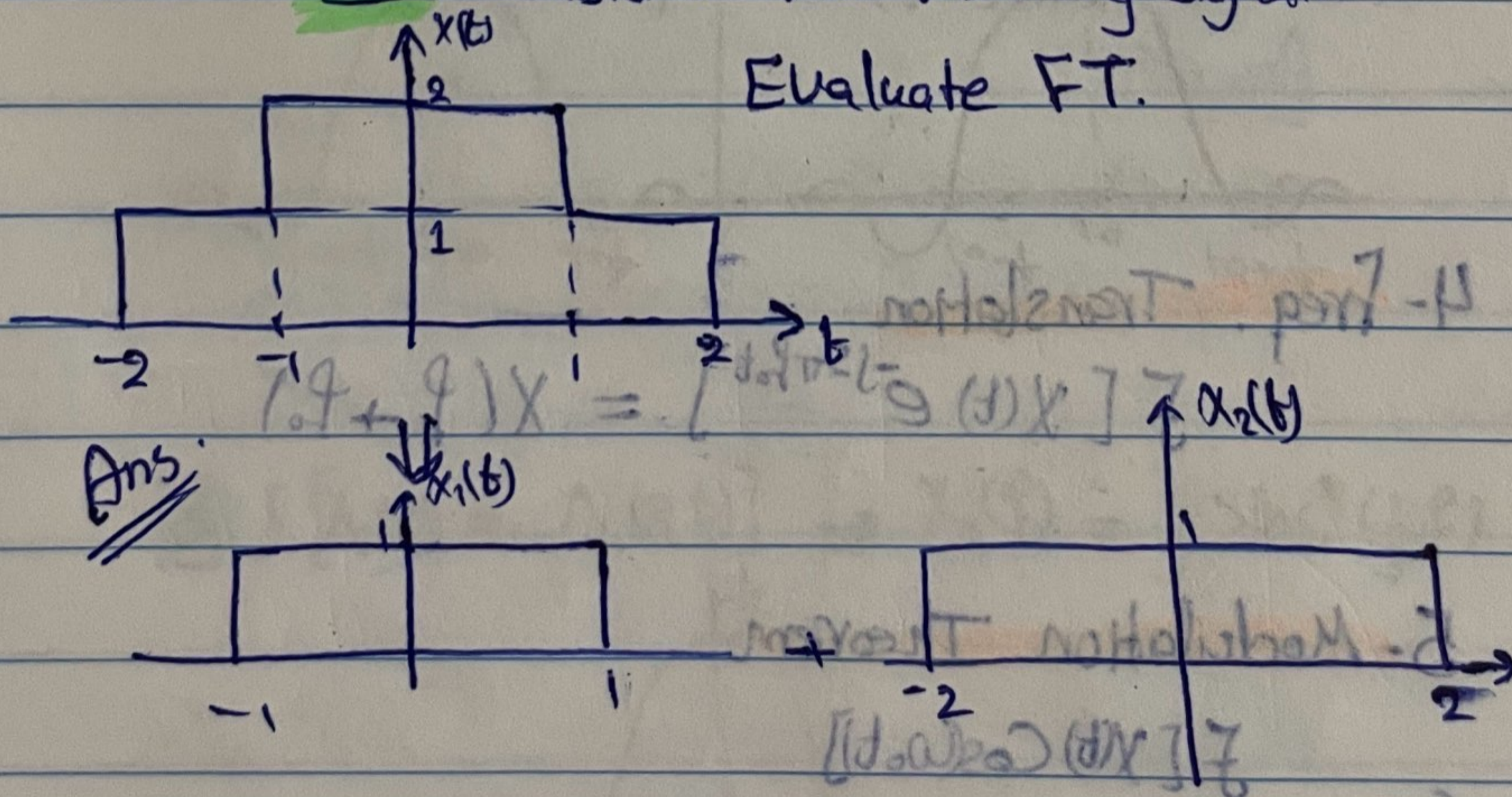
$$\begin{aligned} X(t) &= \mathcal{F}\{\pi(t) + \Lambda(t)\} \\ &= \mathcal{F}\{\pi(t)\} + \mathcal{F}\{\Lambda(t)\} \\ &= \text{sinc}(f) + \text{sinc}^2(f) \end{aligned}$$

2- Scaling:-

$$\mathcal{F}[X(at)] = \frac{1}{|a|} X\left(\frac{f}{a}\right)$$

EX Consider the following signal.

Evaluate FT.



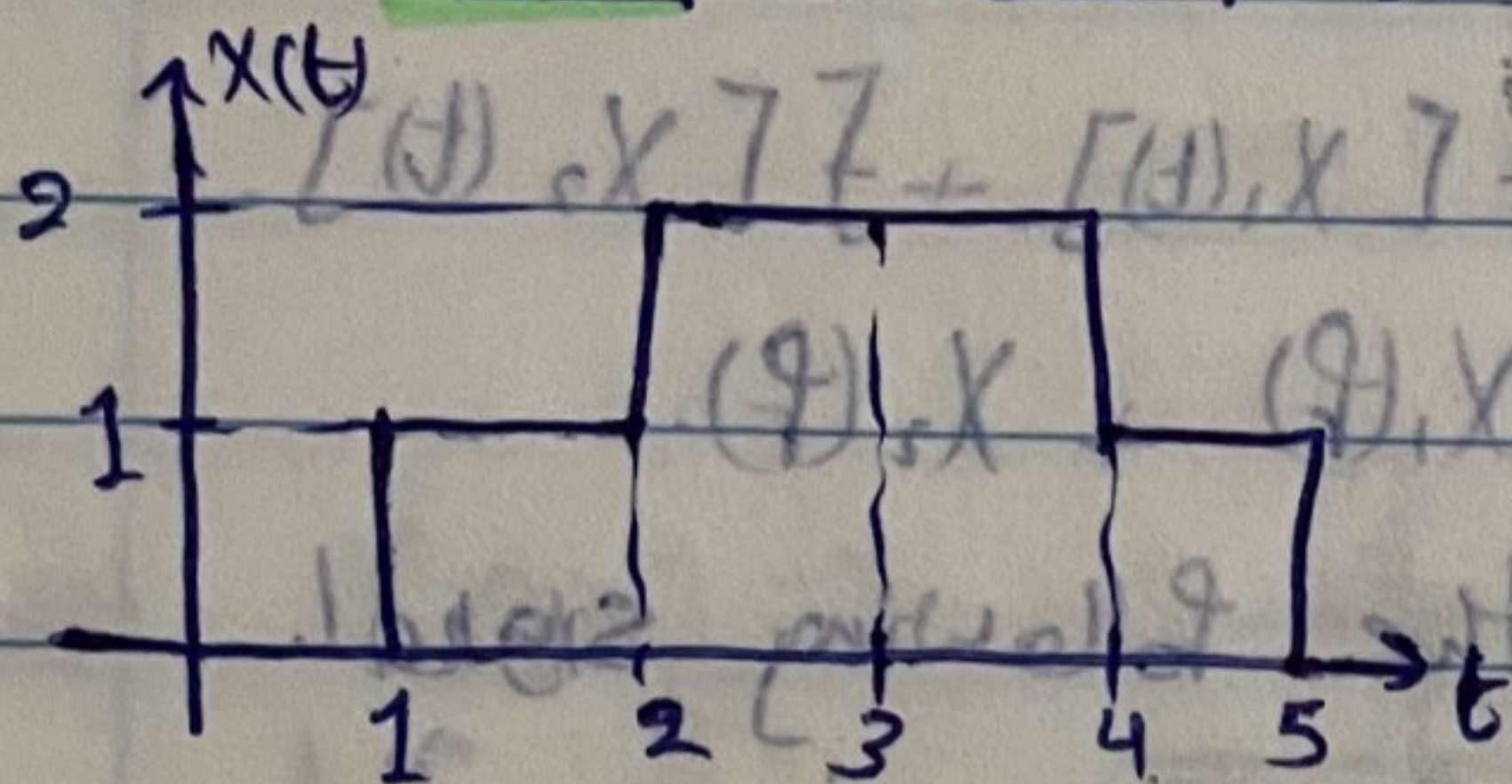
$$X(t) = X_1(t) + X_2(t)$$

$$= \mathcal{F}\left[\pi\left(\frac{t}{2}\right) + \pi\left(\frac{t}{4}\right)\right] \Rightarrow 2 \text{sinc}(2f) + 4 \text{sinc}(4f)$$

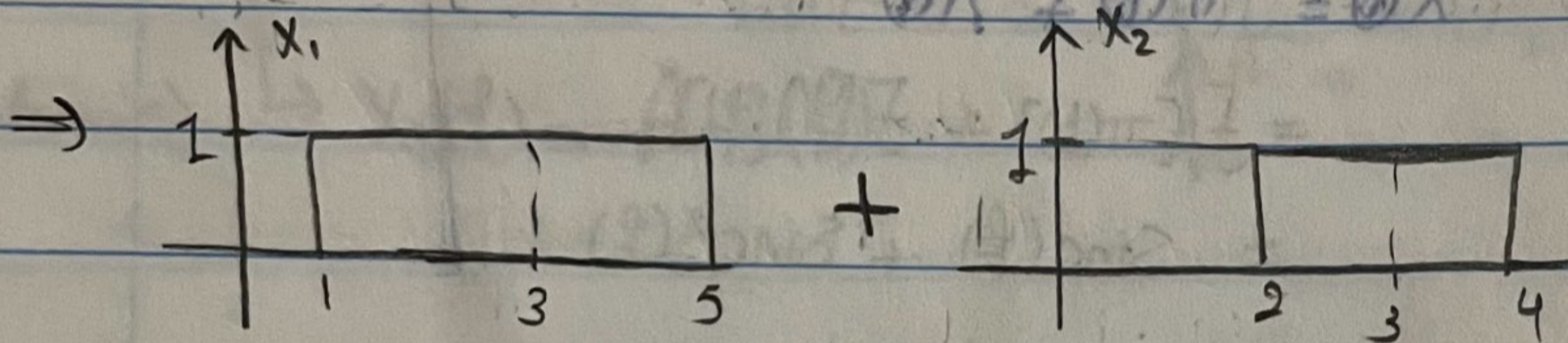
3- Time-delay

$$F[X(t-t_0)] = X(f) e^{-j2\pi f t_0}$$

EX) Consider the following signal.



Evaluate F.T.



$$X(t) = X_1(t) + X_2(t)$$

$$= \int \left[\Pi\left(\frac{t-3}{4}\right) + \Pi\left(\frac{t-3}{2}\right) \right]$$

$$X(f) = 4 \text{sinc}(4f) e^{-j6\pi f} + 2 \text{sinc}(2f) e^{-j6\pi f}$$

4- Freq. Translation

$$F[X(t) e^{-j2\pi f_0 t}] = X(f + f_0)$$

5- Modulation Theorem

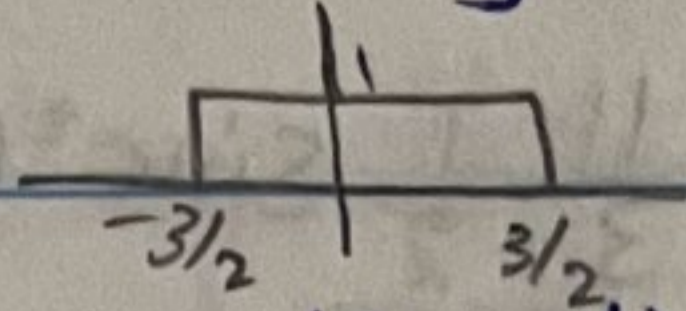
$$F[X(t) \cos(\omega_0 t)]$$

$$\begin{aligned} \left(\text{Since: } \cos(\omega_0 t) = \frac{e^{j\omega_0 t} + e^{-j\omega_0 t}}{2} \right) \\ F[X(t) \left(\frac{e^{j\omega_0 t} + e^{-j\omega_0 t}}{2} \right)] &= \frac{1}{2} F[X(t) e^{j\omega_0 t}] + \frac{1}{2} F[X(t) e^{-j\omega_0 t}] \\ &= \frac{1}{2} X(f - f_0) + \frac{1}{2} X(f + f_0) \end{aligned}$$

(3)

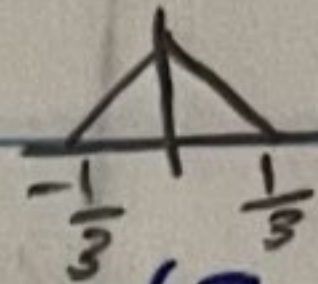
EX1 Consider the following signals.

1. $X_1(t) = \pi\left(\frac{t}{3}\right)$



2. $X_2(t) = \pi\left(\frac{t}{3}\right) \cos(20\pi t)$

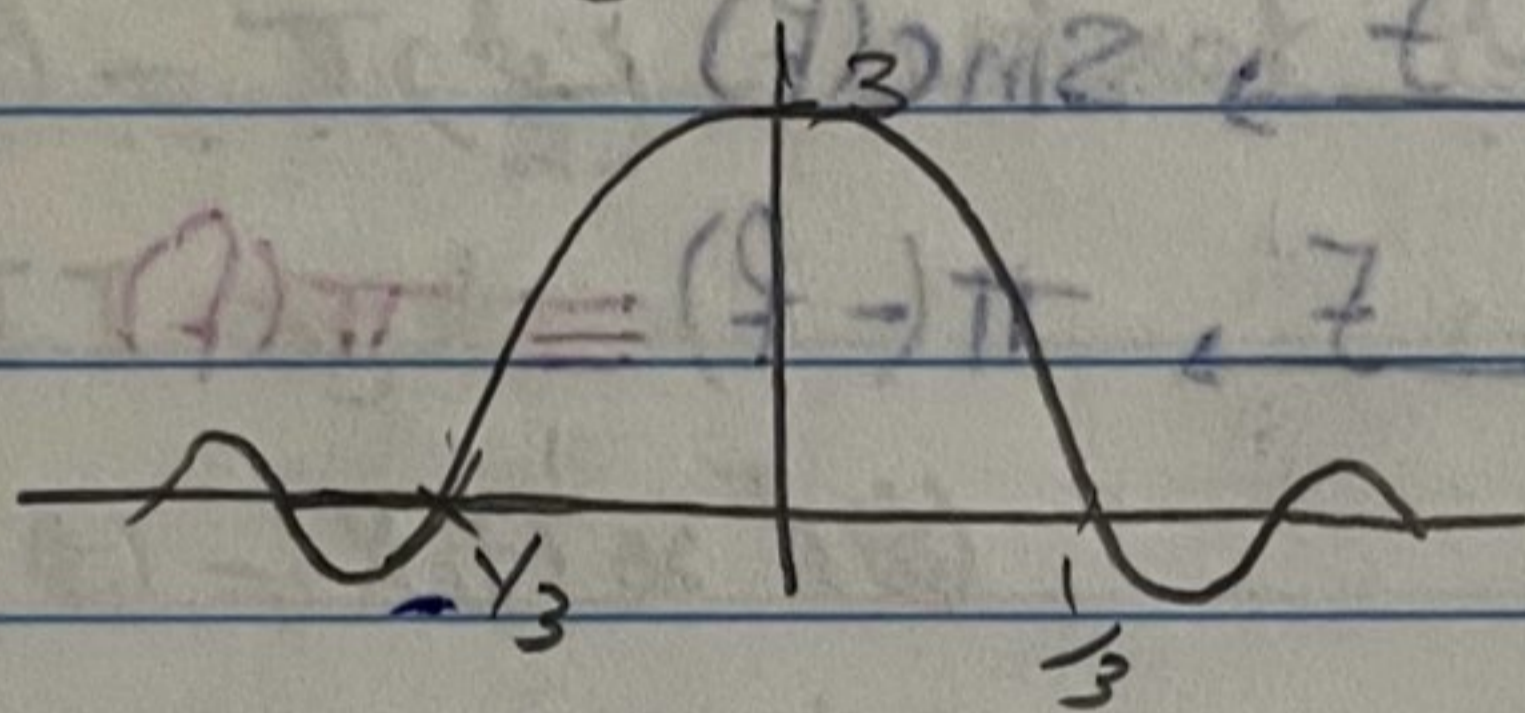
3. $X_3(t) = \wedge(3t)$



4. $X_4(t) = \wedge(3t) \cos(80\pi t)$

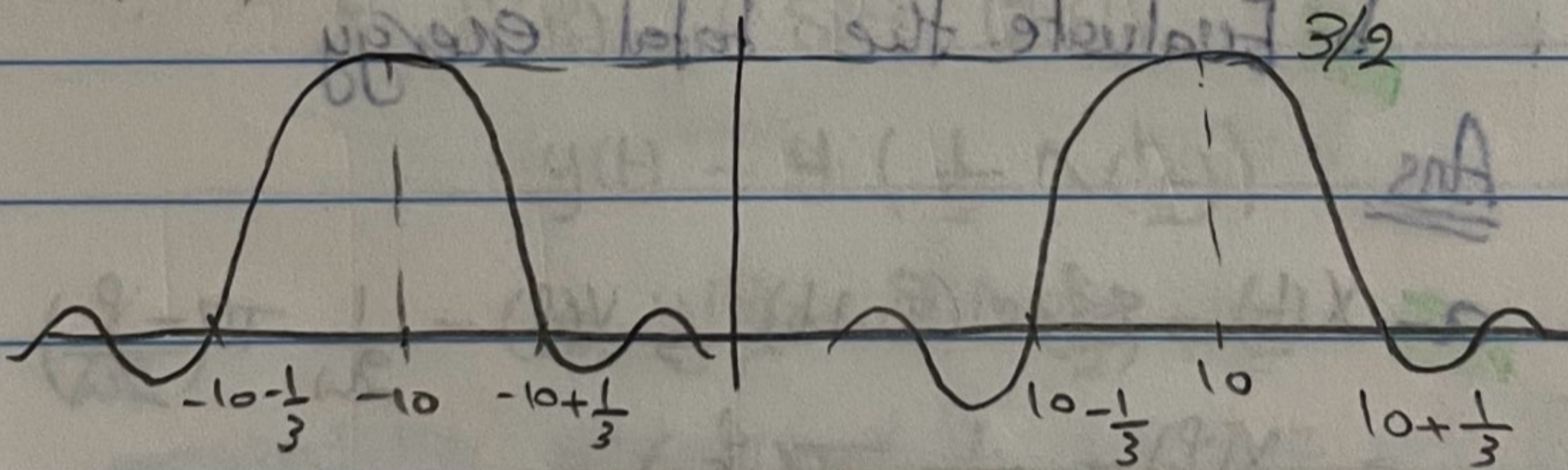
Evaluate and plot FT for each signals.

1] $\mathcal{F}\left[X_1(t) = \pi\left(\frac{t}{3}\right)\right] \Rightarrow X_1(f) = 3 \text{sinc}(3f)$

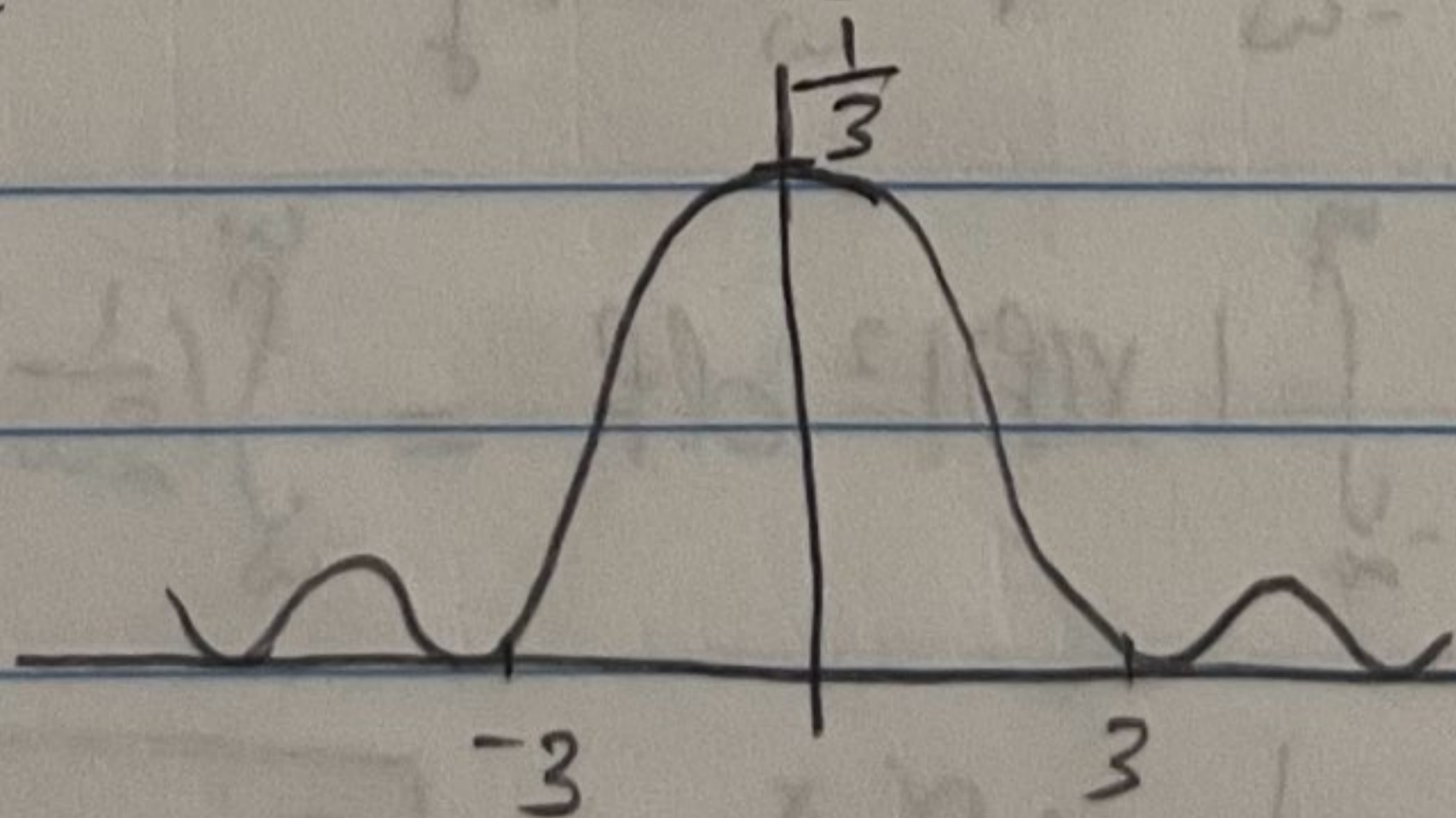


2] $\mathcal{F}\left[X_2(t) = \pi\left(\frac{t}{3}\right) \cos(20\pi t)\right]$

$\rightarrow X_2(f) = \frac{3}{2} \text{sinc}\left(3f - 10\right) + \frac{3}{2} \text{sinc}\left(3f + 10\right)$

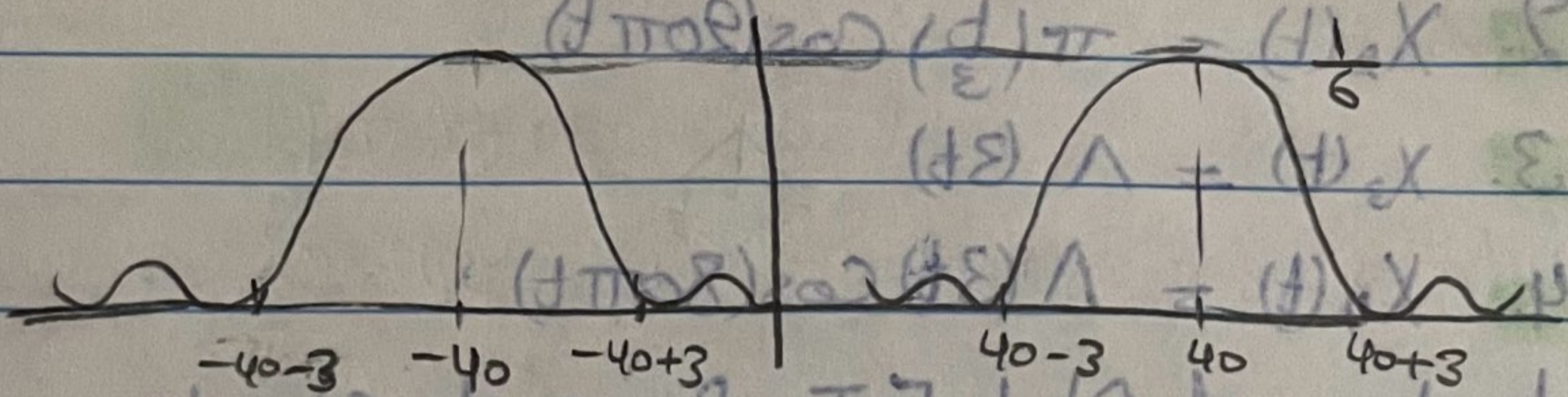


3] $\mathcal{F}\left[X_3(t) = \wedge(3t)\right] \rightarrow X_3(f) = \frac{1}{3} \text{sinc}^2\left(\frac{1}{3}f\right)$



$$[4] f[X_u(t) = A(Bt) \cos(80\pi t)]$$

$$X_u(f) = \frac{1}{3} \cdot \frac{1}{2} \text{sinc}^2\left(\frac{1}{3}(f-40)\right) + \frac{1}{3} \cdot \frac{1}{2} \text{sinc}^2\left(\frac{1}{3}(f+40)\right)$$



6- Duality Theorem.

$$X(t) \xrightarrow{F} \text{sinc}(f)$$

$$\text{sinc}(t) \xrightarrow{F} \pi(-f) \equiv \pi(f) \text{ - even -}$$

EX Consider the following signal.

$$1. X(t) = \text{sinc}(2\omega t)$$

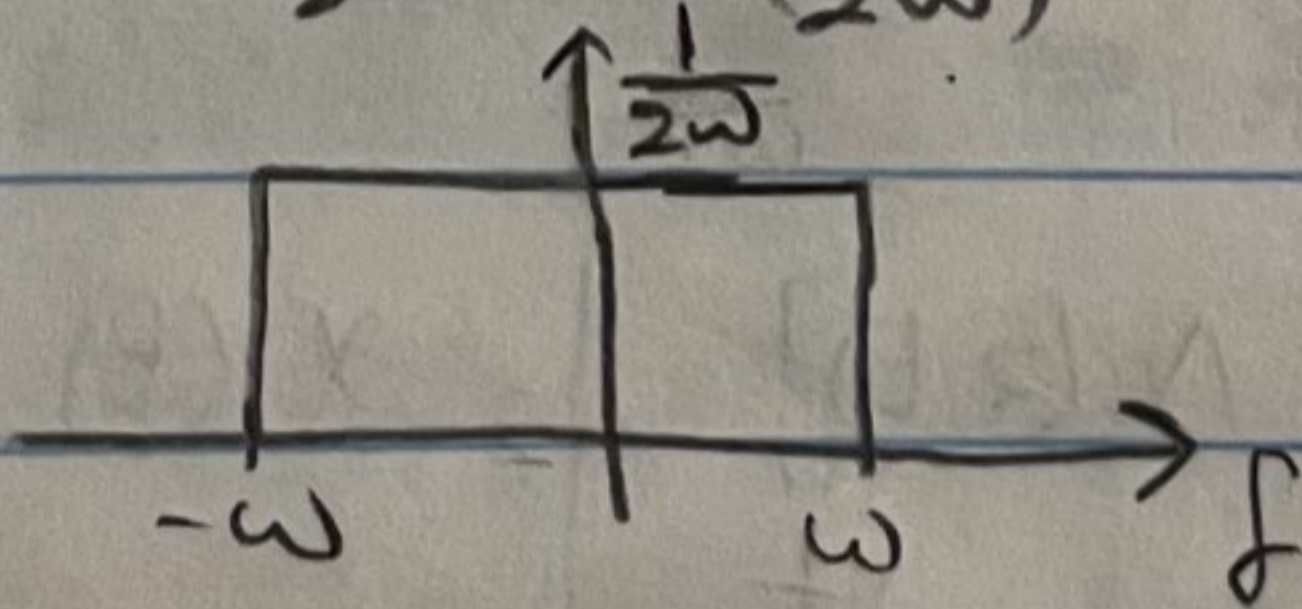
a- Evaluate and plot FT $X(f)$

b- Evaluate the total energy.

Ans.

$$a- X(t) = \text{sinc}(2\omega t) \rightarrow X(f) = \frac{1}{2\omega} \pi\left(\frac{f}{2\omega}\right)$$

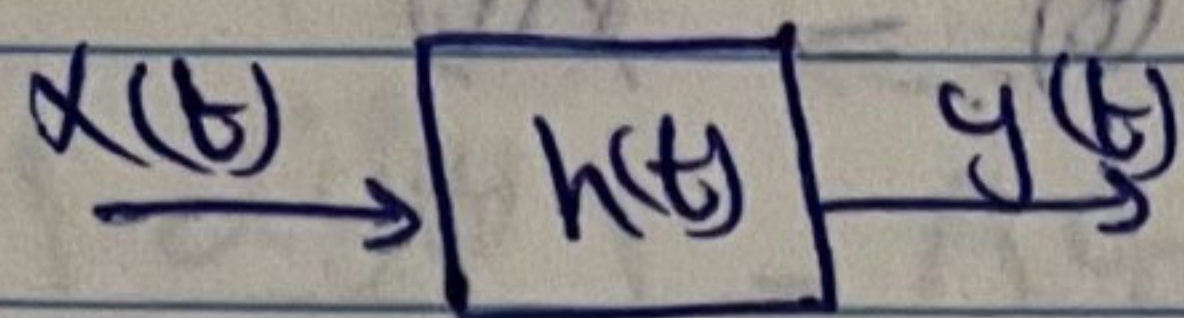
$$\Rightarrow X(f) = \frac{1}{2\omega} \pi\left(\frac{f}{2\omega}\right)$$



$$b- E = \int_{-\infty}^{\infty} |X(f)|^2 df = \int_{-\omega}^{\omega} \left(\frac{1}{2\omega}\right)^2 df$$

$$= \frac{1}{4\omega^2} \cdot 2\omega \Rightarrow \boxed{E = \frac{1}{2\omega}}$$

7- Convolution Theorem



-LTI-

$$y(t) = x(t) * h(t)$$

$$\hookrightarrow Y(\omega) = X(\omega) H(\omega) \Rightarrow H(\omega) = \frac{Y(\omega)}{X(\omega)}$$

EX For LTI system if the input signal

$X(t) = \pi\left(\frac{t}{2}\right)$ & the response of system

$h(t) = \pi\left(\frac{t}{2}\right)$. Evaluate the output signal $y(t)$

For LTI system

$$y(t) = x(t) * h(t)$$

$$\hookrightarrow Y(\omega) = X(\omega) H(\omega)$$

$$= \mathcal{F}\left[\pi\left(\frac{t}{2}\right)\right] \mathcal{F}\left[\pi\left(\frac{t}{2}\right)\right]$$

$$= 2 \operatorname{sinc}(2\omega) 2 \operatorname{sinc}(2\omega)$$

$$\mathcal{F}^{-1}[Y(\omega) = 4 \operatorname{sinc}^2(2\omega)]$$

$$y(t) = 4 \left(\frac{1}{2} \wedge\left(\frac{t}{2}\right)\right)$$

$$\Rightarrow y(t) = 2 \wedge\left(\frac{t}{2}\right)$$

Ex] Consider the following signal

$$RC \frac{dy(t)}{dt} + y(t) = x(t)$$

Evaluate.

① the response of the system $h(t)$.

$$\mathcal{F} \left[RC \frac{dy(t)}{dt} + y(t) = x(t) \right]$$

$$RC j2\pi f Y(f) + Y(f) = X(f)$$

$$Y(f) [RC j2\pi f + 1] = X(f)$$

$$\frac{Y(f)}{X(f)} = \frac{1}{jRC2\pi f + 1} = H(f)$$

$$\rightarrow H(f) = \frac{1}{RC(j2\pi f + \frac{1}{RC})}$$

Since $\mathcal{F}^{-1} \left[\frac{1}{\alpha + j2\pi f} \right] = e^{-\alpha t} u(t)$

$$\rightarrow h(t) = \frac{1}{RC} e^{-t/RC} u(t)$$

② the out put of the impulse ^{input} response

$$y(t) = h(t) \quad \text{In general } y(t) = x(t) * h(t)$$

For impulse Response $x(t) = \delta(t)$

$$y(t) = x(t) * h(t) = \delta(t) * h(t)$$

$$\Rightarrow y(t) = h(t)$$

8 Differentiation & Integration Theorem

$$F\left[\frac{d^n y(t)}{dt^n}\right] = (j2\pi f)^n Y(f)$$

$$F\left[\int_{-\infty}^t h(\tau) d\tau\right] = \frac{1}{j2\pi f} H(f)$$

z.v. → ③ the output signal if $X(t) = e^{-2t} u(t)$.

$$y(t) = X(t) * h(t)$$

$$Y(f) = X(f) H(f)$$

$$= \left(\frac{1}{2 + j2\pi f}\right) \left(\frac{1/R_c}{\frac{1}{R_c} + j2\pi f}\right)$$

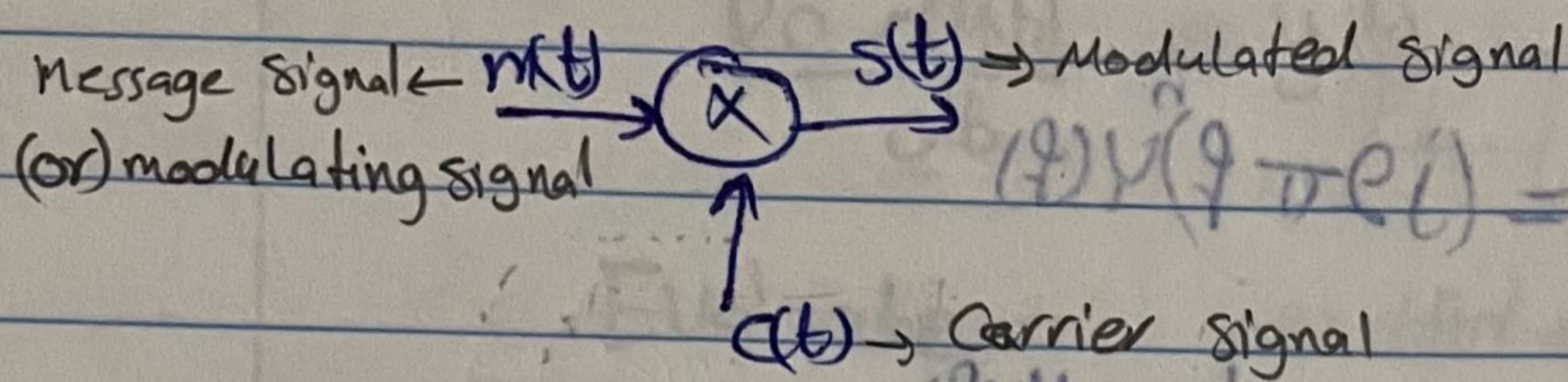
By using partial fraction

$$Y(f) = \frac{A}{2 + j2\pi f} + \frac{(1/R_c)(B)}{\frac{1}{R_c} + j2\pi f}$$

$$= \frac{A\left(\frac{1}{R_c} + j2\pi f\right) + \left(\frac{1}{R_c}\right)(B)(2 + j2\pi f)}{(2 + j2\pi f)\left(\frac{1}{R_c} + j2\pi f\right)}$$

(L4)

Example Consider the following ~~signal~~ system



where $m(t) = 3 \cos(20\pi t)$: message signal

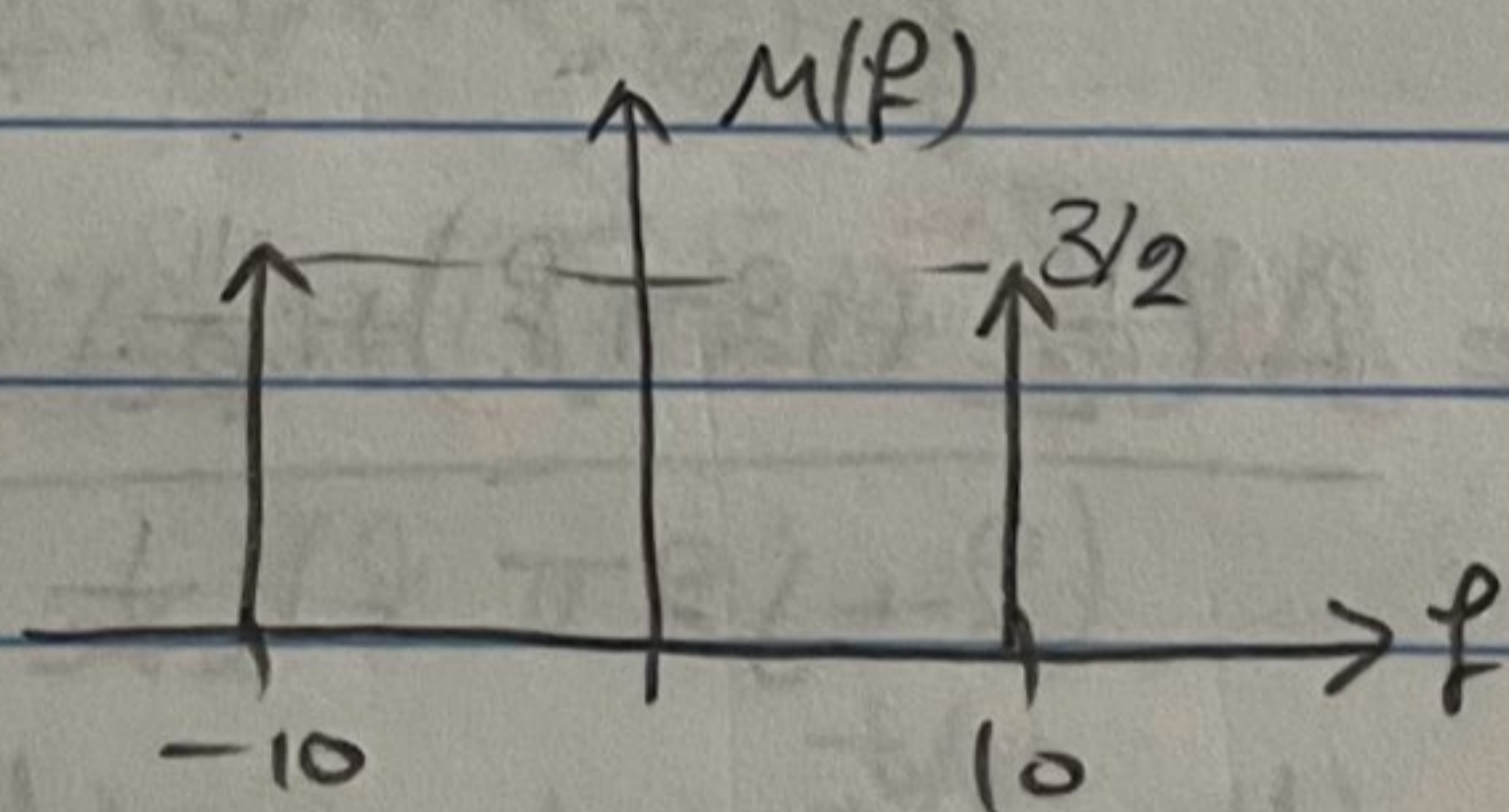
$c(t) = 4 \cos(200\pi t)$: carrier signal

a- Evaluate and plot the spectrum of each message and carrier signal

Ans:

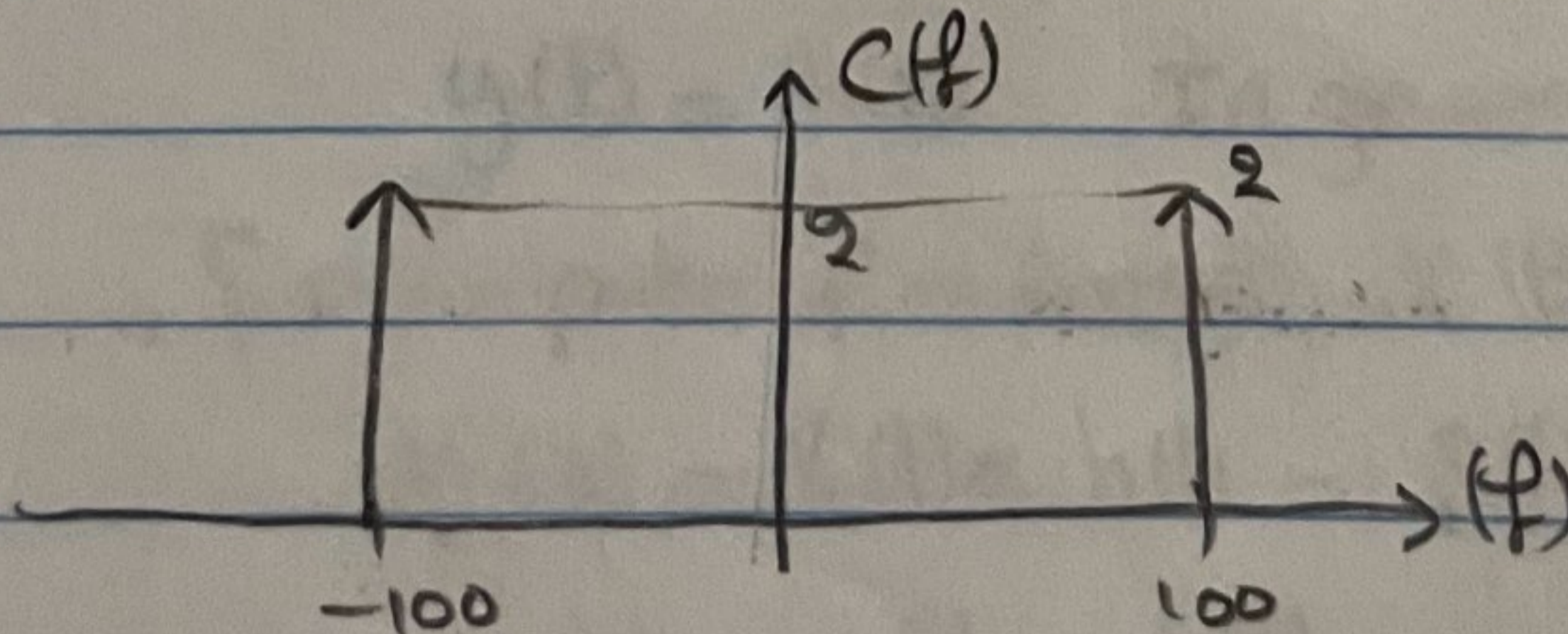
$$f[m(t) = 3 \cos(20\pi t)]$$

$$\hookrightarrow M(f) = \frac{3}{2} \delta(f-10) + \frac{3}{2} \delta(f+10)$$

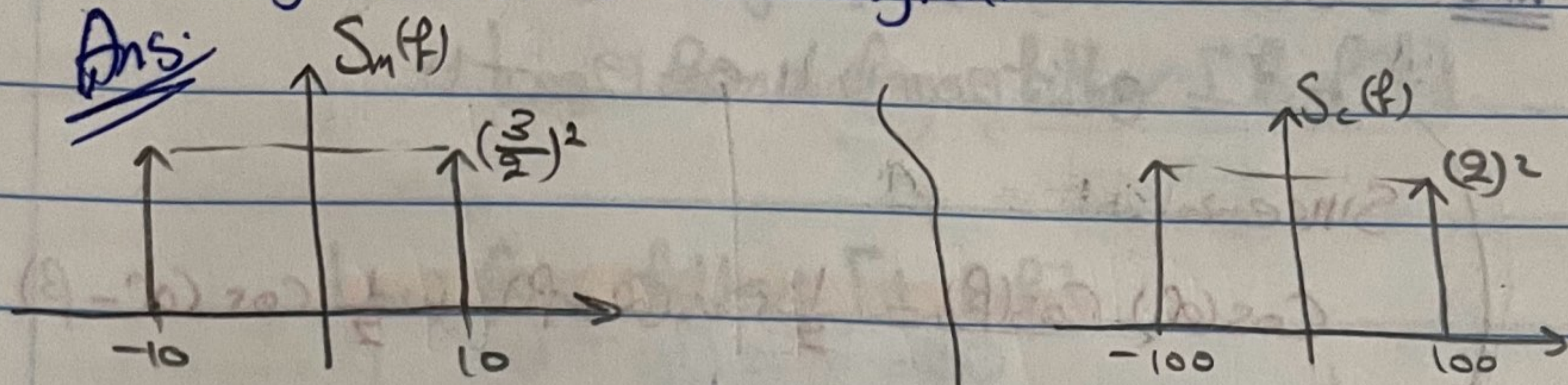


$$f[c(t) = 4 \cos(200\pi t)]$$

$$\hookrightarrow C(f) = 2 \delta(f-100) + 2 \delta(f+100)$$



b - Evaluate and plot PSD for each message signal and carrier signal.



$$S_m(f) = \left(\frac{3}{2}\right)^2 \delta(f-10) + \left(\frac{3}{2}\right)^2 \delta(f+10) \quad \left| \quad S_c(f) = 4 \delta(f-100) + 4 \delta(f+100)\right.$$

c - Evaluate the total power for each message signal and carrier signal.

Ans:

to evaluate Total power \rightarrow Time domain

By using time domain $\left[P = \frac{(A_m A_c)^2}{2} \right]$

freq domain $[P = 2 \cdot (A_m A_c)^2]$

$$P_m = \frac{(3)^2}{2} = \frac{9}{2}$$

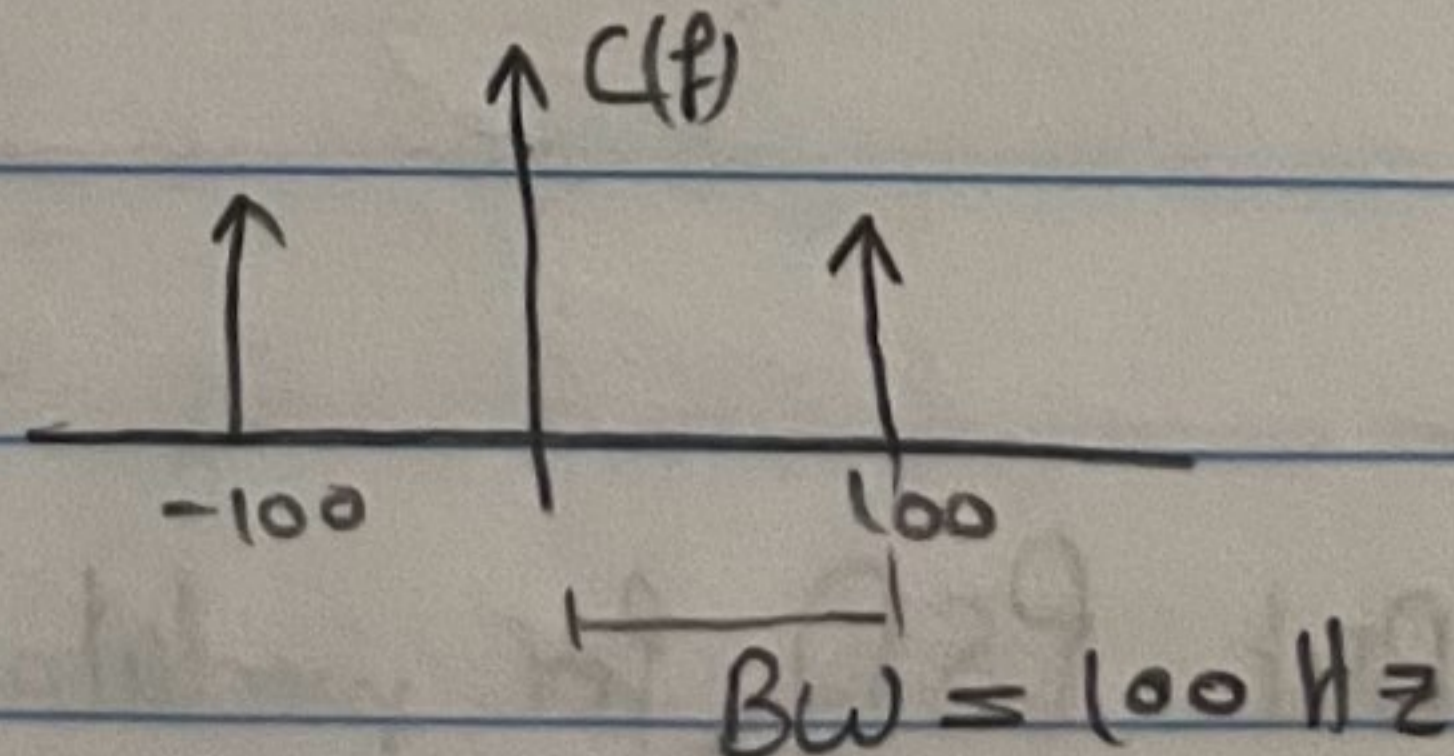
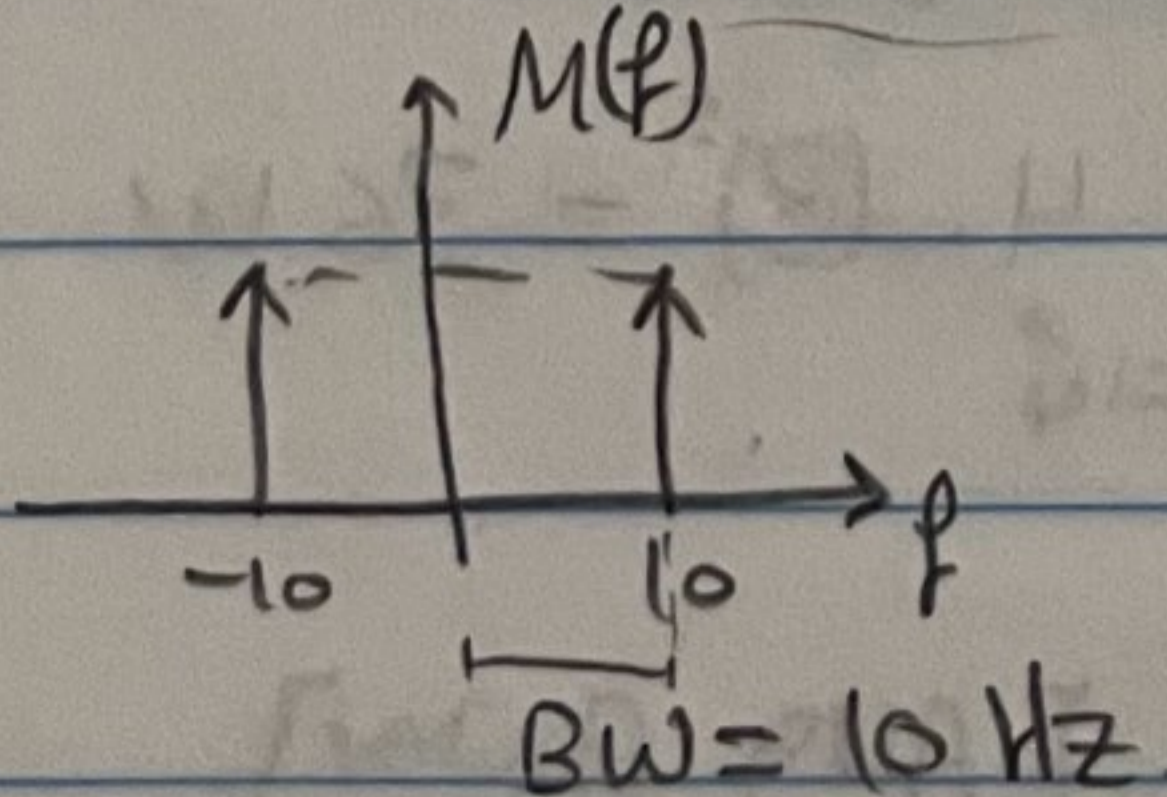
$$P_m = 2 \cdot \left(\frac{3}{2}\right)^2 = \frac{9}{2}$$

$$P_c = \frac{(4)^2}{2} = 8$$

$$P_c = 2 \cdot (2)^2 = 8$$

d - Evaluate the bandwidth (BW) for each message & carrier signal.

Ans Since message & carrier signals are base band signal \rightarrow original



بعد اعمى فورييه
عبر ال origin

e- Evaluate the modulated signal, $S(t)$.

Ans. $S(t) = m(t) c(t)$
 $= 3 \cos(20\pi t) 4 \cos(200\pi t)$

Since \rightarrow

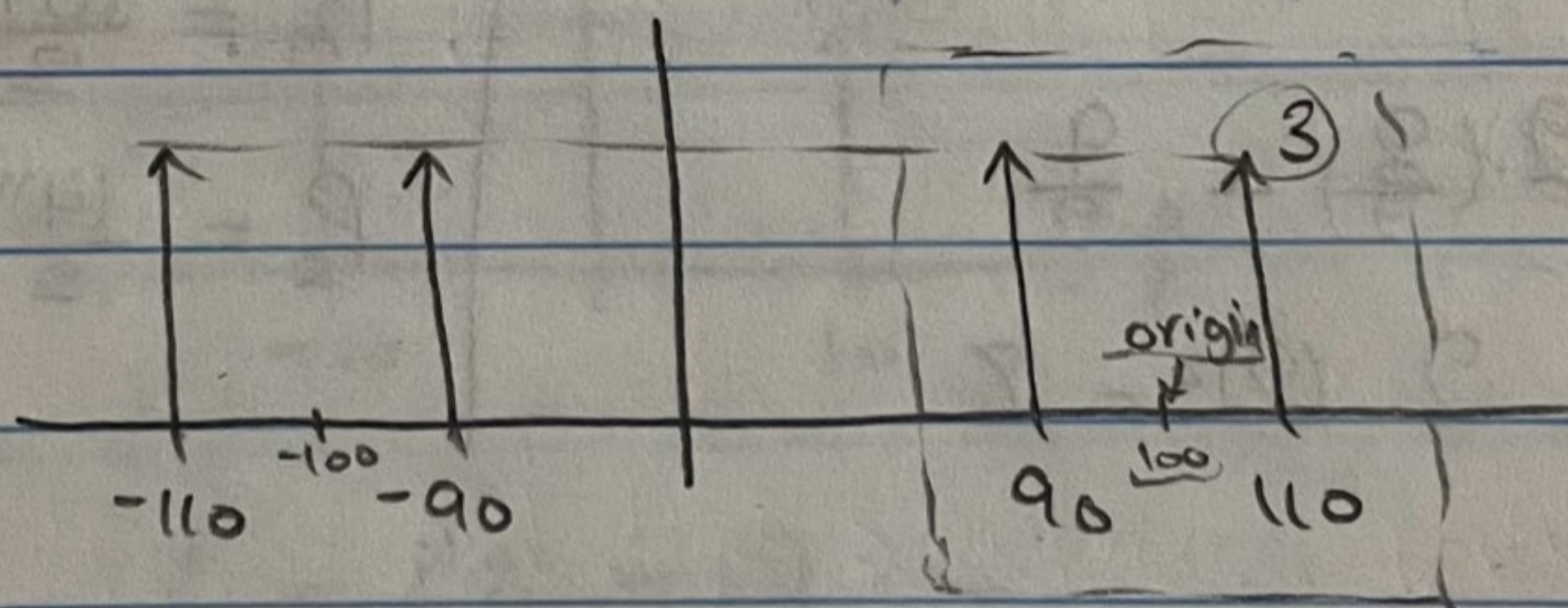
$$\cos(\alpha) \cos(\beta) = \frac{1}{2} \cos(\alpha + \beta) + \frac{1}{2} \cos(\alpha - \beta)$$

$$\rightarrow = 6 \cos(220\pi t) + 6 \cos(180\pi t)$$

f- Evaluate & plot the spectrum of modulated signal.

Ans.

$$S(f) = 3\delta(f-110) + 3\delta(f+110) + 3\delta(f-90) + 3\delta(f+90)$$



Pass band signal

نقطة عزال صفر
محور الترددات

$$\Rightarrow BW = 110 - 90 = 20 \text{ Hz}$$

$$P = 4 \cdot (3)^2 = 36 \text{ W}$$

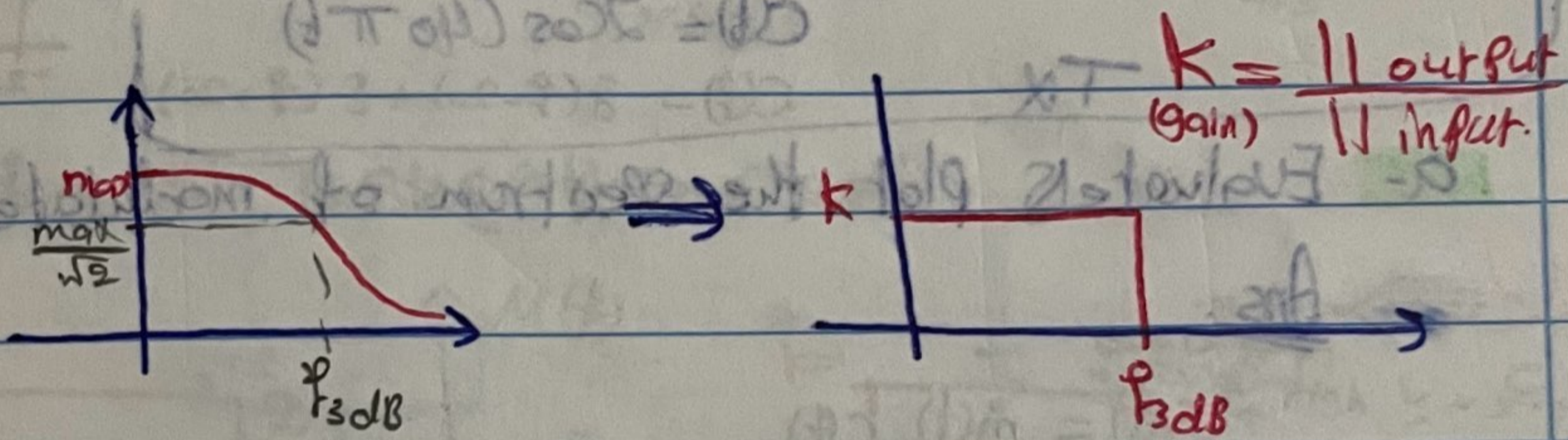
4 انتارات

But PSD for modulated signal [Avg power]

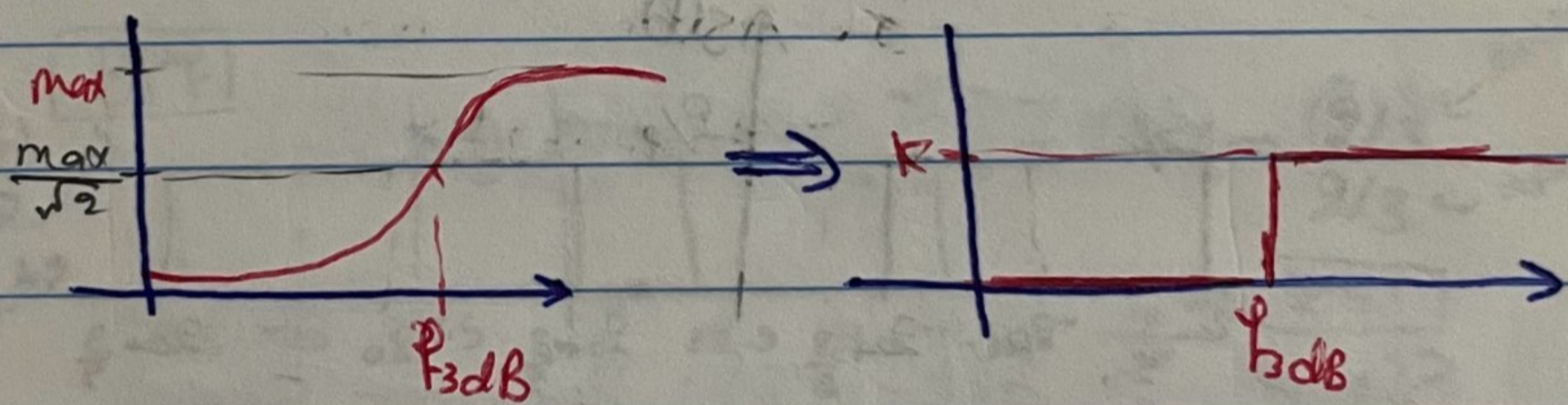
$$S_s(f) = (3)^2 \delta(f-90) + (3)^2 \delta(f+90) + 9\delta(f-110) + 9\delta(f+110)$$

- ≡ Filters.
- ↳ Low Pass filter [L.P.F.]
 - ↳ High Pass filter [H.P.F.]
 - ↳ Band Pass filter [B.P.F.]

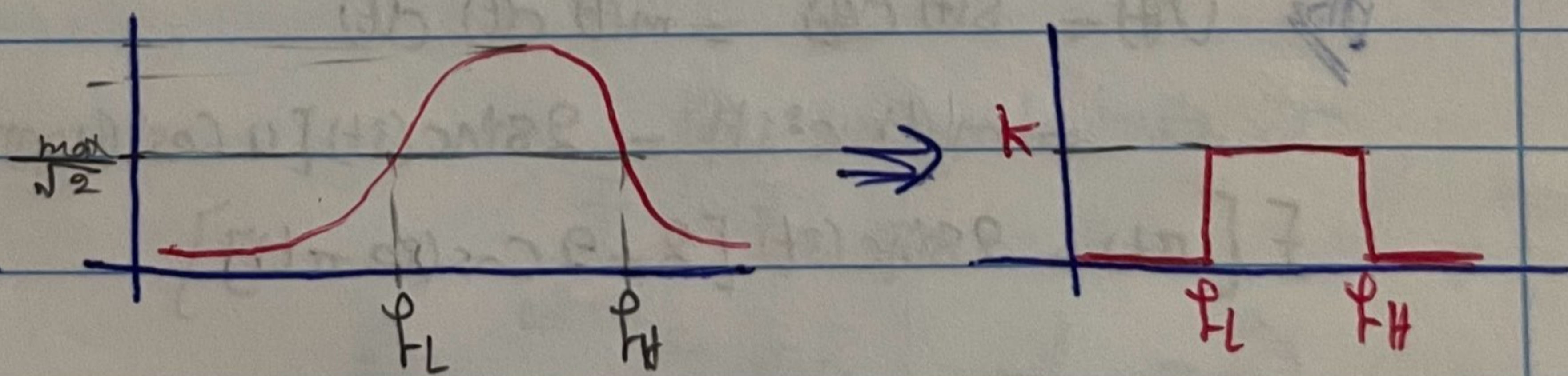
Low Pass filter [L.P.F.]



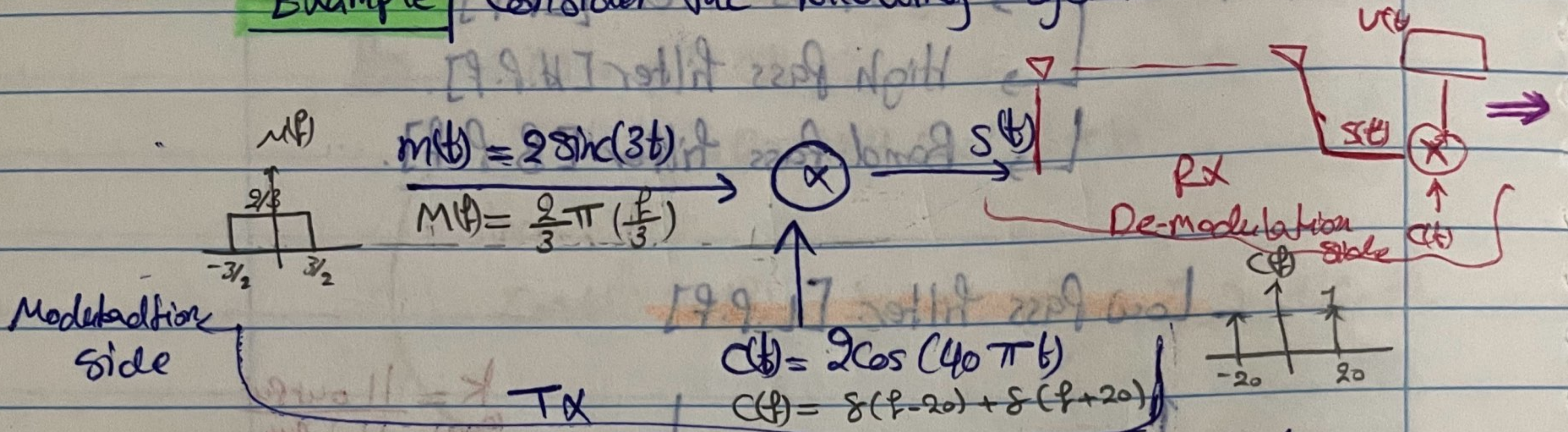
High Pass filter [H.P.F.]



Band Pass filter [B.P.F.]



Example | Consider the following system.



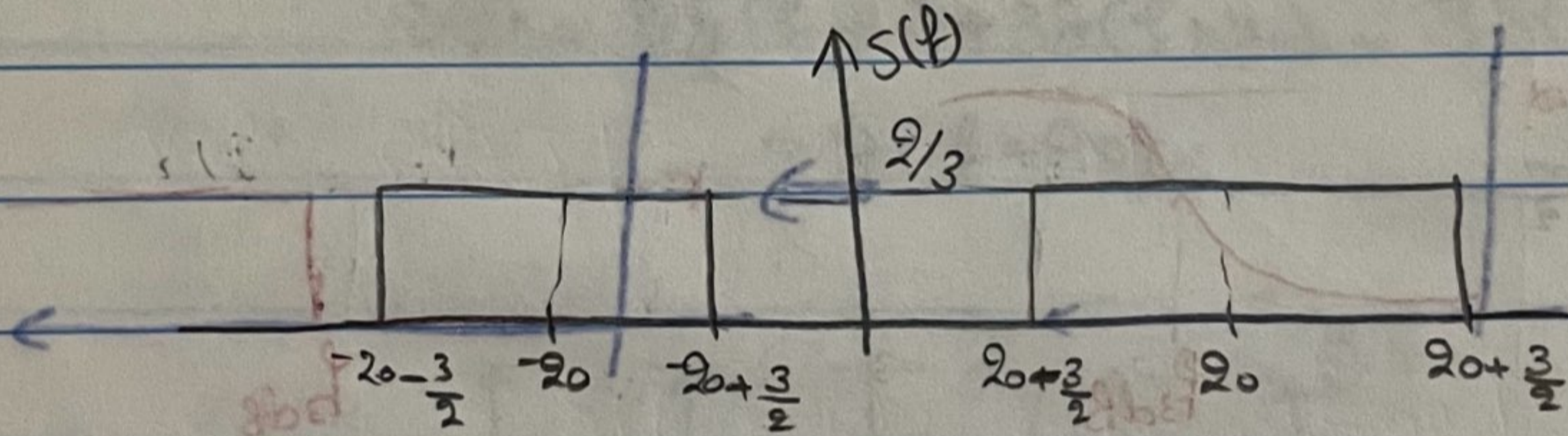
a- Evaluate & plot the spectrum of modulated signal

Ans.

$$s(t) = m(t) c(t)$$

$$= 2 \text{sinc}(3t) \cdot 2 \cos(40\pi t)$$

$$S(f) = 2 \cdot 2 \cdot \frac{1}{3} \cdot \frac{1}{2} \left[\pi \left(\frac{1}{3}(f-20)\right) + \pi \left(\frac{1}{3}(f+20)\right) \right]$$



$$E = \int_{-\infty}^{\infty} |S(f)|^2 df$$

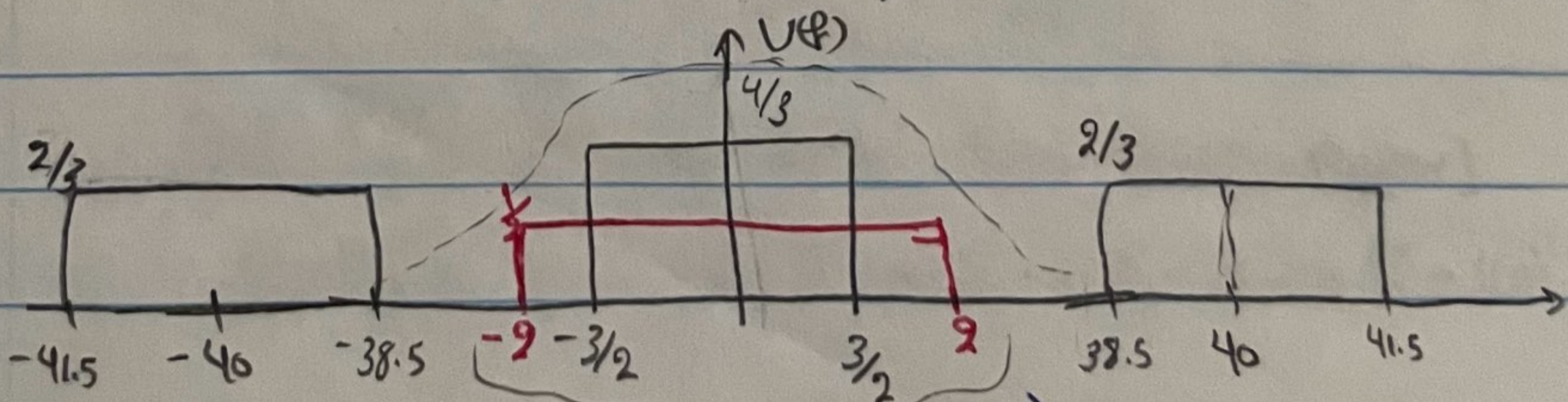
b- Evaluate and plot the spectrum u(t)

Ans: $u(t) = s(t) c(t) = m(t) c(t) c(t)$

$$= m(t) c^2(t) = 2 \text{sinc}(3t) [4 \cos^2(40\pi t)]$$

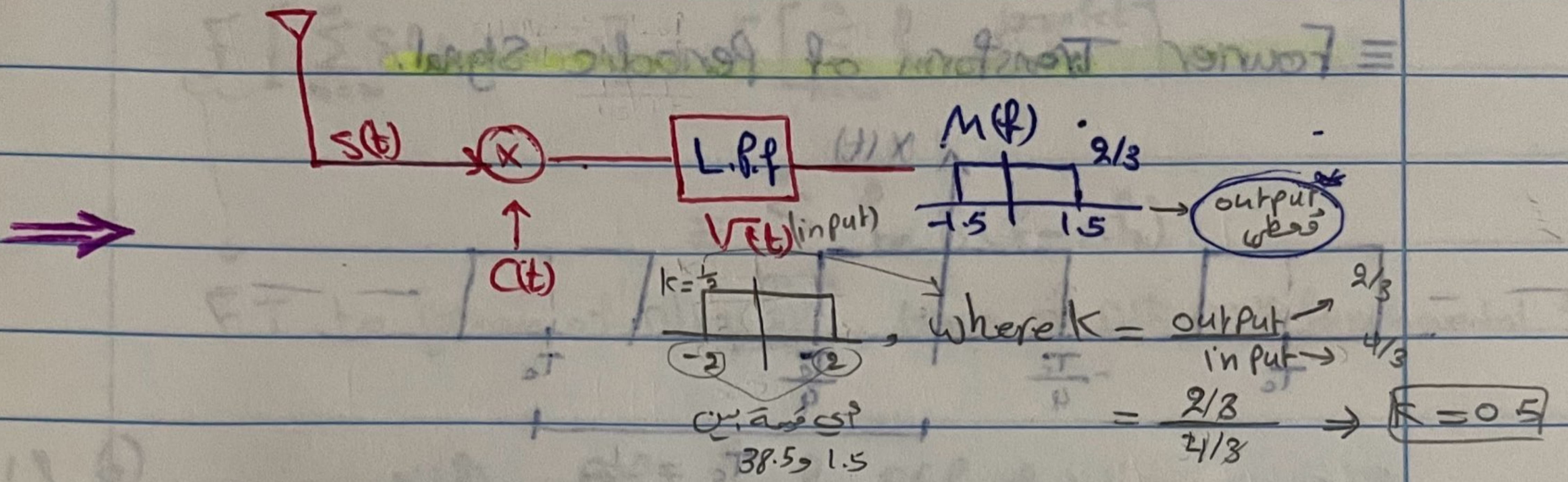
$$F[u(t)] = 2 \text{sinc}(3t) [2 + 2 \cos(80\pi t)]$$

$$U(f) = \frac{4}{3} \pi \left(\frac{f}{3}\right) + \frac{4}{3} \cdot \frac{1}{2} \left[\pi \left(\frac{1}{3}(f-40)\right) + \pi \left(\frac{1}{3}(f+40)\right) \right]$$

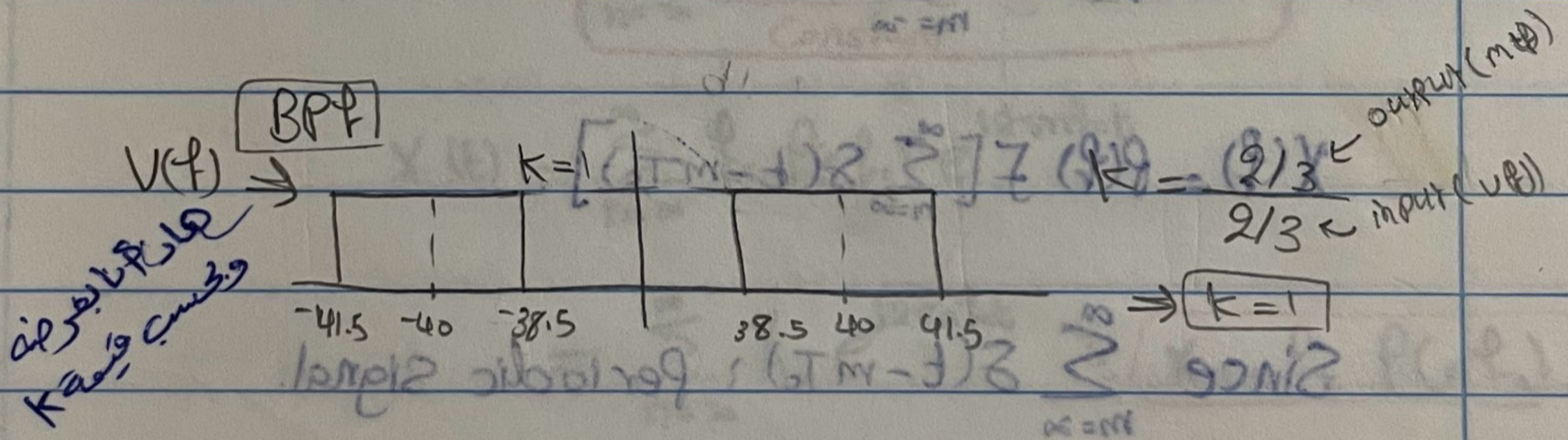
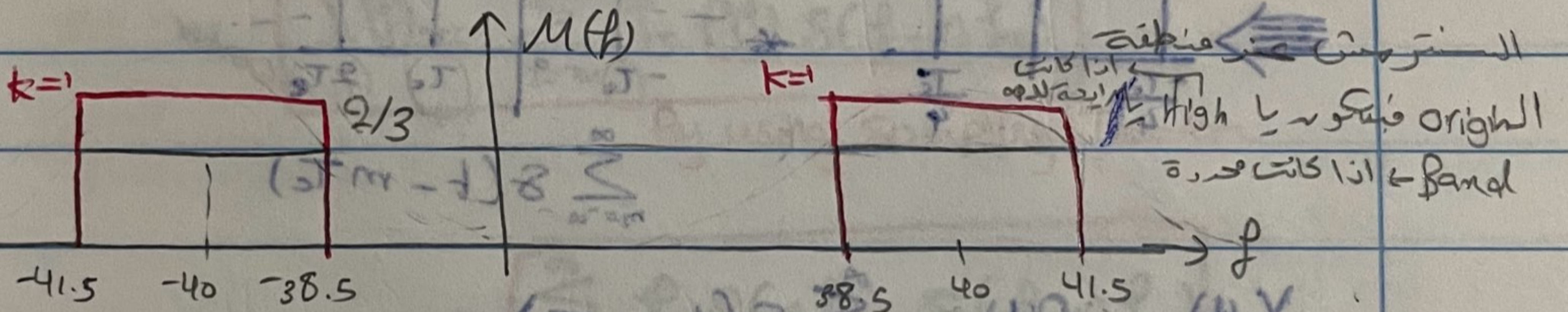


(ب) لو خرابه سيمان بعضيه ال out اي عوطه

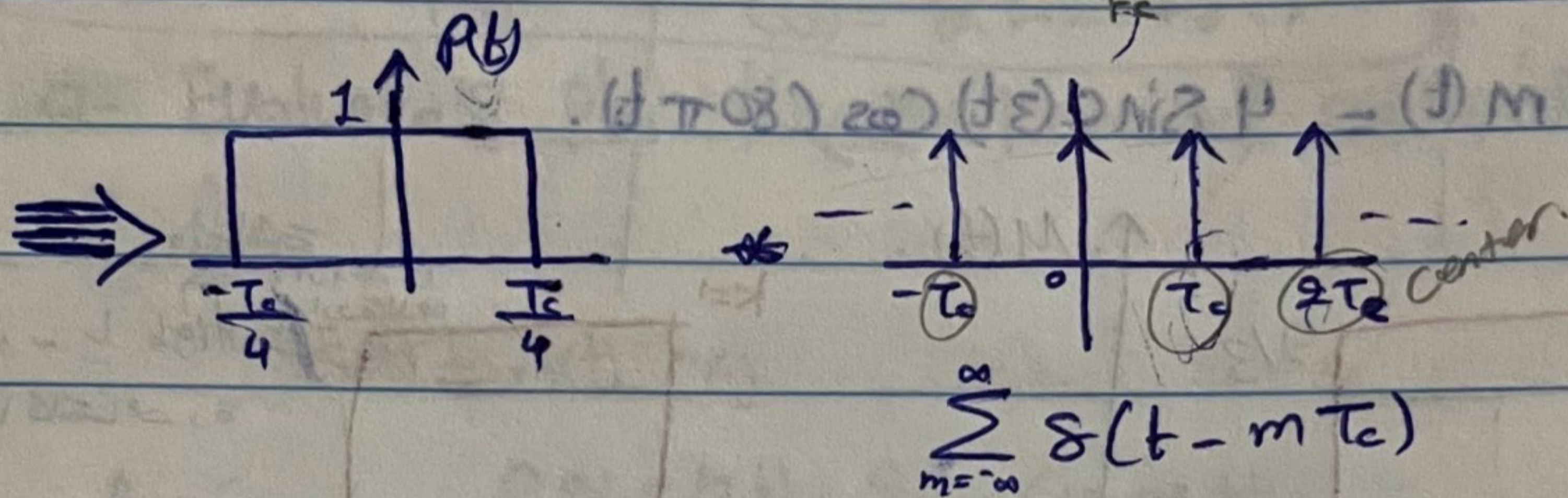
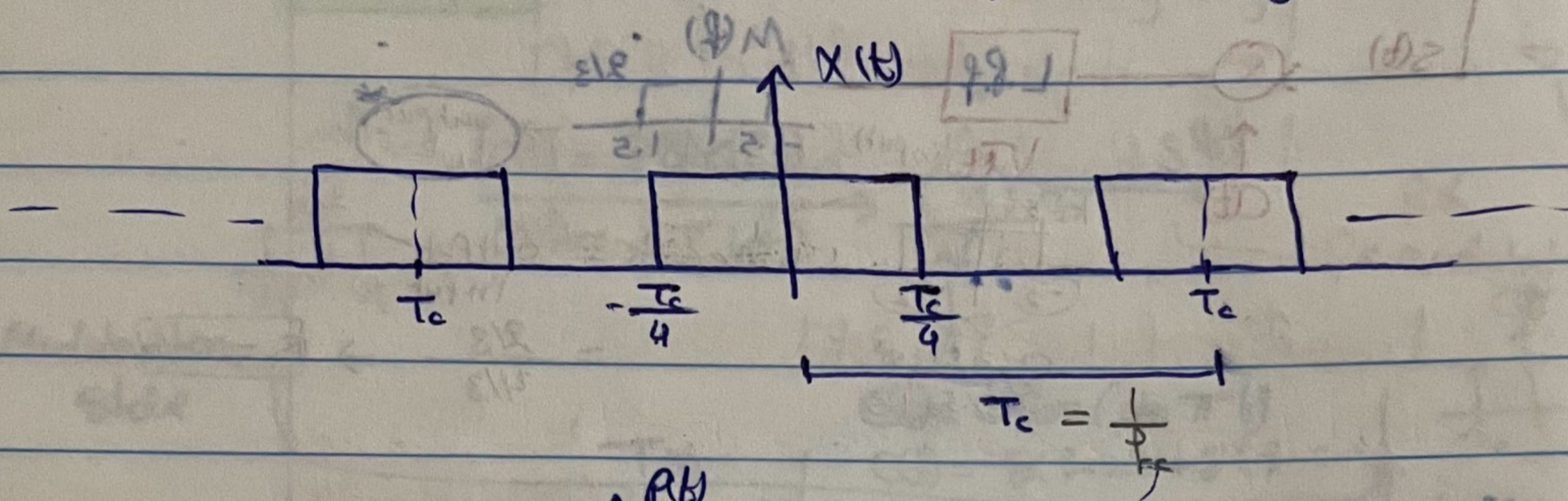
(L5)



c- if $m(t) = 4 \text{sinc}(3t) \cos(80\pi t)$.



≡ Fourier Transform of Periodic Signal.



$$X(t) = P(t) \sum_{m=-\infty}^{\infty} \delta(t - mT_c)$$

$$X(f) = P(f) \mathcal{F}\left[\sum_{m=-\infty}^{\infty} \delta(t - mT_c)\right]$$

Since $\sum_{m=-\infty}^{\infty} \delta(t - mT_c)$ is periodic signal.

$$\Rightarrow \sum_{m=-\infty}^{\infty} \delta(t - mT_c) = \sum_{m=-\infty}^{\infty} C_n e^{j2\pi nft}$$

To evaluate C_n

$$C_n = \frac{1}{T_c} \int_{-\frac{T_c}{2}}^{\frac{T_c}{2}} \delta(t) e^{-j2\pi nft} dt$$

$t_0 = 0$
 $\frac{-T_c}{2}$ and $\frac{T_c}{2}$

$\int e^0 dt = 1$

By using sifting theorem.

$$C_n = \frac{1}{T_c} = f_c$$

$$F \left[\sum_{m=-\infty}^{\infty} \delta(t - mT_c) \right] = F \left[\sum_{n=-\infty}^{\infty} f_c e^{j2\pi n f_c t} \right]$$

$$\equiv \sum_{n=-\infty}^{\infty} f_c \delta(f - n f_c)$$

FT to [train of Delta(δ)] \rightarrow train of Delta(δ) * fundamental freq.

(L6) $\rightarrow X(f) = P(f) \sum_{n=-\infty}^{\infty} f_c \delta(f - n f_c)$

$$X(f) = \sum_{n=-\infty}^{\infty} f_c P(f) \delta(f - n f_c)$$

By using Sampling Theorem.

$$= \sum_{n=-\infty}^{\infty} f_c \underbrace{P(n f_c)}_{\text{Constant}} \delta(f - n f_c)$$

$$X(t) = \sum_{n=-\infty}^{\infty} f_c P(n f_c) e^{j2\pi n f_c t}$$

$$\equiv \sum_{n=-\infty}^{\infty} X_n e^{j2\pi n f_c t}$$

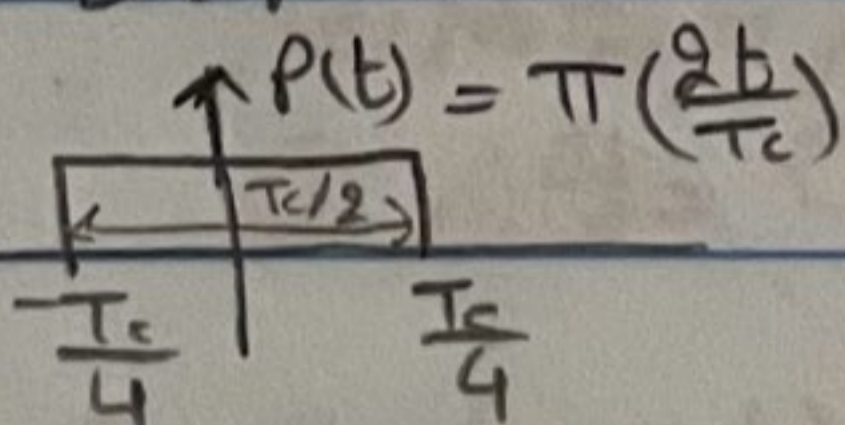
$$; X_n = f_c P(n f_c)$$

For previous example,

1. Evaluate FT of $x(t)$.

$$X(f) = \sum_{n=-\infty}^{\infty} f_c P(f) \delta(f - n f_c)$$

$$f_c = \frac{1}{T_c}$$

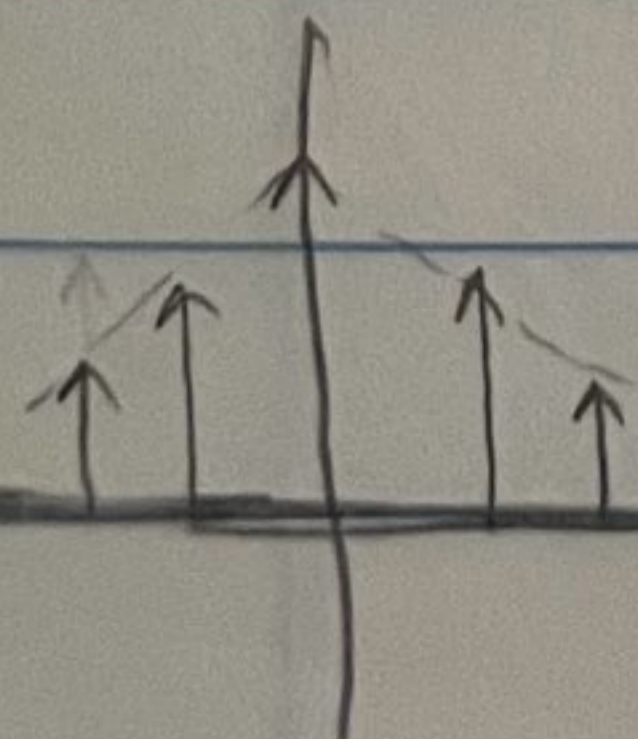


$\rightarrow P(f)$

$$P(n f_c) = \frac{T_c}{2} \text{sinc} \left(\frac{T_c}{2} n f_c \right)$$

$$\rightarrow X(f) = \sum_{n=-\infty}^{\infty} \frac{1}{T_c} \cdot \frac{T_c}{2} \text{sinc} \left(\frac{T_c}{2} n \cdot \frac{1}{T_c} \right) \delta$$

$$\Rightarrow X(f) = \sum_{n=-\infty}^{\infty} \frac{1}{2} \text{sinc} \left(\frac{n}{2} \right) \delta(f - n f_c)$$



1. يكتب المعادلة الأسية
2. $f_c = \frac{1}{T_c}$

3. يأخذ بيريوود وحدة
و يطلع منها $P(f)$ ويوجد
ياخذها FT $\leftarrow P(f)$

4. عوضنا $P(f)$ $\leftarrow P(n f_c)$
5. نعوض في المعادلة الأصلية

2. Evaluate $X(t)$.

$$X(t) = \sum_{n=-\infty}^{\infty} P_c P(nT_c) e^{j2\pi n f_c t}$$

$$= \sum_{n=-\infty}^{\infty} \frac{1}{2} \text{sinc}\left(\frac{n}{2}\right) e^{j2\pi n f_c t}$$

3. Evaluate the Trigonometric Coefficient Fourier series.

$$X(t) = a_0 + \sum_{n=1}^{\infty} a_n \cos(n\omega_0 t) + \sum_{n=1}^{\infty} b_n \sin(n\omega_0 t)$$

$\omega_0 = \omega_c$, $b_n = 0$ - even function

$$a_0 = \frac{1}{T_c} \int_{-T_c/4}^{T_c/4} (1) dt \rightarrow \frac{1}{T_c} \cdot \frac{T_c}{2} \Rightarrow a_0 = \frac{1}{2}$$

$a_0 = X_0 = P(0) = \frac{1}{2} \cdot \text{sinc}(0) \Rightarrow a_0 = \frac{1}{2}$

Since $X_n = \dots$

$$X_n = \begin{cases} \frac{1}{2}(a_n - j b_n), & n > 0 \\ \frac{1}{2}(a_n + j b_n), & n < 0 \\ a_0, & n = 0 \end{cases}$$

$X_n = P(nT_c)$

$$a_n = 2 \text{Re}\{X_n\}, \quad b_n = 2 \text{Im}\{X_n\}, \quad a_0 = X_0$$

For previous example

$$a_n = 2 \cdot \frac{1}{2} \text{sinc}\left(\frac{n}{2}\right) \Rightarrow a_n = \text{sinc}\left(\frac{n}{2}\right)$$

4- Evaluate PSD.

$$S_x(f) = \sum_{n=-\infty}^{\infty} |X_n|^2 \delta(f - n f_c)$$

$$= |X_0|^2 \delta(f) + 2 \sum_{n=1}^{\infty} |X_n|^2 \delta(f - n f_c)$$

$$S_x(f) = \left(\frac{1}{2}\right)^2 \delta(f) + 2 \sum_{n=1}^{\infty} \left(\frac{1}{2} \text{sinc}\left(\frac{n}{2}\right)\right)^2 \delta(f - n f_c)$$

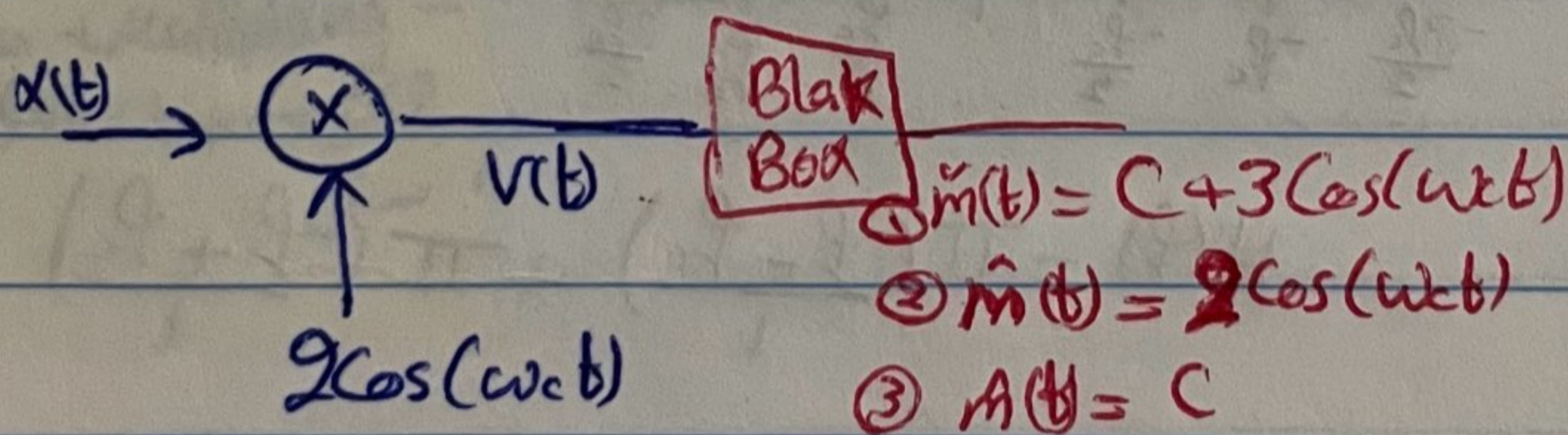
5- Evaluate the total power $(-1 < n < 1)$.

$$|X_0|^2 = \left(\frac{1}{2}\right)^2 = \frac{1}{4}$$

$$|X_1|^2 = |X_{-1}|^2 = \left(\frac{1}{2} \text{sinc}\left(\frac{1}{2}\right)\right)^2$$

$$P_{-1 < n < 1} = |X_0|^2 + 2|X_1|^2$$

6- Based on $X(t)$ (in previous part). Consider the following system.



$$X(t) = \frac{1}{2} + \sum_{n=1}^{\infty} \text{sinc}\left(\frac{n}{2}\right) \cos(n \omega_c t)$$

6-a- Evaluate $v(t) = x(t) \cdot 2 \cos(\omega_c t)$

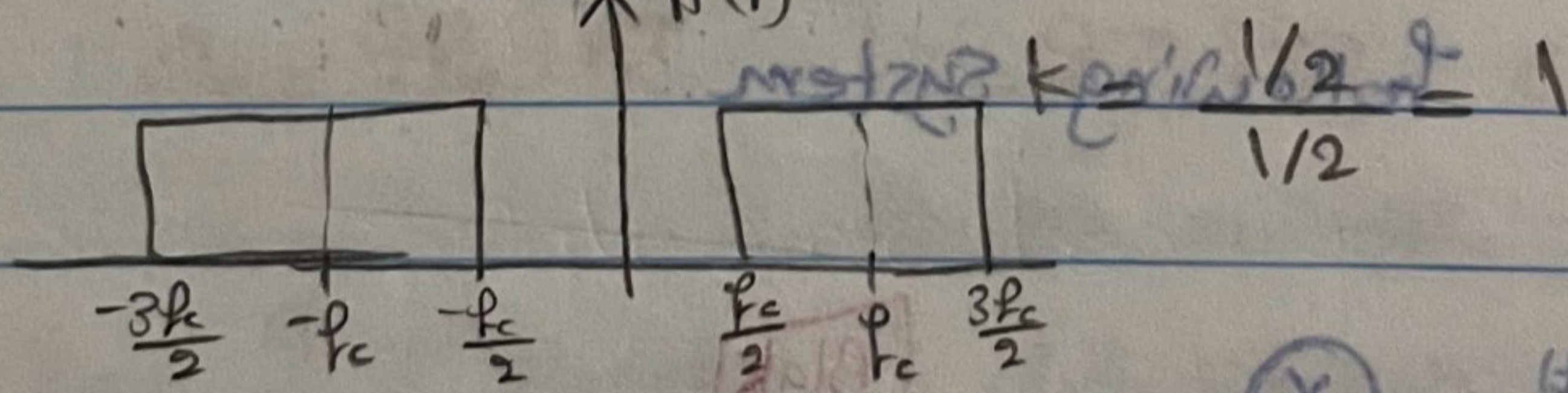
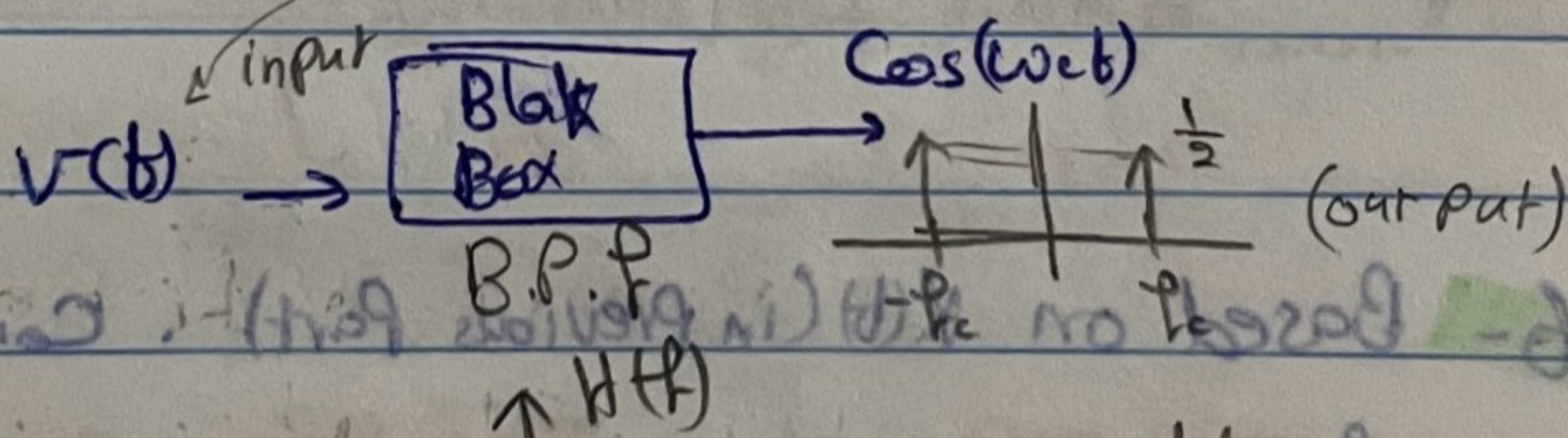
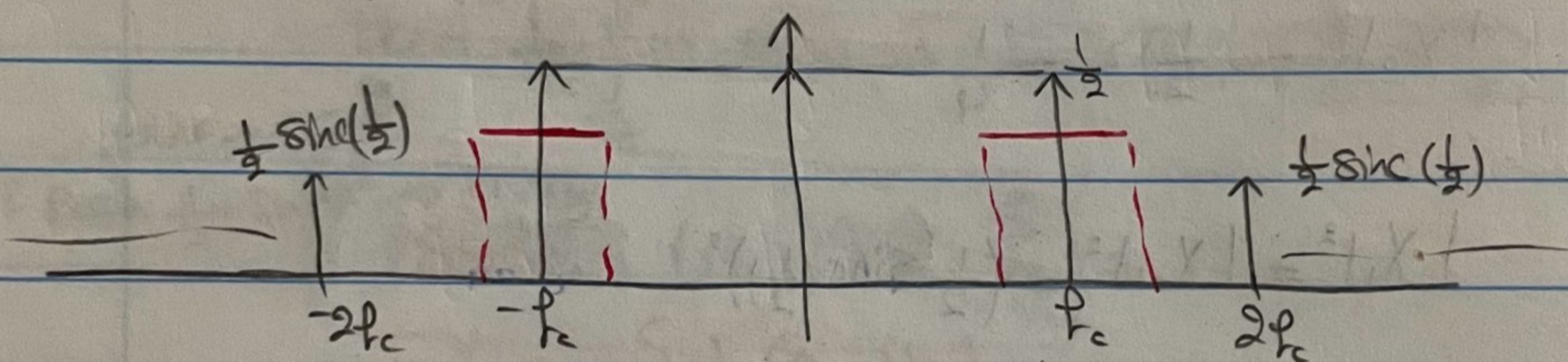
$$= \left[\frac{1}{2} + \sum_{n=1}^{\infty} \text{sinc}\left(\frac{n}{2}\right) \cos(n \omega_c t) \right] \cdot 2 \cos(\omega_c t)$$

$$V(t) = \cos(\omega_c t) + \sum_{n=1}^{\infty} 2 \operatorname{sinc}\left(\frac{n}{2}\right) \cos(n\omega_c t) \cos(\omega_c t)$$

$$V(t) = \cos(\omega_c t) + \sum_{n=1}^{\infty} 2 \operatorname{sinc}\left(\frac{n}{2}\right) \left[\frac{1}{2} \cos((n+1)\omega_c t) + \frac{1}{2} \cos((n-1)\omega_c t) \right]$$

$$V(t) = \cos(\omega_c t) + \sum_{n=1}^{\infty} \operatorname{sinc}\left(\frac{n}{2}\right) \cos((n+1)\omega_c t) + \sum_{n=1}^{\infty} \operatorname{sinc}\left(\frac{n}{2}\right) \cos((n-1)\omega_c t)$$

$$V(f) = \frac{1}{2} \delta(f - f_c) + \frac{1}{2} \delta(f + f_c) + \sum_{n=1}^{\infty} \operatorname{sinc}\left(\frac{n}{2}\right) \left[\frac{1}{2} \delta(f - (n+1)f_c) + \frac{1}{2} \delta(f + (n+1)f_c) \right] + \sum_{n=1}^{\infty} \operatorname{sinc}\left(\frac{n}{2}\right) \left[\frac{1}{2} \delta(f - (n-1)f_c) + \frac{1}{2} \delta(f + (n-1)f_c) \right]$$

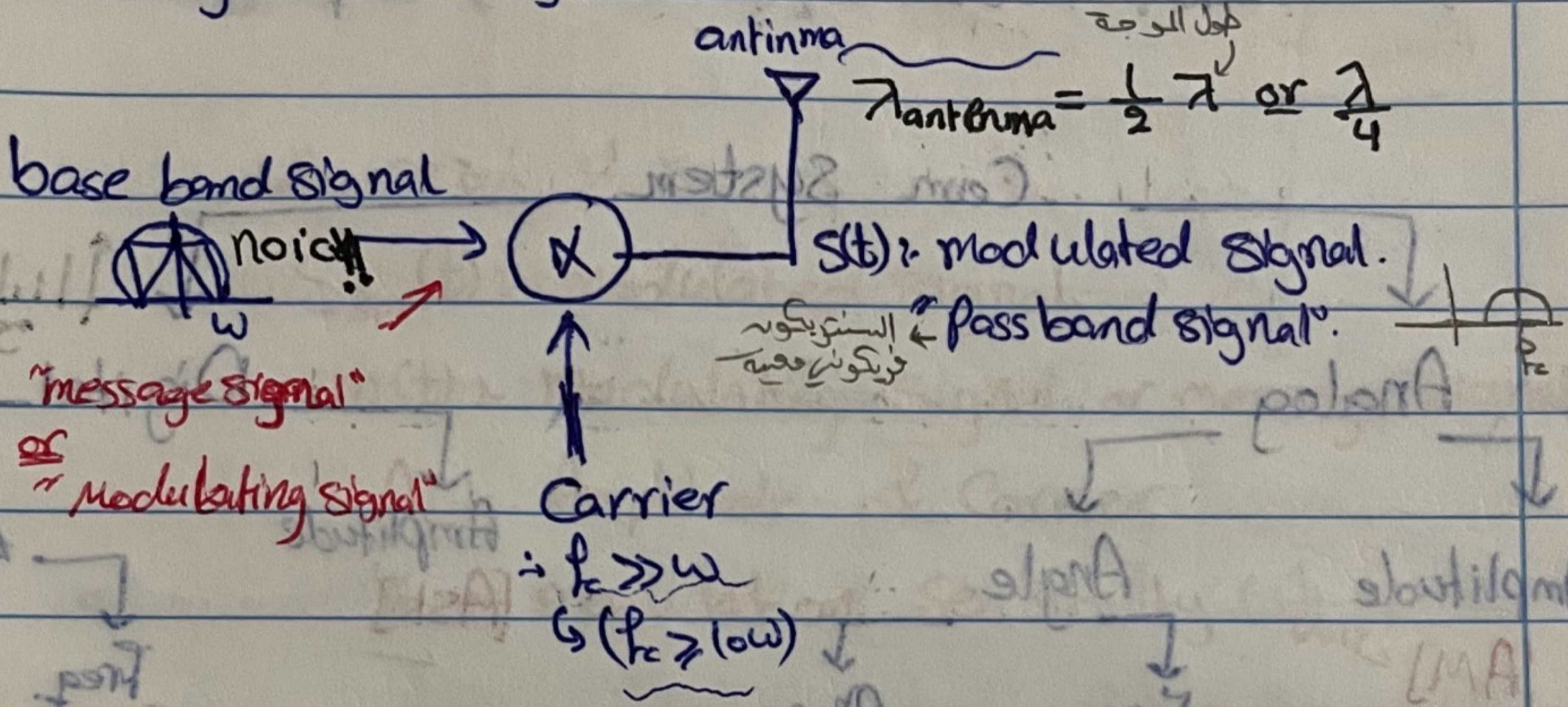


$$H(f) = \frac{1}{2} \Pi\left(\frac{f - f_c}{f_c}\right) + \frac{1}{2} \Pi\left(\frac{f + f_c}{f_c}\right)$$

(L7)

- Communication part -

↳ Analog Com } Modulation scheme.
 ↳ Digital Com }



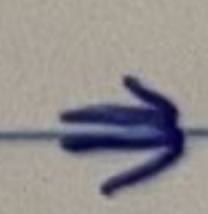
Why Modulation!

التحكم في ال antenna.
 له في الوضع الطبيعي ال signal
 الي ناعما بنقلها الفريكوئسي
 الها قليلة وهذا اعراضه طول
 الموجة عالى وطول الموجة
 عالى يعني طول ال antenna الي
 كبير نستغل عليه كبير
 بالتالي من الصعب نقل ال إشارة
 ع طول على ال antenna فيعمل ال Modem
 - Channel & زم تكون -
 Pass band signal.
 - Multiplexing - بقدر عمل
 أكثر Channel وكل وحدة ال
 ستر

eg : $m(t) = \cos(3000\pi t)$
 سرعة الضوء
 $\lambda = \frac{c}{f} = \frac{3 \times 10^8}{1.5 \times 10^3}$

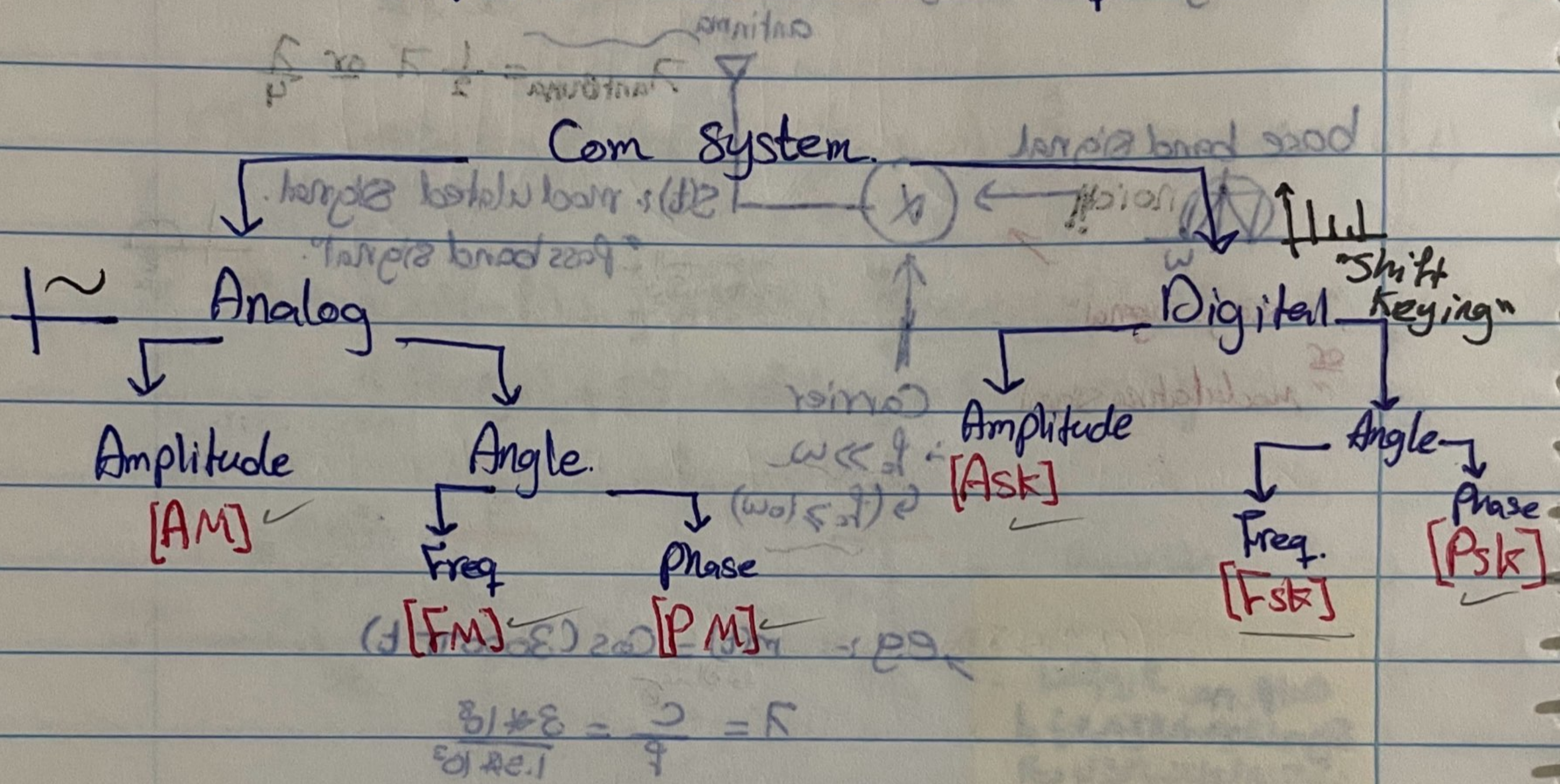
كبير جداً و
 صعب نقله على
 $\lambda = 2 \times 10^5$

ال antenna ع طول غير ضل معه Carrier
 قيمة الفريكوئسي فيها عالية عشان نقل ال



- In general :-

$$C(t) = \underbrace{A_c}_{\text{Amplitude}} \cos(\underbrace{\theta}_{\text{Angle}}) = A_c \cos(\underbrace{\omega t}_{\text{freq}} + \underbrace{\phi}_{\text{Phase}})$$



• Four types of AM :-

1] Normal AM

2] Double sideband suppressed carrier (DSB)

3] SSB single side band

(L8)

≡ Normal Amplitude modulation [AM] ^{تعليق على اللانسة}
على ال Amp Carrier
"DSB-FC"

$$S_{AM}(t) = [1 + k_a m(t)] \cdot A_c \cos(2\pi f_c t)$$

where:

$S_{AM}(t)$: modulated signal.

$m(t)$: modulating signal. or message signal.

A_c : Amplitude of Carrier.

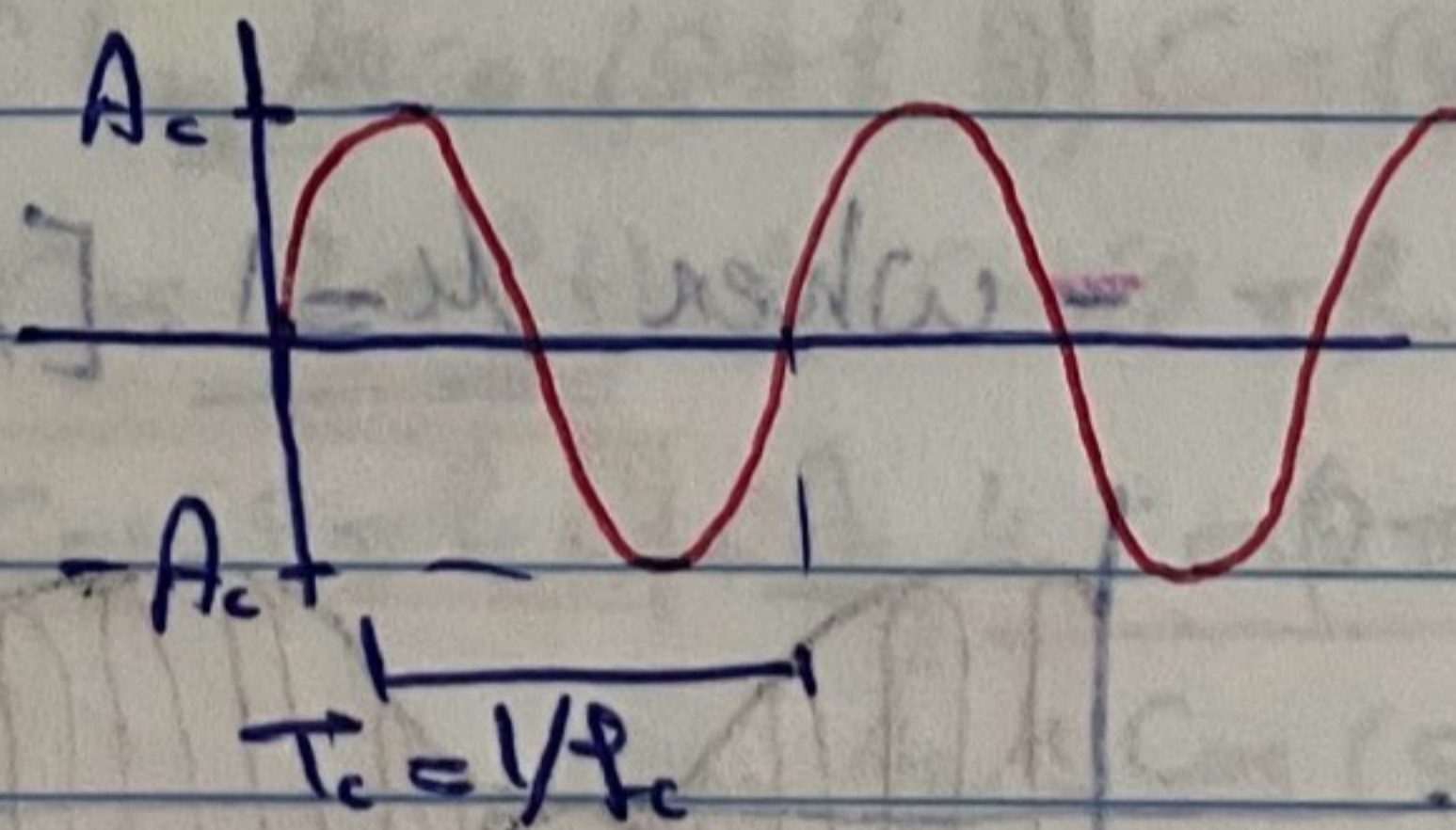
k_a : modulation sensitivity ($\frac{1}{V_{01}}$)

(Now), let $m(t) = A_m \cos(2\pi f_m t)$

$$m(t) = A_m \cos(2\pi f_m t)$$

$$\rightarrow S_{AM}(t) = A_c (1 + k_a A_m \cos(2\pi f_m t)) \cos(2\pi f_c t)$$

• For carrier signal. $c(t) = A_c \cos(2\pi f_c t)$

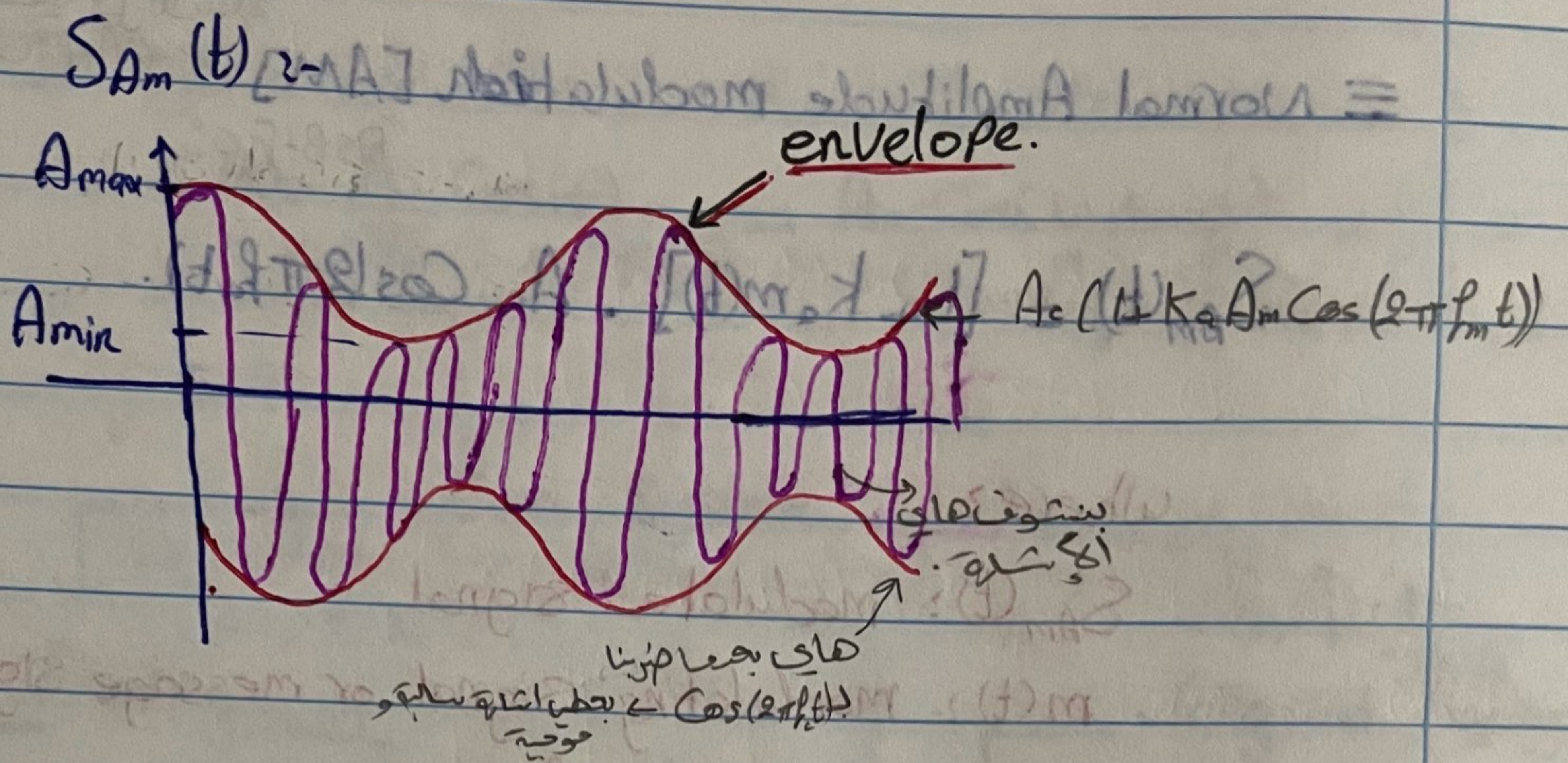


ال Amp تابع ال Carrier بظل ثابت
لهار يتغير عن طريقه
 $1 + k_a A_m \cos(2\pi f_m t)$

• Now, let us take

$$|A_c (1 + k_a A_m \cos(2\pi f_m t))| \begin{cases} \rightarrow (1 + k_a A_m) A_c \rightarrow A_{max} \\ \rightarrow (1 - k_a A_m) A_c \rightarrow A_{min} \end{cases}$$

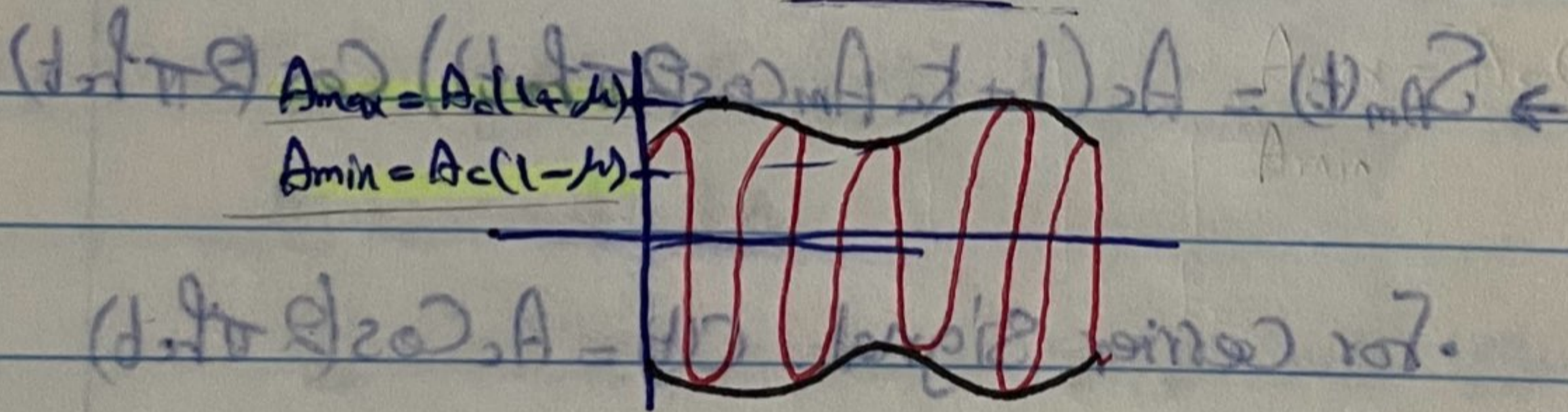
envelop لا يتغير الطرفين الموجب



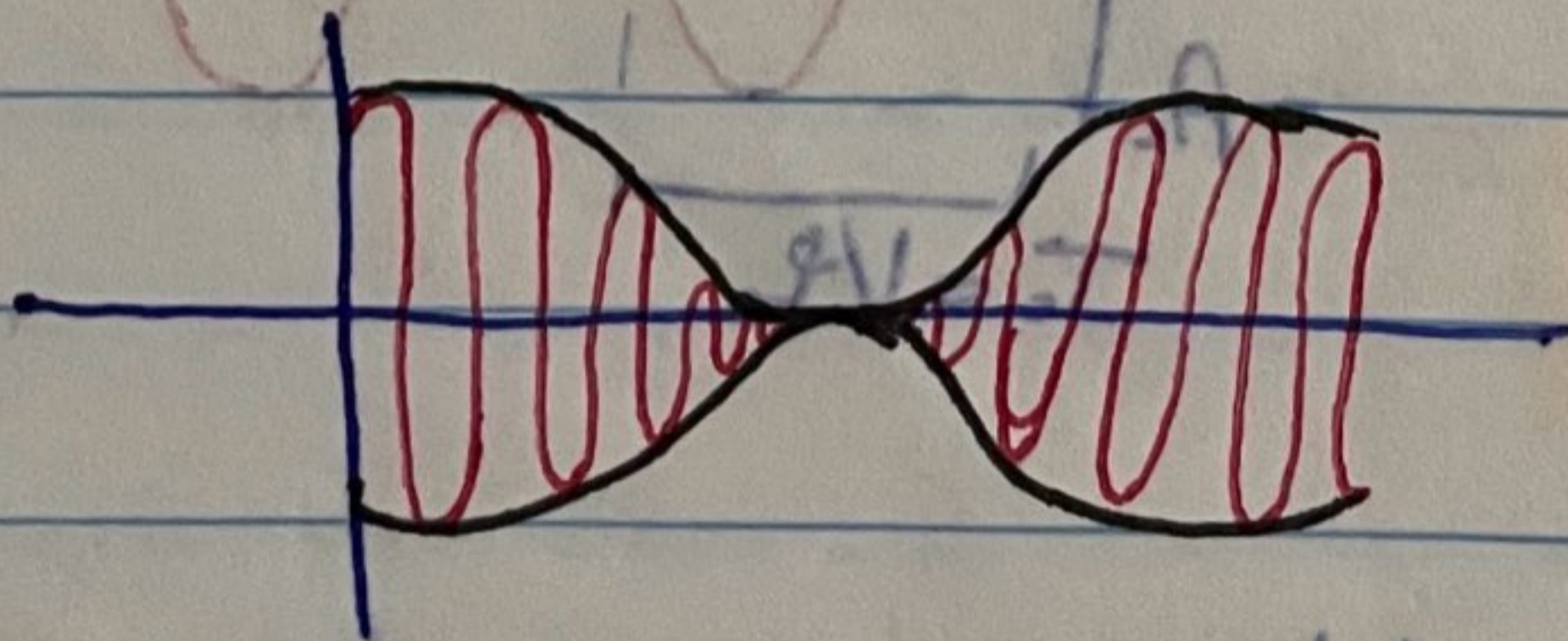
• Now, Let $\mu = K_a A_m$; $\mu =$ modulation index.

$\rightarrow S_{AM}(t) = A_c [1 + \mu \cos(2\pi f_m t)] \cos(2\pi f_c t)$

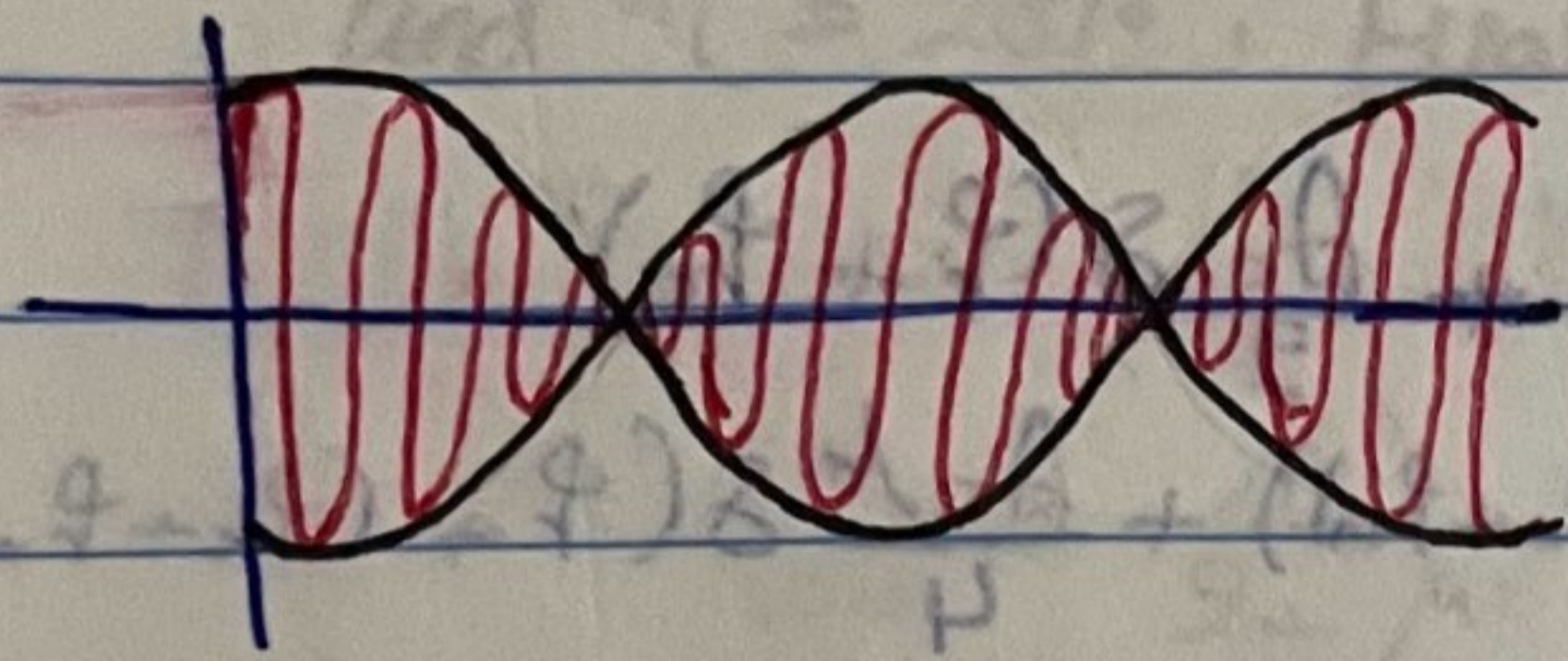
- when $\mu < 1$ [Under modulation].



- when $\mu = 1$ [Normal modulation].



- when $\mu > 1$. [Over modulation].



في ساي الى الطارة و راح ال message

بسته $A_{max} > A_c$ و $\mu > 1$

$0 < \mu \leq 1$ في ساي الطارة و راح ال message

• To evaluate modulation index (μ)

(82) $A_{max} = A_c(1 + \mu)$ [From figure].

$A_{min} = A_c(1 - \mu)$

$\rightarrow \frac{A_{max}}{A_{min}} \times \frac{1 + \mu}{1 - \mu} \Rightarrow A_{max} - \mu A_{max} = A_{min} + \mu A_{min}$

$A_{max} - A_{min} = \mu A_{max} + \mu A_{min}$

$\Rightarrow \mu = \frac{A_{max} - A_{min}}{A_{max} + A_{min}}$

$\mu = k_a A_m$ [From $S_{AM}(t)$].

• To evaluate Power.

$S_{AM}(t) = A_c(1 + \mu \cos(2\pi f_m t)) \cos(2\pi f_c t)$

$= A_c \cos(2\pi f_c t) + A_c \mu \cos(2\pi f_m t) \cos(2\pi f_c t)$

$= \underbrace{A_c \cos(2\pi f_c t)}_{P_c} + \underbrace{\frac{A_c \mu}{2} \cos(2\pi (f_c + f_m)t)}_{P_{side1} = P_{usb}}$

$+ \underbrace{\frac{A_c \mu}{2} \cos(2\pi (f_c - f_m)t)}_{P_{side2} = P_{lsb}}$

\therefore (m) μ \rightarrow

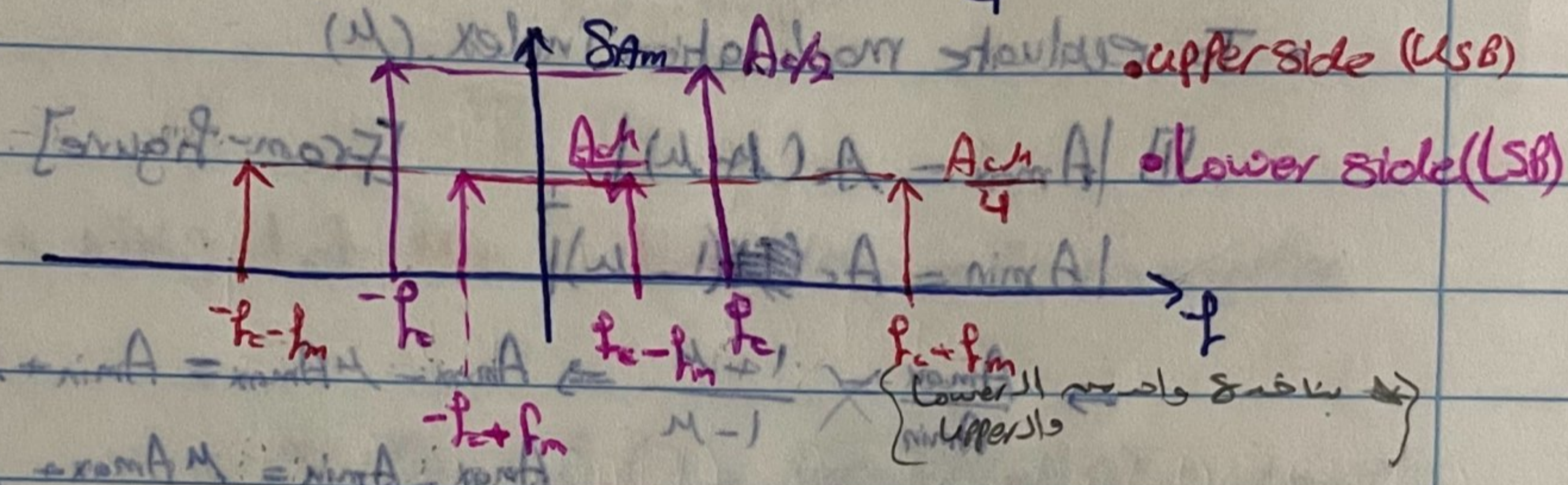
$\mu = \frac{P_{side1} + P_{side2}}{P_c} = \frac{P_{usb} + P_{lsb}}{P_c}$

$\mu = \frac{P_{side1} + P_{side2}}{P_c}$

$\mu = \frac{P_{side1} + P_{side2}}{P_c}$

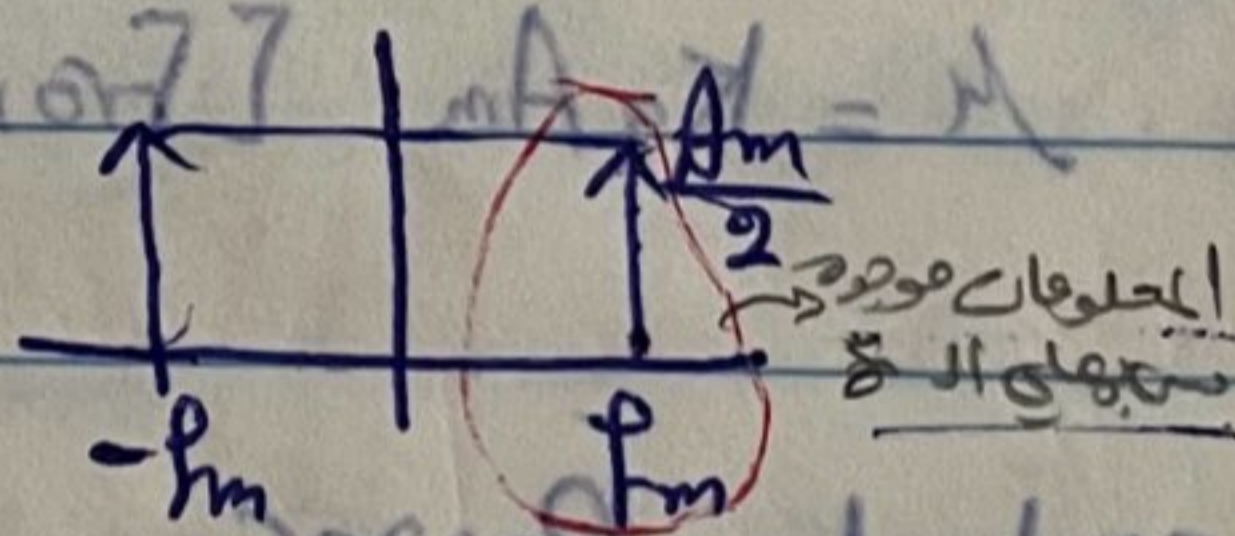
- To evaluate and sketch the spectrum of modulated signal.

$$S_{Am}(f) = \frac{A_c}{2} \delta(f - f_c) + \frac{A_c}{2} \delta(f + f_c) + \frac{A_c \mu}{4} \delta(f - (f_c + f_m)) + \frac{A_c \mu}{4} \delta(f + (f_c + f_m)) + \frac{A_c \mu}{4} \delta(f - (f_c - f_m)) + \frac{A_c \mu}{4} \delta(f + (f_c - f_m))$$



Since $m(t) = A_m \cos(2\pi f_m t)$

$$m(f) = \frac{A_m}{2} \delta(f - f_m) + \frac{A_m}{2} \delta(f + f_m)$$



$$P_{total} = P_c + P_{USB} + P_{LSB}; P_c = \frac{A_c^2}{2}$$

$$P_{USB} = \frac{(A_c \mu / 2)^2}{2}$$

$$P_{LSB} = \frac{(A_c \mu / 2)^2}{2}$$

Power.

بتعدلي انا فصار البوراني فيها كفضله ابي اعرض منها ال Data \Rightarrow efficiency (η):

$$\eta = \frac{P_{sides}}{P_{total}} = \frac{P_{USB} + P_{LSB}}{P_c + P_{USB} + P_{LSB}} \times 100\%$$

$$= \frac{2 \frac{(A_c \mu / 2)^2}{2}}{\frac{A_c^2}{2} + (A_c \mu / 2)^2} \Rightarrow \eta = \frac{\mu^2}{2 + \mu^2} \times 100\%$$

eg. if $m(t) = 2 \cos(20\pi t)$, $c(t) = 4 \cos(100\pi t)$

and $\mu = 20\%$. Evaluate μ .

Now let assume $m(t) = A_m \cos(2\pi f_m t)$

$$\frac{20}{100} = \frac{\mu^2}{2 + \mu^2} \rightarrow \frac{1}{5} \times = \frac{\mu^2}{2 + \mu^2}$$

$$(2 + \mu^2) \times \frac{1}{5} = \mu^2 \rightarrow 2 + \mu^2 = 5\mu^2$$

$$2 = 4\mu^2$$

$$\sqrt{\mu^2} = \sqrt{\frac{1}{2}}$$

$$\mu = \sqrt{0.5}$$

- Evaluate K_a

$$\mu = 0.71$$

$$\mu = K_a A_m \rightarrow 0.71 = K_a \cdot 2$$

$$K_a = 0.35$$

$$\text{if } \mu = 1 \Rightarrow \frac{\mu}{100\%} = \frac{1}{2+1} \times 100\% \Rightarrow \mu = 33\%$$

To evaluate power in time domain

$$P = \frac{A^2}{2}$$

$$\frac{(A_m \mu)^2}{2} = P_m \leftarrow \text{side}$$

(L9)

$$S_{AM}(t) = A_c (1 + k_a m(t)) \cos(2\pi f_c t)$$

Now, Let assume $m(t) = A_m \cos(2\pi f_m t)$.

$$\begin{aligned} \Rightarrow S_{AM}(t) &= A_c (1 + k_a A_m \cos(2\pi f_m t)) \cos(2\pi f_c t) \\ &= A_c (1 + \mu \cos(2\pi f_m t)) \cos(2\pi f_c t) \end{aligned}$$

• Power efficiency.

كفاءة البور الى موجود بالمزيد الى
بحاجي المسح بالنسبة للبور الكلي

$$\eta_{\text{left}} = \frac{P_{\text{sides}}}{P_{\text{total}}} = \frac{P_{\text{sides}}}{P_c + P_{\text{sides}}}$$

$$\Rightarrow S_{AM}(t) = A_c \cos(2\pi f_c t) + A_c \mu \cos(2\pi f_m t) \cos(2\pi f_c t)$$

$$P_c = \underbrace{A_c \cos(2\pi f_c t)}_{\text{Carrier}} + \underbrace{\frac{A_c \mu \cos(2\pi (f_c + f_m)t)}{2}}_{\text{Upper Sideband}}$$

$$+ \underbrace{\frac{A_c \mu \cos(2\pi (f_c - f_m)t)}{2}}_{\text{Lower Sideband}} = P_{\text{sides}}$$

To evaluate power $\begin{cases} \rightarrow \text{Time-domain} \\ \rightarrow \text{freq-domain} \end{cases}$

- In Time domain :-

$$P_c = \frac{A_c^2}{2}$$

$$P_{\text{sides}} \begin{cases} \rightarrow P_{\text{USB}} = \frac{(A_c \mu / 2)^2}{2} \\ \rightarrow P_{\text{LSB}} = \frac{(A_c \mu / 2)^2}{2} \end{cases}$$

\Rightarrow

$$M_{\text{eff}\%} = \frac{2(A_c \mu/2)^2}{\frac{A_c^2}{2} + \frac{2(A_c \mu/2)^2}{2}} \times 100\%$$

$$= \frac{(A_c \mu/2)^2}{\frac{A_c^2}{2} + (\mu A_c/2)^2} \rightarrow \frac{A_c^2 \mu^2 / 4}{\frac{2A_c^2}{2} + \frac{A_c^2 \mu^2}{4}}$$

$$M_{\text{eff}\%} = \frac{\mu^2}{2 + \mu^2} \times 100\%$$

For $\mu = 1$ أفضل حالة في عملية البث (بموجب شروطها)

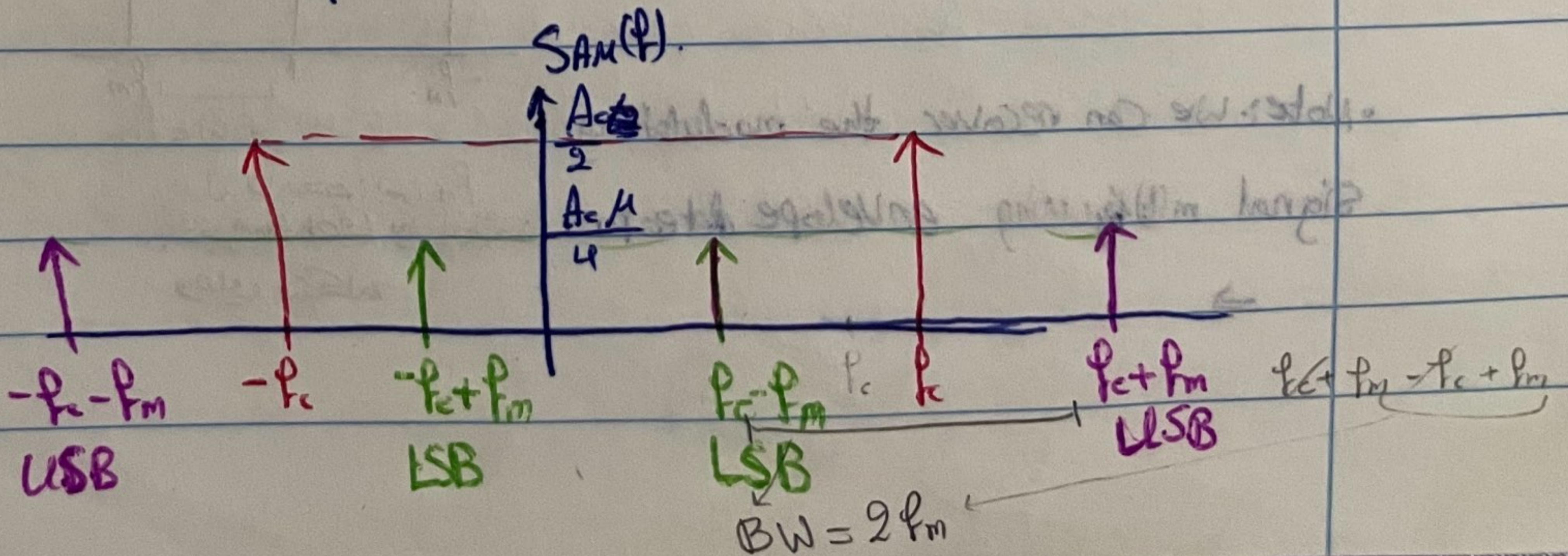
$M_{\text{eff}\%} = 33.33\%$ كل ما كانت M_{eff} عالية كل الحالات البث التي يتجلى فيها المسج سجلت أعلى
Very small!

- In freq domain.

$$S_{AM}(t) = A_c \cos(2\pi f_c t) + \frac{A_c \mu}{2} \cos(2\pi(f_c + f_m)t) + \frac{A_c \mu}{2} \cos(2\pi(f_c - f_m)t)$$

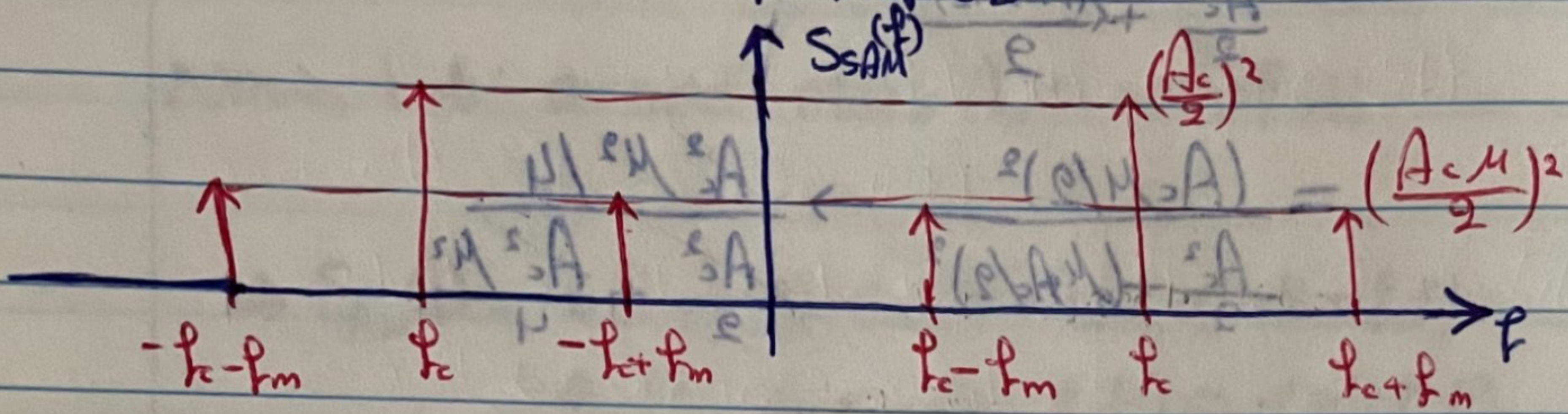
$$\rightarrow S_{AM}(f) = \frac{A_c}{2} \delta(f - f_c) + \frac{A_c}{2} \delta(f + f_c) + \frac{A_c \mu}{4} \delta(f - (f_c + f_m))$$

$$+ \frac{A_c \mu}{4} \delta(f + (f_c + f_m)) + \frac{A_c \mu}{4} \delta(f - (f_c - f_m)) + \frac{A_c \mu}{4} \delta(f + (f_c - f_m))$$



→ To evaluate power efficiency from freq. domain

- Evaluate and plot PSD.



$$S_{SAM}(f) = \left(\frac{A_c}{2}\right)^2 \delta(f - f_c) + \left(\frac{A_c}{2}\right)^2 \delta(f + f_c) + \left(\frac{A_c \mu}{2}\right)^2 \delta(f - (f_c - f_m)) + \left(\frac{A_c \mu}{2}\right)^2 \delta(f + (f_c - f_m)) + \left(\frac{A_c \mu}{2}\right)^2 \delta(f - (f_c + f_m)) + \left(\frac{A_c \mu}{2}\right)^2 \delta(f + (f_c + f_m))$$

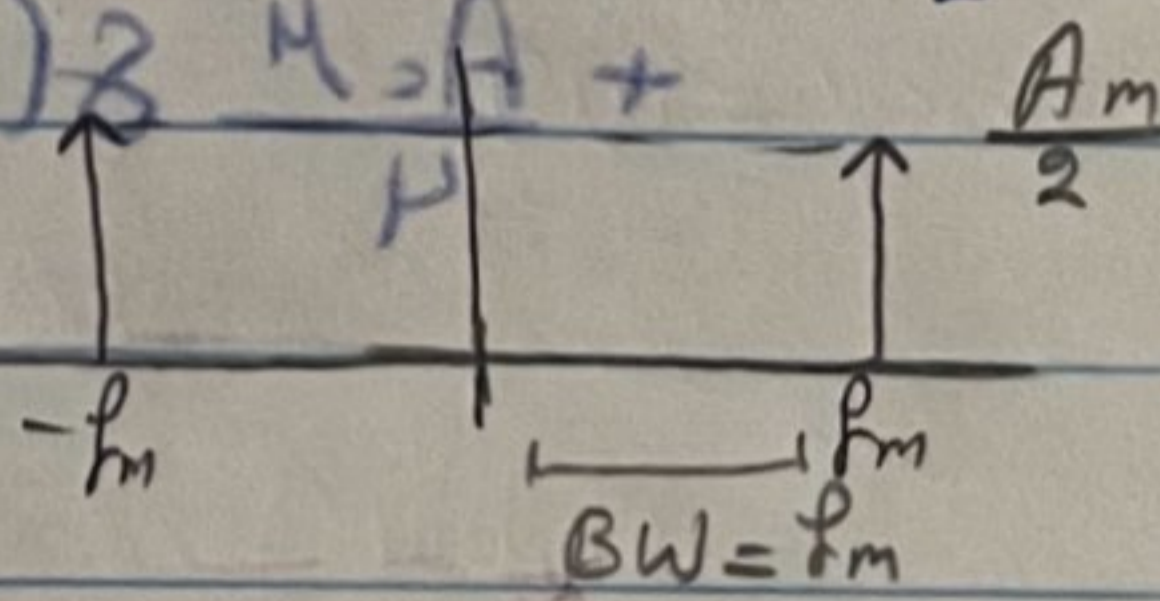
4 انتقارات →

$$\eta_{eff} = \frac{P_{sides}}{P_c + P_{sides}} \times 100\% = \frac{4 \left(\frac{A_c \mu}{4}\right)^2}{2 \left(\frac{A_c}{2}\right)^2 + 4 \left(\frac{A_c \mu}{4}\right)^2} \times 100\%$$

$$\eta_{eff} = \frac{\mu^2}{2 + \mu^2} \times 100\%$$

(Note: Remember:-

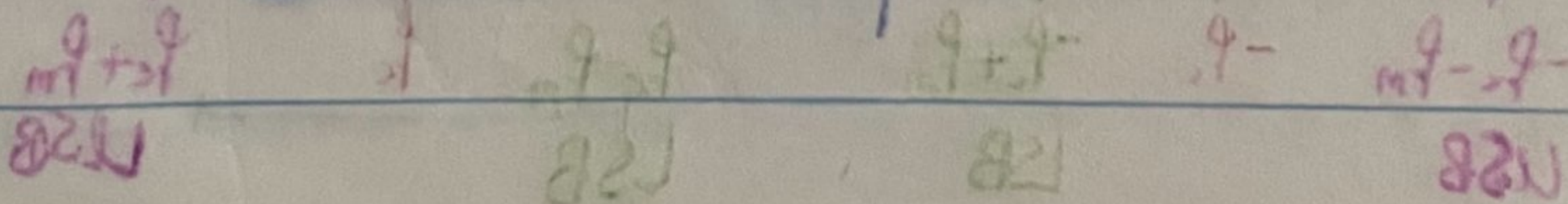
base band signal $m(t) = A_m \cos(2\pi f_m t) \rightarrow M(f) = \frac{A_m}{2} \delta(f - f_m) + \frac{A_m}{2} \delta(f + f_m)$



• Note: We can recover the modulating signal $m(t)$ using envelope detector.

بدل ما نحجز بس f_m بـ (Channel) نصف عرض نطاق وهاي مشكلة.

→



Example if $m(t) = 4\cos(30\pi t)$ and $c(t) = 2\cos(300\pi t)$.

Assume we have normal AM, where the power efficiency at this modulation scheme is 20%. Evaluate the amplitude sensitivity " K_a ".

Ans: For normal AM

$$\eta_{\%} = \frac{\mu^2}{2 + \mu^2} = 0.2$$

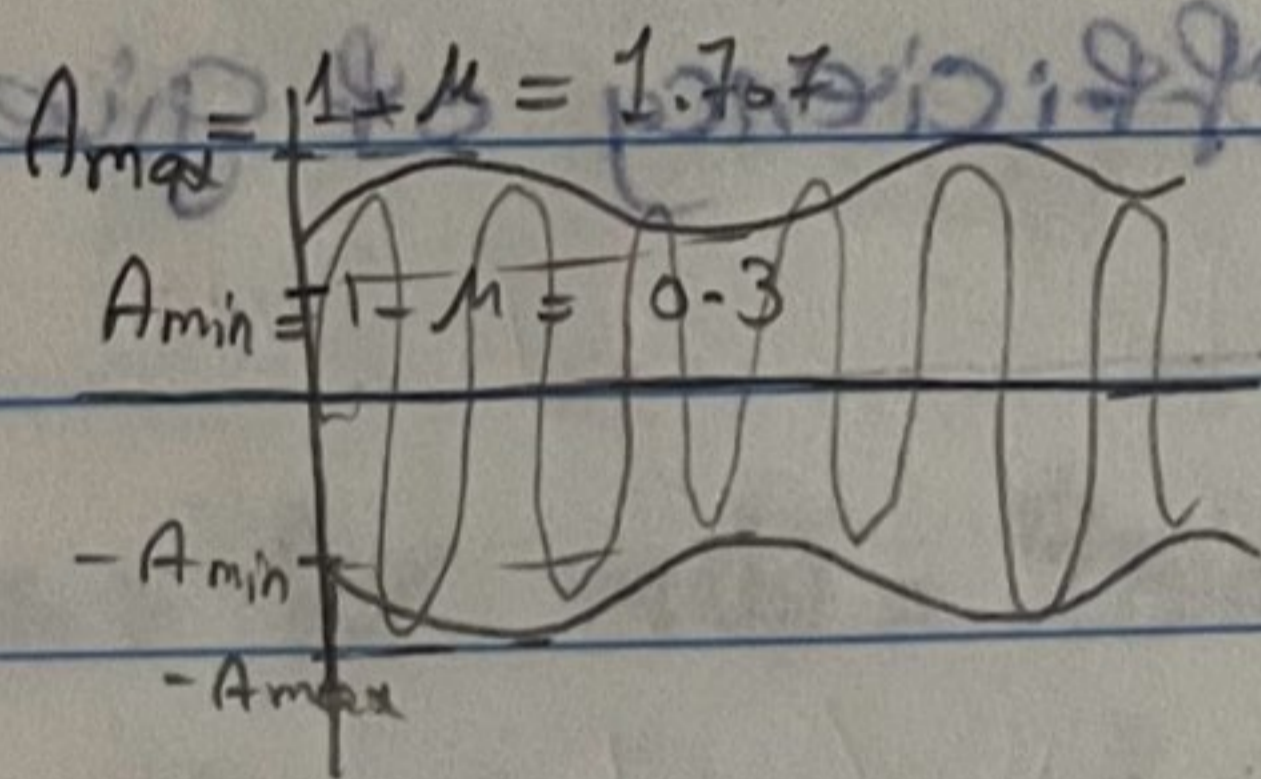
$$0.4 + 0.2\mu^2 = \mu^2$$

$$\sqrt{\frac{0.4}{0.8}} = \frac{\mu}{0.8}$$

$$\Rightarrow \mu = 0.707 \text{ "under"}$$

$$M = K_a A_m \Rightarrow K_a = \frac{M}{A_m} = \frac{0.707}{4}$$

$$\Rightarrow K_a = 0.177$$



Example Consider Normal AM modulation scheme if the modulating signal $m(t) = 2 \cos(20\pi t)$

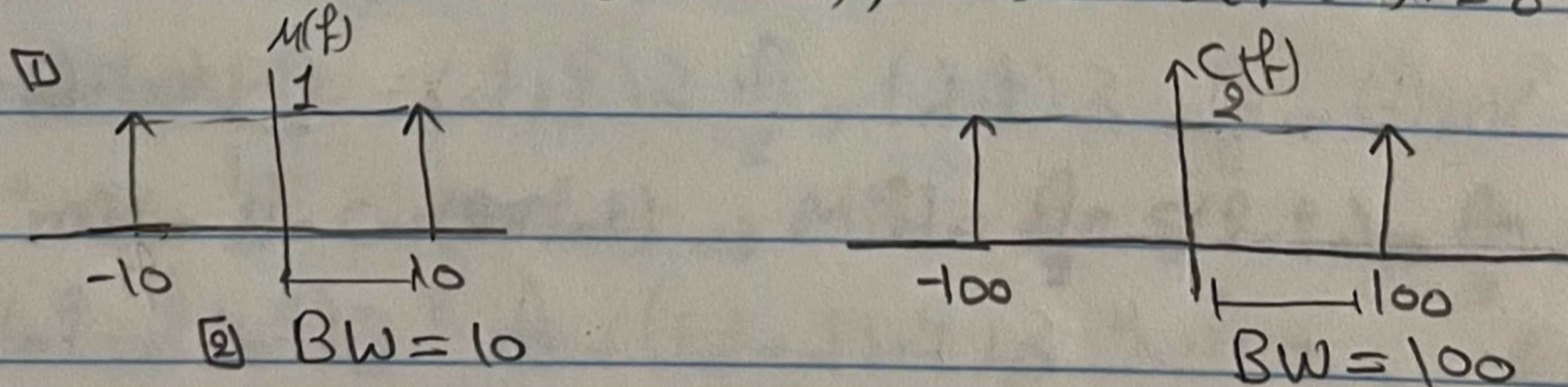
and $c(t) = 4 \cos(200\pi t)$

and $c(t) = 4 \cos(200\pi t)$

- Evaluate and plot the spectrum of modulating signal & Carrier signal
- Evaluate the BW of modulating & carrier signals.
- Write the expression of the modulated signal. Assume the amplitude sensitivity $K_a = 1$
- Evaluate & plot the spectrum of modulated signal
- Evaluate the BW of modulated signal
- Evaluate the power efficiency of given modulation scheme.

Ans: For $m(t) = 2 \cos(20\pi t)$ & $c(t) = 4 \cos(200\pi t)$

$$M(f) = \delta(f-10) + \delta(f+10), \quad C(f) = 2\delta(f-100) + 2\delta(f+100)$$

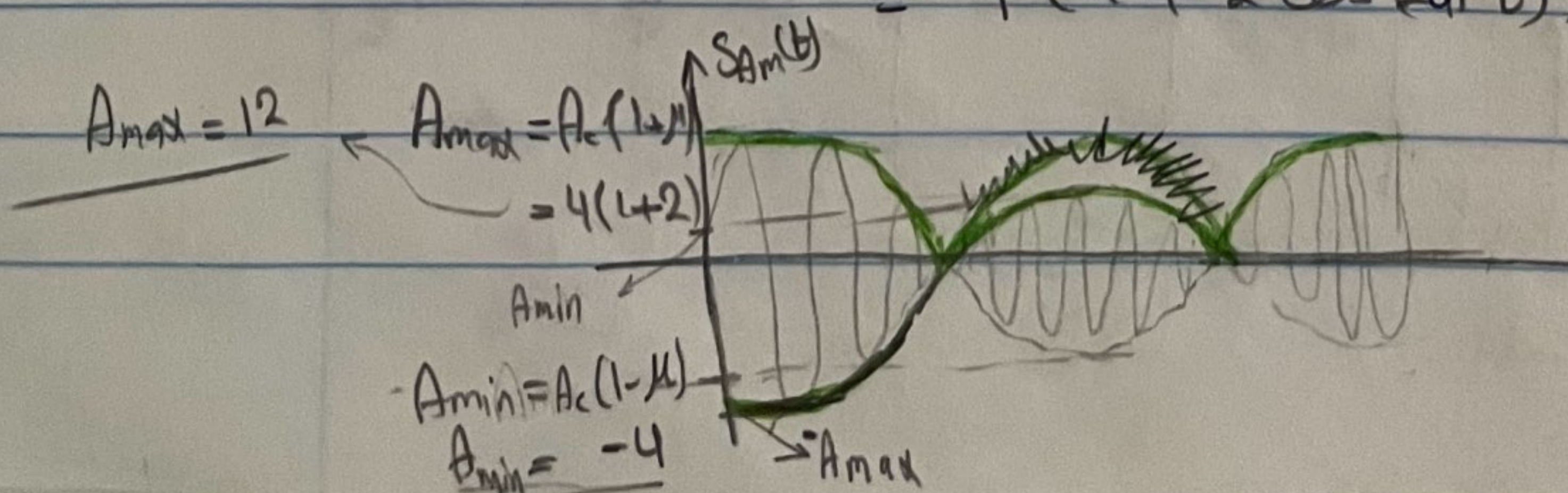


Since we have Normal AM

$$S_{AM}(t) = A_c(1 + K_a m(t)) \cos(2\pi f_c t)$$

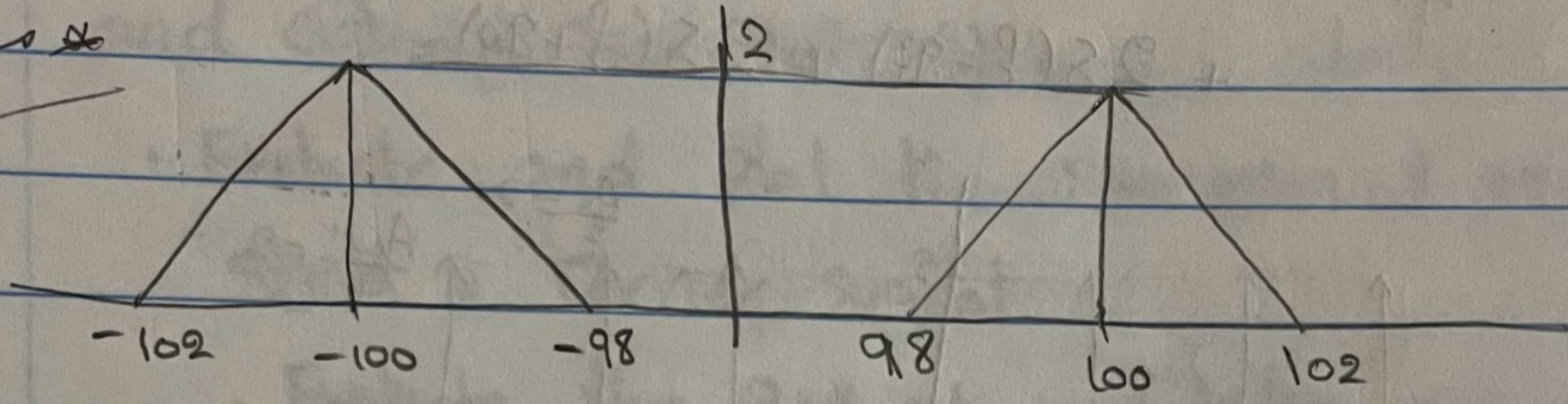
$$= 4(1 + 2 \cos(20\pi t)) \cos(200\pi t)$$

$$\mu = K_a A_m = (1)(2) = 2$$



$$S_{AM}(t) = 4 \cos(200\pi t) + 8 \operatorname{sinc}^2(2t) \cos(200\pi t)$$

$$S(f) = 2\delta(f-100) + 2\delta(f+100) + 2\Lambda\left(\frac{1}{2}(f-100)\right) + 2\Lambda\left(\frac{1}{2}(f+100)\right)$$



$$BW = 4.$$

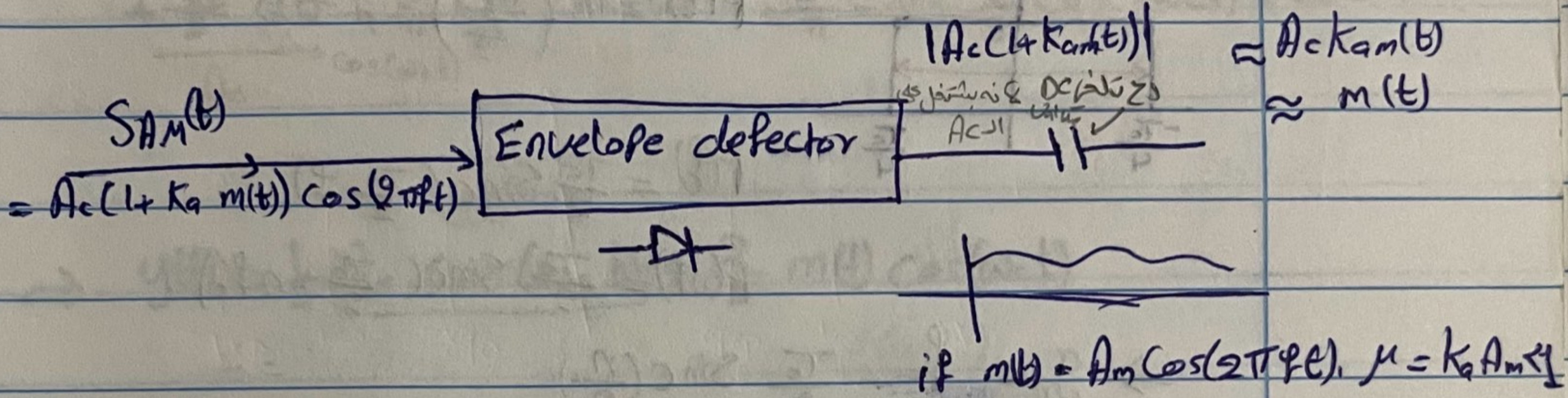
$$M_{\text{eff}} = \frac{\mu^2}{2 + \mu^2} = \frac{2^2}{2 + 2^2}$$

$$\Rightarrow M_{\text{eff}} = 66.6\%$$

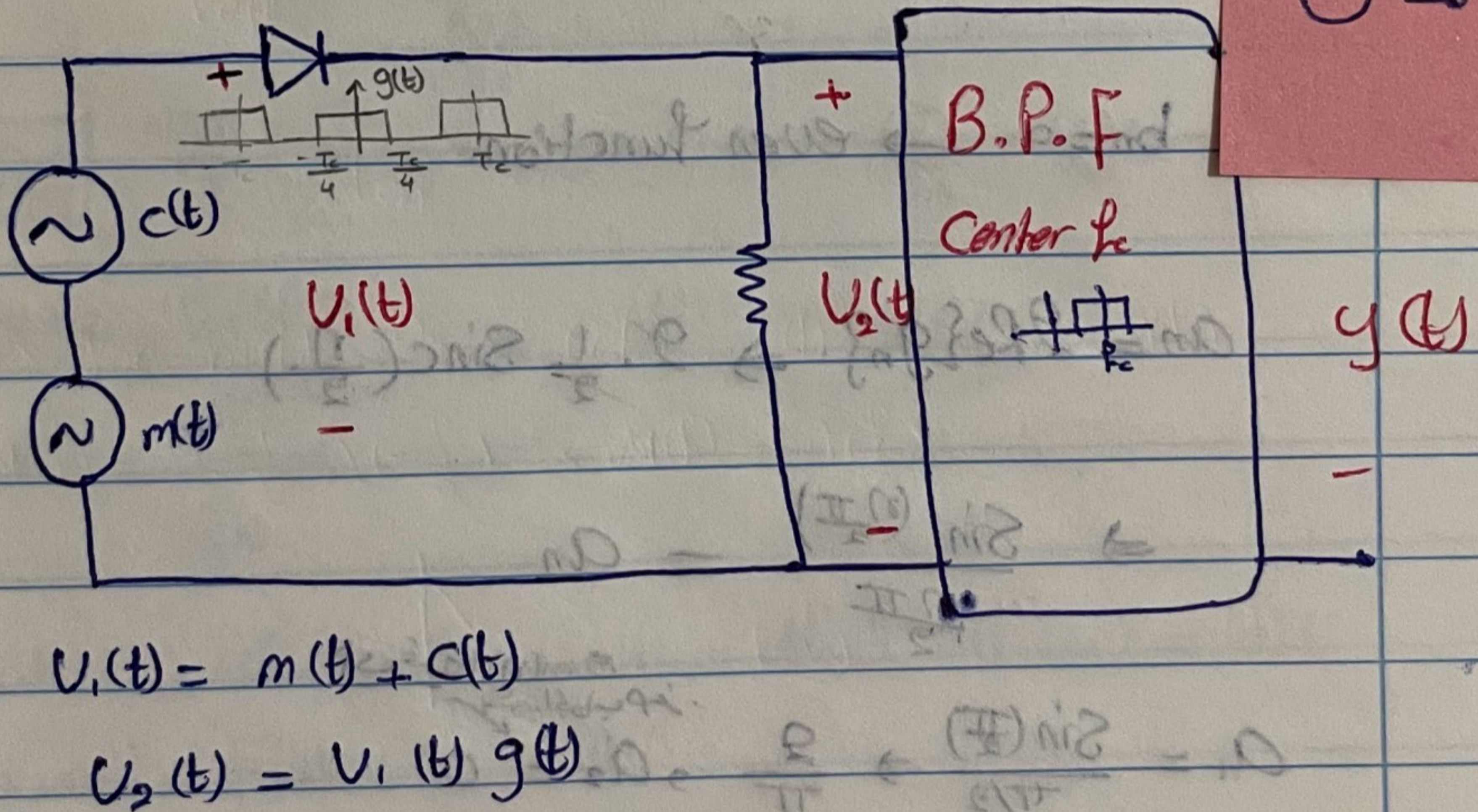
Ans for m(f) = 2 cos(200πt), (f) sinc²(2t) = (f) m(f) = 2 cos(200πt)

(L10)
 [5] New.

• Note: we can recover the modulation signal $m(t)$, using envelope detector.



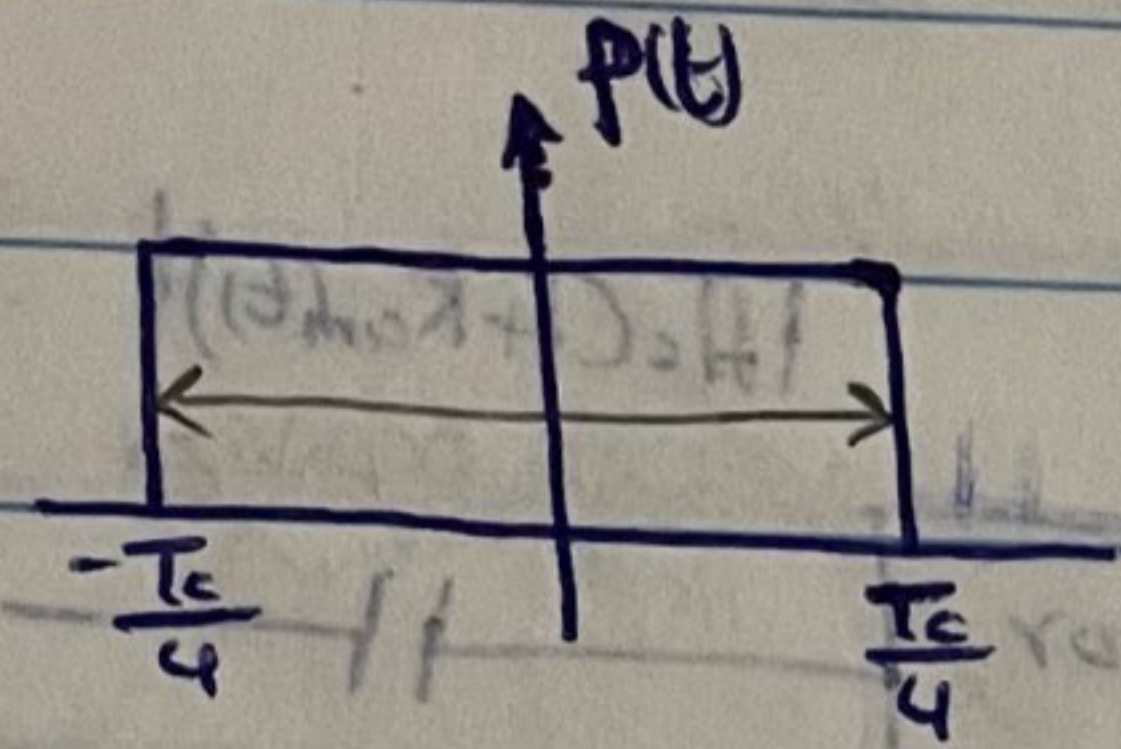
≡ Generation Normal AM.



Since $g(t)$ is periodic signal \rightarrow We can express $g(t)$ as complex exponential Fourier series or Trigonometric coefficient Fourier series.

by Exponential Fourier Series.

$$g(t) = \sum_{n=-\infty}^{\infty} g_n e^{jn\omega_c t} ; g_n = \int_c P(t) e^{-jn\omega_c t} dt$$



$$P(t) = \Pi\left(\frac{t}{T_c/2}\right) ; \tau = \frac{T_c}{2}$$

$$P(f) = \frac{T_c}{2} \text{sinc}\left(\frac{T_c}{2} f\right)$$

$$P(nf) = \frac{T_c}{2} \text{sinc}\left(\frac{T_c}{2} \cdot n f_c\right)$$

$$\rightarrow g_n = \int_c \frac{T_c}{2} \text{sinc}\left(\frac{n}{2}\right)$$

$$\rightarrow g_n = \frac{1}{2} \text{sinc}\left(\frac{n}{2}\right)$$

$$a_0 = g_0 = \frac{1}{2} \text{sinc}(0) \rightarrow a_0 = \frac{1}{2}$$

$b_n = 0 \rightarrow$ even function.

$$a_n = 2 \text{Re}\{g_n\} \Rightarrow 2 \cdot \frac{1}{2} \text{sinc}\left(\frac{n}{2}\right)$$

$$\Rightarrow \frac{\sin\left(\frac{n\pi}{2}\right)}{\frac{n\pi}{2}} = a_n$$

$$a_1 = \frac{\sin\left(\frac{\pi}{2}\right)}{\pi/2} \Rightarrow \frac{2}{\pi}, a_2 = 0$$

$$a_3 = \frac{\sin\left(\frac{3\pi}{2}\right)}{3\pi/2} \Rightarrow -\frac{2}{3\pi}, a_4 = 0$$

$$g(t) = a_0 + \sum_{n=1}^{\infty} a_n \cos(n\omega_c t) + \sum_{n=1}^{\infty} b_n \sin(n\omega_c t)$$

$$g(t) = \frac{1}{2} + \frac{2}{\pi} \left(\cos(\omega_c t) - \frac{1}{3} \cos(3\omega_c t) + \dots \right)$$

$$V_2(t) = (m(t) + c(t)) \left[\frac{1}{2} + \frac{2}{\pi} (\cos(\omega_c t) - \frac{1}{3} \cos(3\omega_c t) + \dots) \right]$$

$$= \frac{1}{2} m(t) + \frac{2}{\pi} m(t) \cos(\omega_c t) + \frac{2}{\pi} m(t) \cdot \left(-\frac{1}{3}\right) \cos(3\omega_c t) + \dots$$

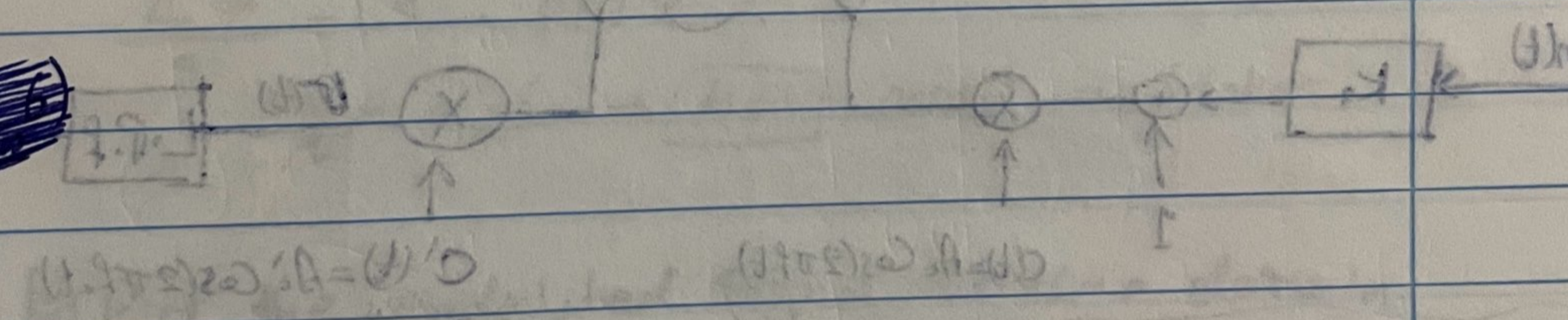
$$+ \frac{1}{2} c(t) + \frac{2}{\pi} c(t) \cos(\omega_c t) + \frac{2}{\pi} c(t) \cdot \left(-\frac{1}{3}\right) \cos(3\omega_c t) + \dots$$

$\underbrace{\hspace{1.5cm}}_{A_c} \xrightarrow{\cos(\omega_c t)}$

$$\Rightarrow y(t) = \frac{1}{2} A_c \overset{c(t)}{\cos(\omega_c t)} + \frac{2}{\pi} m(t) \cos(\omega_c t)$$

$$y(t) = \frac{A_c}{2} \cos(\omega_c t) \left[1 + \frac{4}{\pi A_c} m(t) \right]$$

Since $S_{AM}(t) = A_c (1 + k_a m(t)) \overset{2\pi f_c}{\cos(\omega_c t)}$

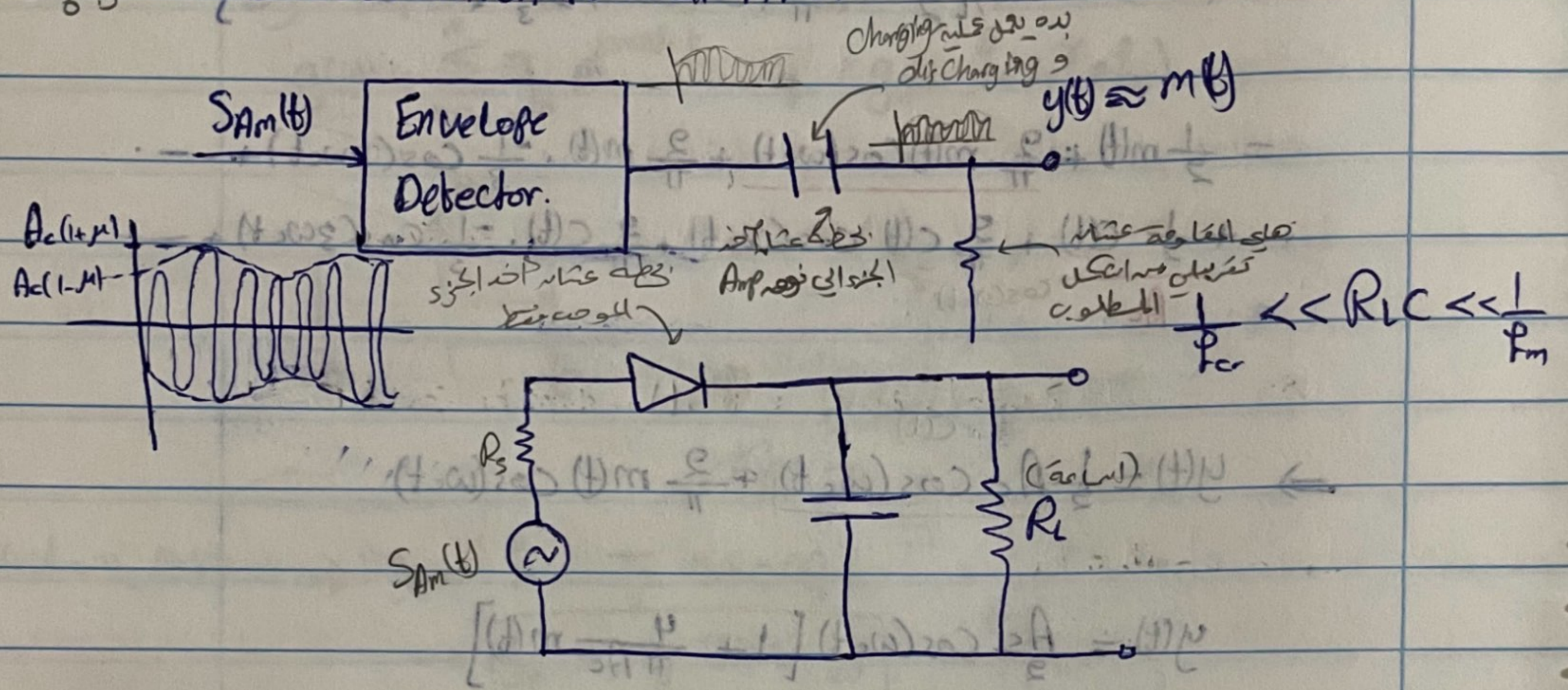


7.9.1

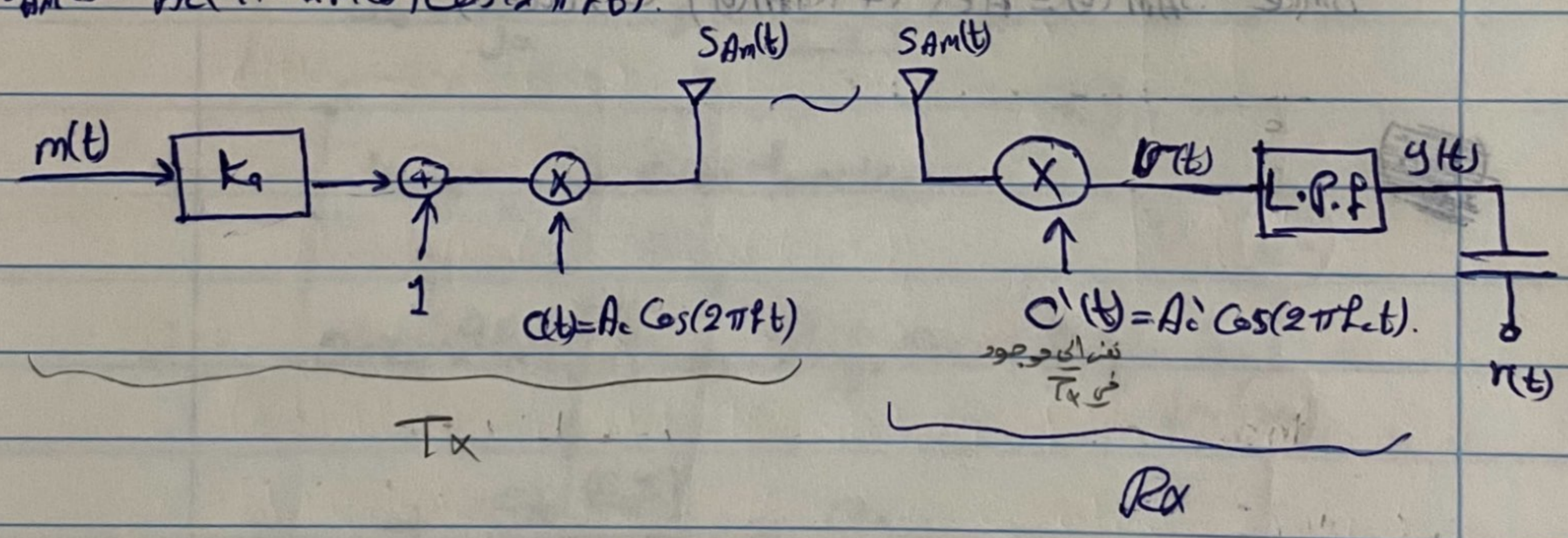
AM Modulation Efficiency
 Efficiency = $\frac{P_m}{P_m + P_c}$
 Efficiency = $\frac{m^2}{m^2 + 2}$

(E6) new

Demodulation Normal AM



$S_{AM}(t) = A_c(1 + k_a m(t)) \cos(2\pi f_c t)$



$$v(t) = S_{AM}(t) \cdot c'(t) = A_c(1 + k_a m(t)) \cos(2\pi f_c t) \cdot A_c' \cos(2\pi f_c t)$$

$$= A_c A_c' (1 + k_a m(t)) \left[\frac{1}{2} + \frac{1}{2} \cos(4\pi f_c t) \right]$$

$$\Rightarrow v(t) = \frac{A_c A_c'}{2} (1 + k_a m(t)) + \frac{A_c A_c'}{2} (1 + k_a m(t)) \cos(4\pi f_c t)$$

↓ DC value ←
 ← Constant

L.P.F

$$\Rightarrow y(t) = \frac{1}{2} A_c A_c' (1 + k_a m(t))$$

صنعتنا على قيمة نغنا (f_c) ونغنا الأجلية نغنا

Example The amplitude of sinusoidal carrier is

modulated by a single sinusoidal to obtain the

amplitude modulated signal $S(t) = 1.5 \cos(900\pi t) + 3 \cos(1000\pi t) + 1.5 \cos(1100\pi t)$

Note: $S_{AM}(t) = A_c (1 + K_a m(t)) \cos(2\pi f_c t) = A_c \cos(2\pi f_c t) + K_a m(t) \cos(2\pi f_c t)$

1) Evaluate the modulation index

By using $S_{AM}(t) = A_c \cos(2\pi f_c t) + K_a m(t) \cos(2\pi f_c t)$ and

$m(t) = A_m \cos(2\pi f_m t)$

$\rightarrow S_{AM} = A_c \cos(2\pi f_c t) + A_c K_a A_m \cos(2\pi f_m t) \cos(2\pi f_c t)$

$$= A_c \cos(2\pi f_c t) + \frac{A_c \mu}{2} \cos(2\pi(f_c + f_m)t) + \frac{A_c \mu}{2} \cos(2\pi(f_c - f_m)t)$$

$$\Rightarrow A_c = 3$$

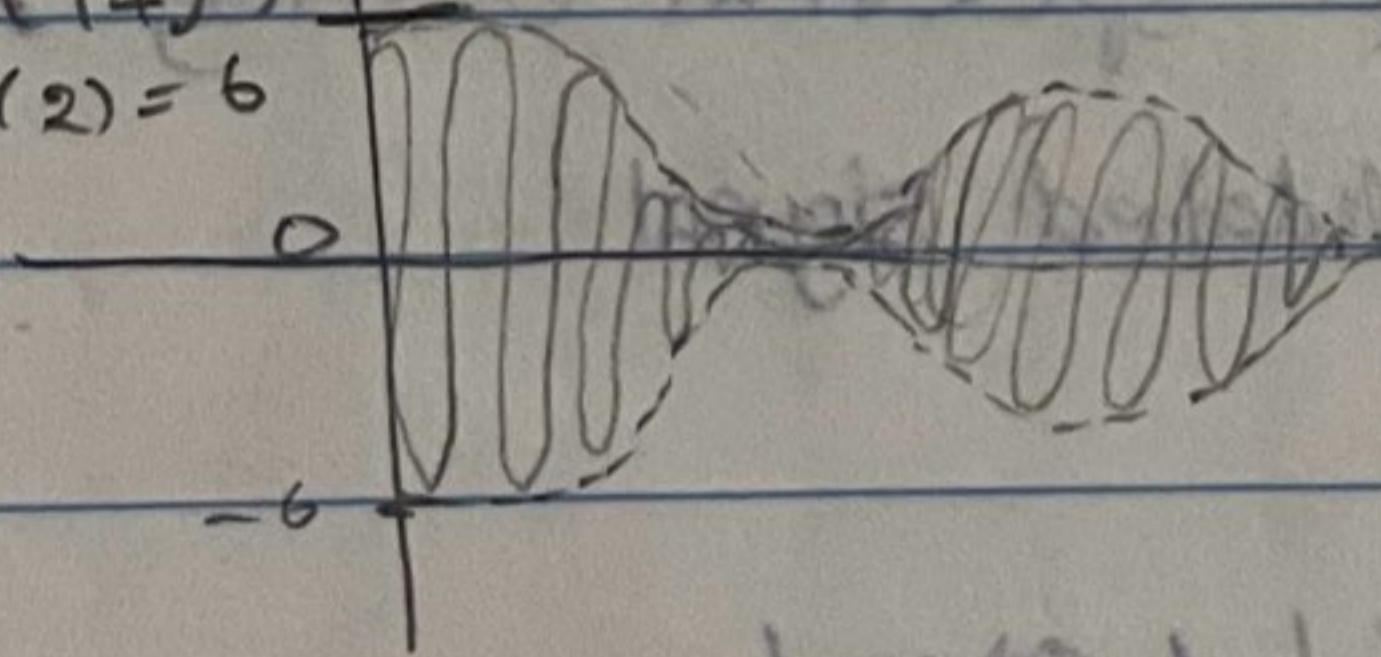
$$\frac{A_c \mu}{2} = 1.5, A_c = 3$$

$$\frac{3}{2} \mu = 1.5 \Rightarrow \mu = 1 \text{ normal modulation}$$

2) Plot the modulated signal in time domain.

Since $\mu = 1$, $A_{max} = A_c(1 + \mu) = 3(1 + 1) = 6$

$$\frac{A_c(1 + \mu)}{2} = 3(2) = 6$$



$$A_{min} = A_c(1 - \mu)$$

$$= 3(1 - 1) \Rightarrow A_{min} = 0$$

3] Evaluate and plot the spectrum of message & carrier signal. assume $k_a = 1$

From modulated signal given in our example -

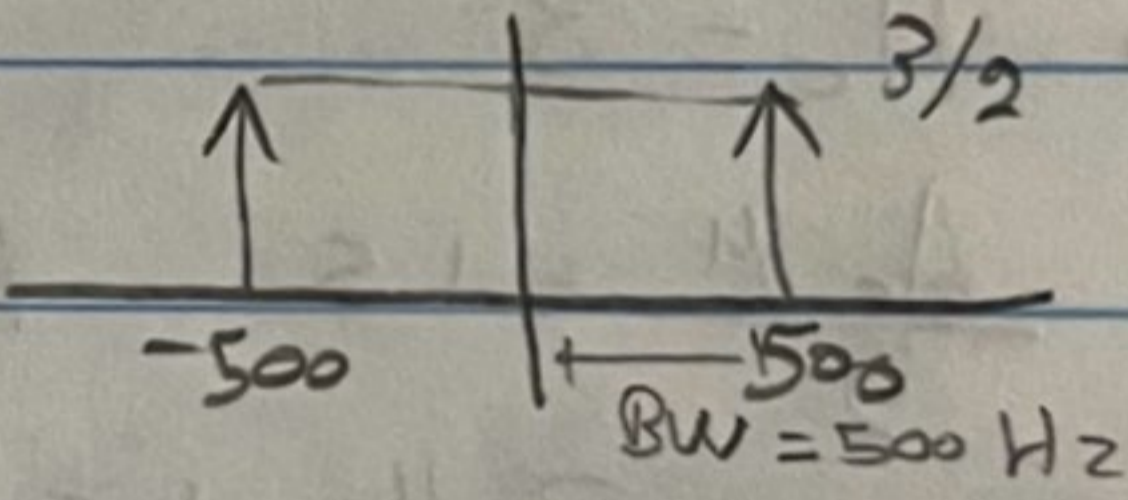
$$S_{AM}(t) = 1.5 \cos(900\pi t) + 3 \cos(1000\pi t) + 1.5 \cos(1100\pi t)$$

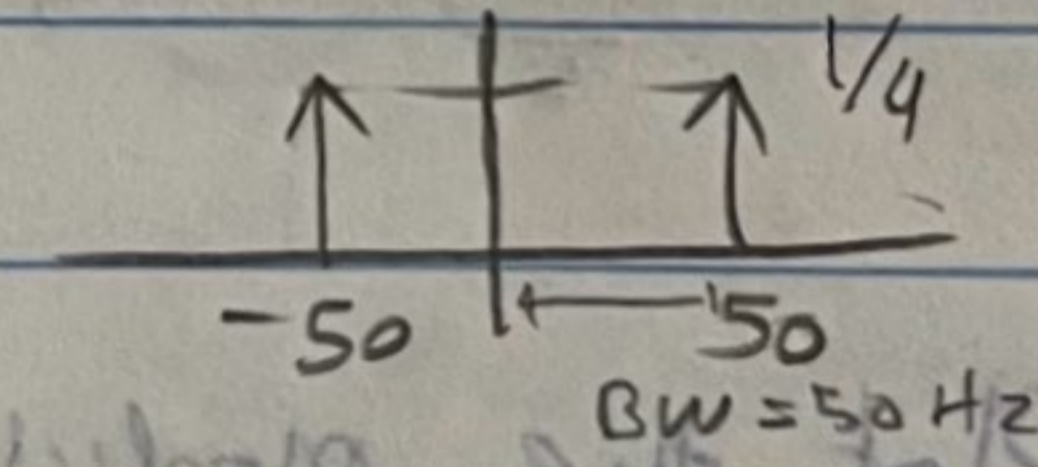
$2\pi(f_c - f_m)$ carrier $M = k_a A_m$ $2\pi(f_c + f_m) = 1100\pi$
 500 $f_c + f_m = 550$

$$C(t) = A_c \cos(2\pi f_c t) = 3 \cos(1000\pi t) \Rightarrow f_m = 50$$

$$M = k_a A_m \Rightarrow A_m = \frac{1}{2}$$

$$m(t) = A_m \cos(2\pi f_m t) = \frac{1}{2} \cos(100\pi t)$$

$$C(f) = \frac{3}{2} (\delta(f-500) + \delta(f+500))$$


$$m(f) = \frac{1}{4} (\delta(f-50) + \delta(f+50))$$


4] Evaluate and plot the spectrum of modulated signal

5] Evaluate and plot the power spectral density for carrier, message and modulated signal

6] Evaluate the M

7] Evaluate the BW of modulated signal.

8] Draw the demodulator Block diagram to recover $m(t)$.

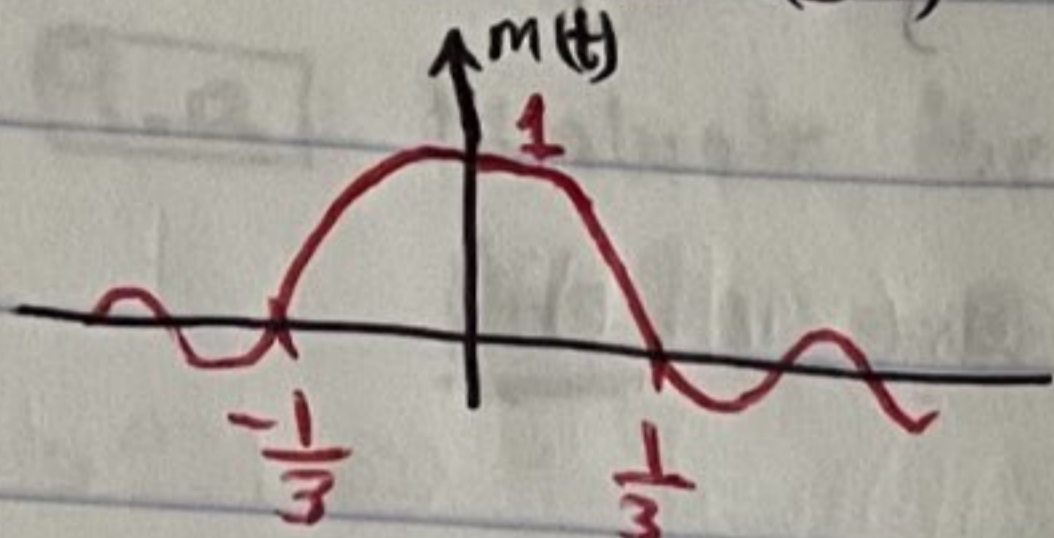
Examples on Normal Am.

(L7) [1]

Example 1 Consider the message signal $m(t) = \text{sinc}^2(3t)$ and carrier signal, $c(t) = 3\cos(200\pi t)$ are applied to a modulator that generate Normal AM.

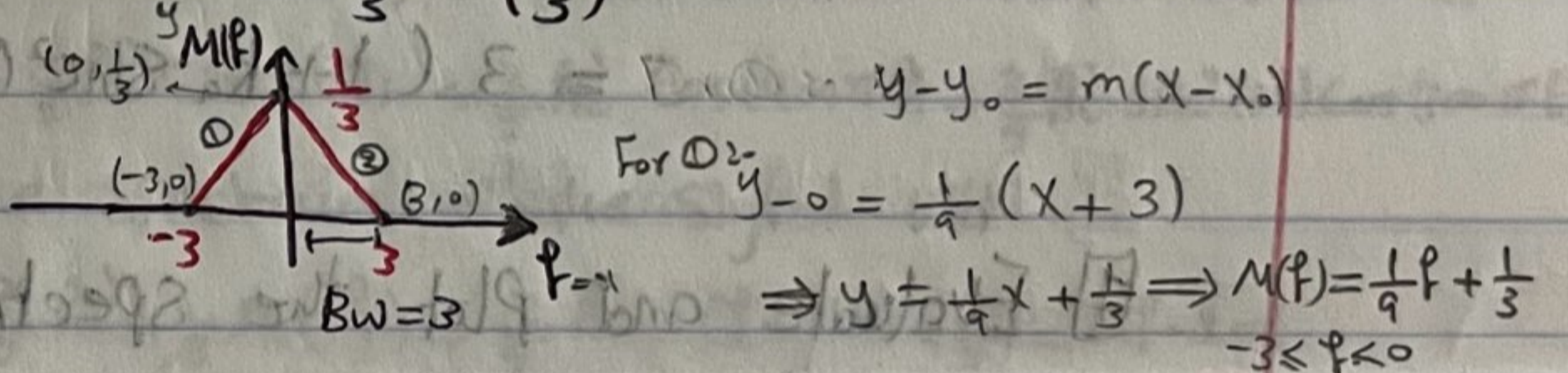
[1] sketch the message signal (modulating signal) in time domain.

Ans: $m(t) = \text{sinc}^2(3t)$



[2] Evaluate & plot the spectrum of the modulating signal

Ans: $m(t) = \text{sinc}^2(3t) \xrightarrow{f} M(f) = \frac{1}{3} \wedge \left(\frac{f}{3}\right)$



[3] Evaluate the Energy spectral density and the total energy

Ans:

$$\text{ESD} \Rightarrow G_M(f) = |M(f)|^2$$

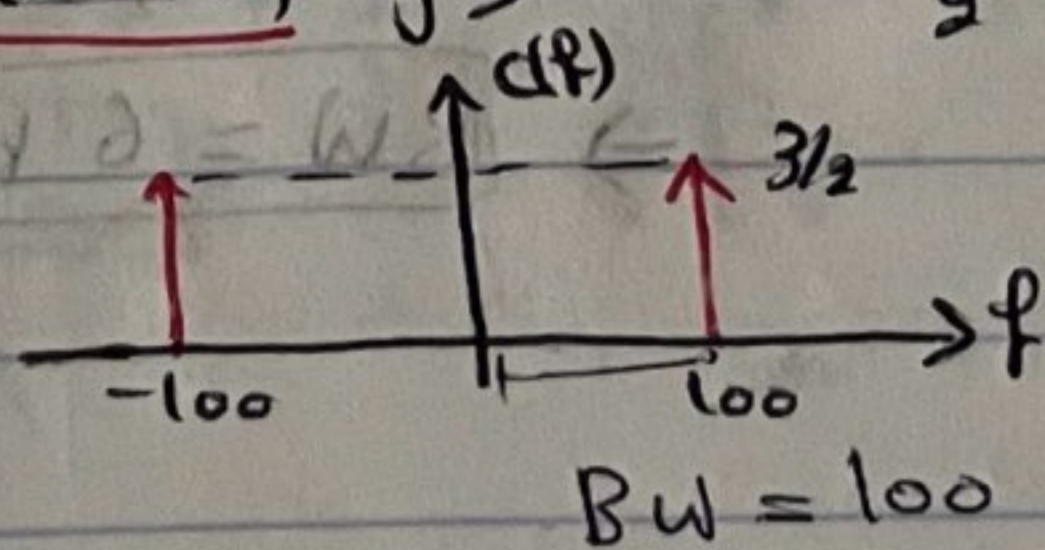
$$|M(f)|^2 = \begin{cases} \left(\frac{1}{3}f + \frac{1}{3}\right)^2, & -3 \leq f < 0 \\ \left(-\frac{1}{3}f + \frac{1}{3}\right)^2, & 0 \leq f < 3 \end{cases}$$

$$E = \int_{-3}^3 |M(f)|^2 df = \int_{-3}^0 \left(\frac{1}{3}f + \frac{1}{3}\right)^2 df + \int_0^3 \left(-\frac{1}{3}f + \frac{1}{3}\right)^2 df$$

[4] Evaluate and plot the spectrum of the carrier signal.

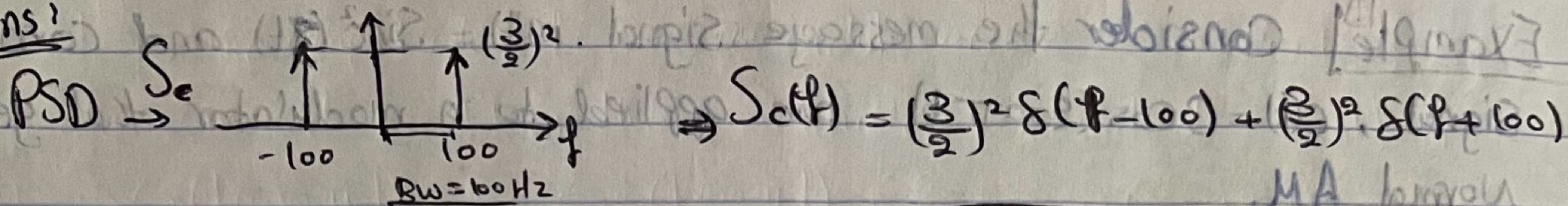
Ans: $c(t) = 3\cos(200\pi t) \xrightarrow{f} C(f) = \frac{3}{2} \delta(f-100) + \frac{3}{2} \delta(f+100)$

Periodic signal
→ Power signal



5) Evaluate the average power for carrier signal.

Ans:



$$S_c(f) = (\frac{3}{2})^2 \delta(f-100) + (\frac{3}{2})^2 \delta(f+100)$$

$$P_{total} = (\frac{3}{2})^2 + (\frac{3}{2})^2 \Rightarrow 2 \cdot \frac{9}{4} \Rightarrow \boxed{P_{tot} = \frac{9}{2} \text{ W}}$$

or we can evaluate the total power by using time domain.

Since $c(t) = 3 \cos(200\pi t)$

$$P_{tot} = \frac{(3)^2}{2} \Rightarrow P_{tot} = \frac{9}{2} \text{ W}$$

6) Write the expression of the modulated signal in time domain.

Ans: Since we have normal AM.

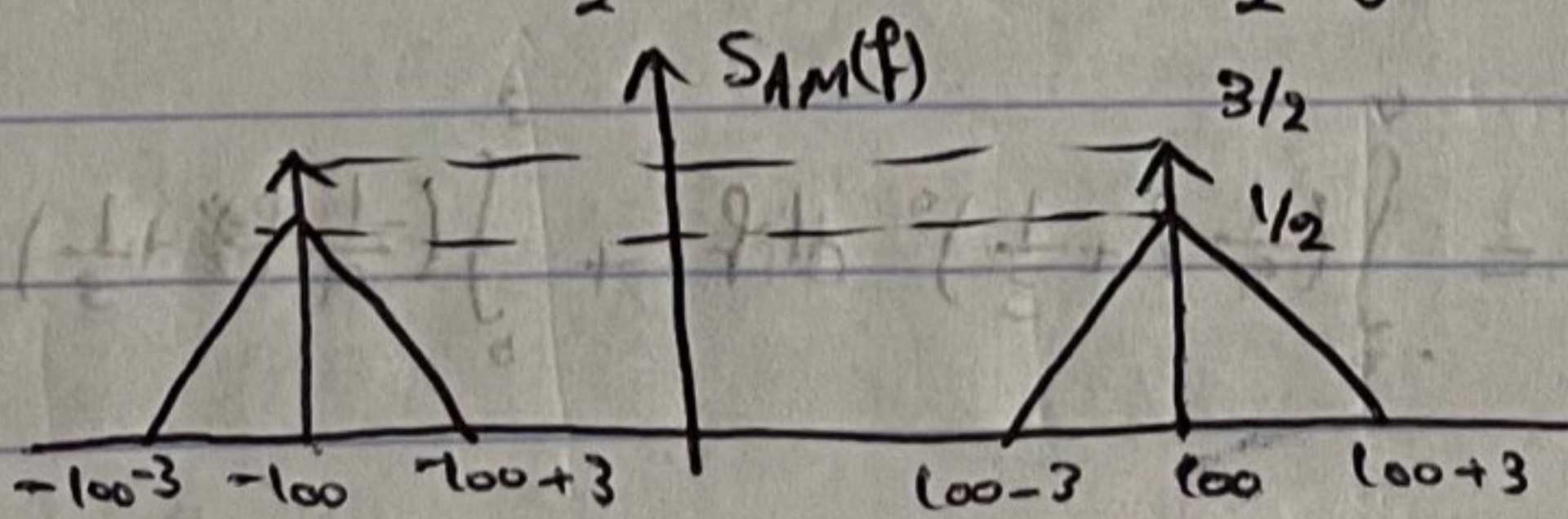
$$S_{AM}(t) = A_c (1 + K_a m(t)) \cos(2\pi f_c t) = 3 (1 + K_a \sin^2(3t)) \cos(200\pi t)$$

7) Evaluate and plot the spectrum of the modulated signal; assume unity of the amplitude sensitivity ($K_a=1$).

Ans:

$$S_{AM}(t) = 3(1 + \sin^2(3t)) \cos(200\pi t) = 3 \cos(200\pi t) + 3 \sin^2(3t) \cos(200\pi t)$$

$$S_{AM}(f) = \frac{3}{2} \delta(f-100) + \frac{3}{2} \delta(f+100) + \frac{3}{2} \cdot \frac{1}{3} \Lambda(\frac{1}{3}(f-100)) + \frac{3}{2} \cdot \frac{1}{3} \Lambda(\frac{1}{3}(f+100))$$



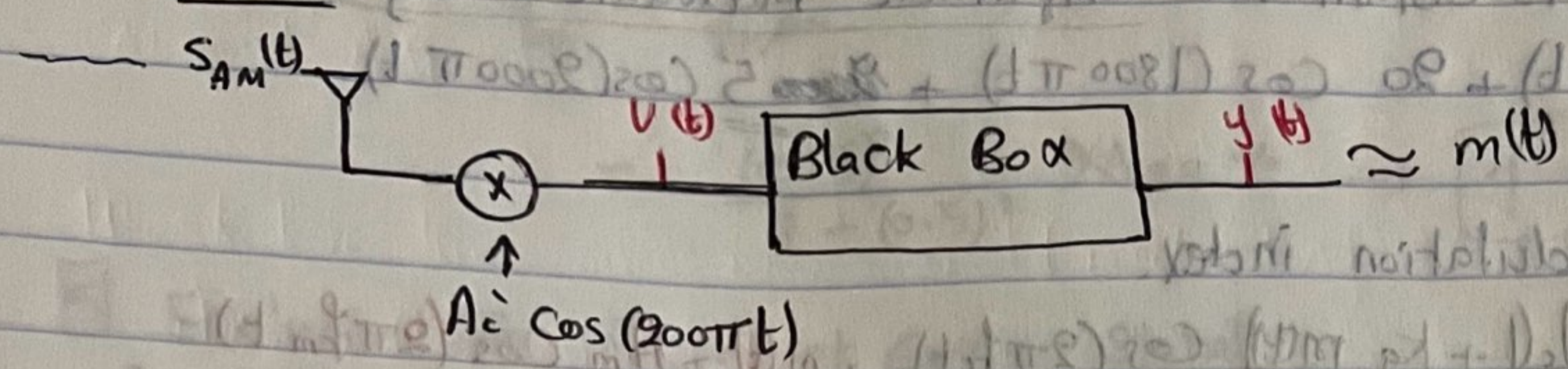
8) Evaluate the Bandwidth of modulated signal

Ans: $BW = (100+3) - (100-3)$

$$\Rightarrow \boxed{BW = 6 \text{ Hz}} = 2f_m$$

Q Now, Consider the following demodulated schem for normal AM.

Ans:



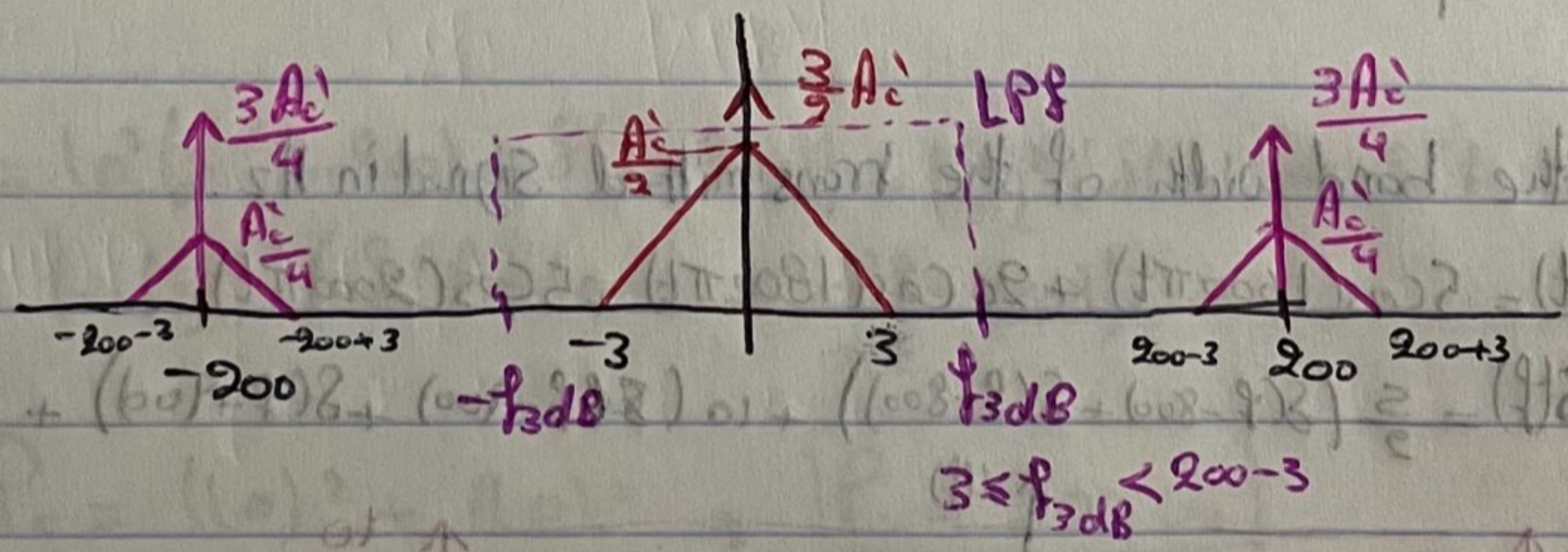
Q.a Evaluate the signal V(t) in time domain. (k_a = 1).

Ans. $V(t) = s_{AM}(t) \cdot A_c \cos(2\pi f_c t)$

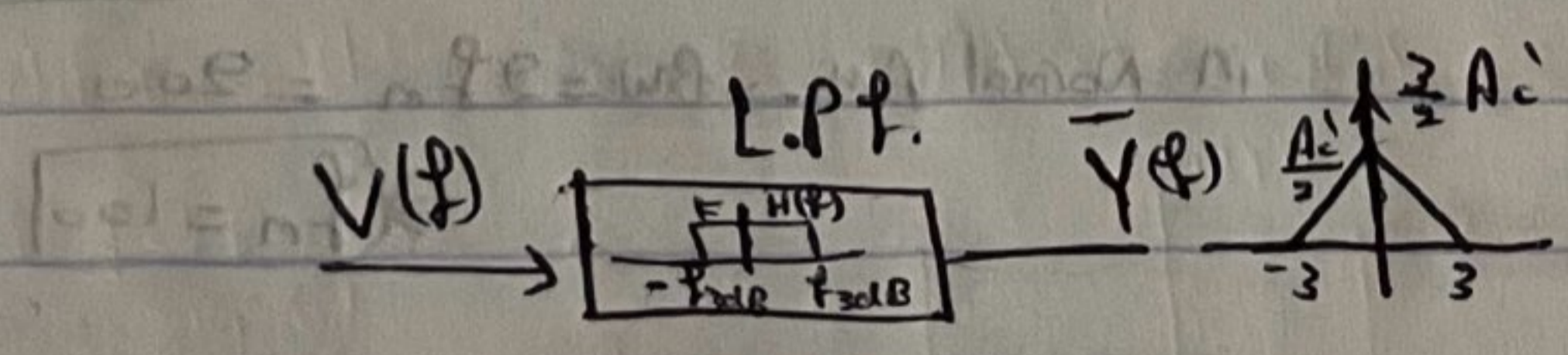
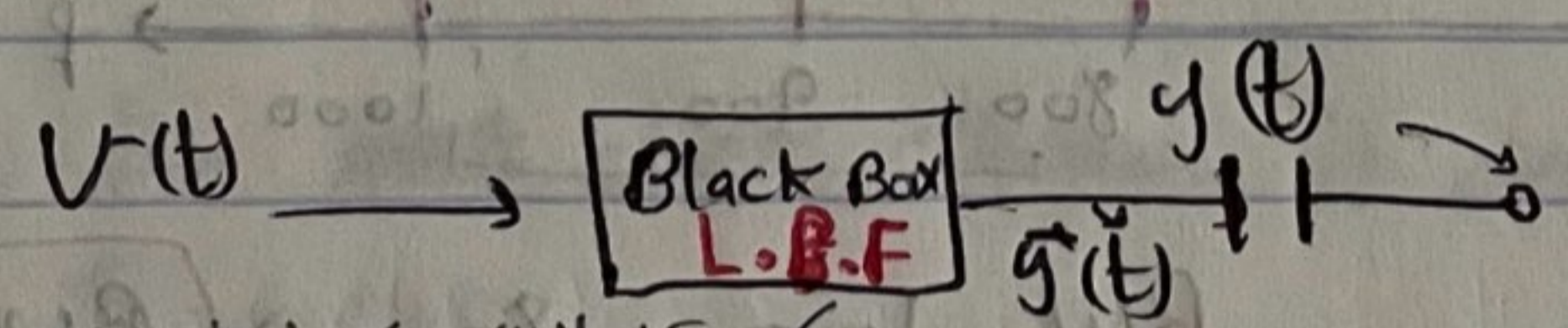
$$\begin{aligned}
 &= [3(1 + \text{sinc}^2(3t)) \cos(200\pi t)] A_c \cos(200\pi t) \\
 &= 3A_c (1 + \text{sinc}^2(3t)) \cos^2(200\pi t) \\
 &= 3A_c (1 + \text{sinc}^2(3t)) \left[\frac{1}{2} + \frac{1}{2} \cos(400\pi t) \right] \\
 &V(t) = \frac{3A_c}{2} (1 + \text{sinc}^2(3t)) + \frac{3A_c}{2} (1 + \text{sinc}^2(3t)) \cos(400\pi t) \\
 &= \frac{3}{2} A_c + \frac{3}{2} A_c \text{sinc}^2(3t) + \frac{3}{2} A_c \cos(400\pi t) + \frac{3}{2} A_c \text{sinc}^2(3t) \cos(400\pi t)
 \end{aligned}$$

Q.b Evaluate and plot the spectrum of the signal V(t)

$$\begin{aligned}
 V(f) &= \frac{3}{2} A_c \delta(f) + \frac{3}{2} A_c \cdot \frac{1}{3} \Lambda\left(\frac{f}{3}\right) + \frac{3}{2} A_c \delta(f-200) + \frac{3}{2} A_c \delta(f+200) \\
 &+ \frac{3}{4} A_c \cdot \frac{1}{3} \Lambda\left(\frac{f-200}{3}\right) + \frac{3}{4} A_c \cdot \frac{1}{3} \Lambda\left(\frac{f+200}{3}\right)
 \end{aligned}$$



To obtain $y(t) \approx m(t)$



$$\begin{aligned}
 Y(f) &= \frac{3}{2} A_c \delta(f) + \frac{A_c}{2} \Lambda\left(\frac{f}{3}\right) \\
 y(t) &= \frac{3}{2} A_c + \frac{A_c}{2} \cdot 3 \text{sinc}^2(3t)
 \end{aligned}$$

D value

بدراسة قيمتها وحصص على
 بعد ما نضيف ال capacitor
 $y(t) = \frac{A_c}{2} \cdot 3 \text{sinc}^2(3t)$ \Rightarrow if $k = \frac{1}{\frac{A_c}{2} \cdot 3} \Rightarrow y(t) \approx m(t)$
 بدراسة قيمتها وحصص على
 بعد ما نضيف ال capacitor
 بدراسة قيمتها وحصص على

(L7) 2

Example | The amplitude of a sinusoidal carrier is modulated by a single sinusoid to obtain the amplitude modulated signal → Normal AM.

$$S(t) = 5 \cos(1600\pi t) + 20 \cos(1800\pi t) + 5 \cos(2000\pi t)$$

II Evaluate the modulation index.

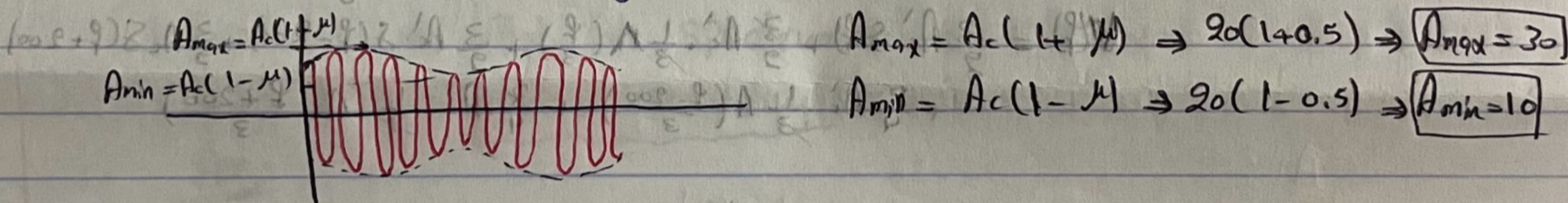
Ans: $S_{AM}(t) = A_c(1 + k_a m(t)) \cos(2\pi f_c t)$, $m(t) = A_m \cos(2\pi f_m t)$

$$S_{AM}(t) = A_c \cos(2\pi f_c t) + A_c k_a A_m \cos(2\pi f_m t) \cos(2\pi f_c t)$$
$$= A_c \cos(2\pi f_c t) + \frac{A_c M}{2} \cos(2\pi(f_c + f_m)t) + \frac{A_c M}{2} \cos(2\pi(f_c - f_m)t)$$

(we can conclude: $A_c = 20$ and $f_c = 900$)

$$(5 = \frac{A_c M}{2}) \Rightarrow \boxed{\mu = 0.5} \text{ [under modulation]}$$

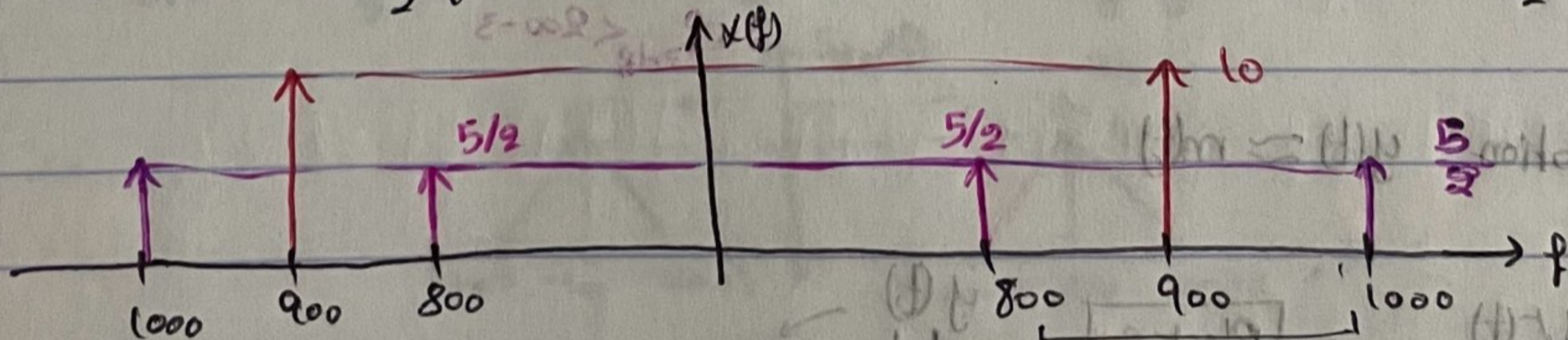
III Sketch the modulated signal in time domain.



IV Find the band width of the transmitted signal in Hz.

Ans: $S(t) = 5 \cos(1600\pi t) + 20 \cos(1800\pi t) + 5 \cos(2000\pi t)$

$$\rightarrow S(f) = \frac{5}{2} (\delta(f-800) + \delta(f+800)) + 10 (\delta(f-900) + \delta(f+900)) + \frac{5}{2} (\delta(f-1000) + \delta(f+1000))$$



$$BW = 1000 - 800 \Rightarrow \boxed{BW = 200 \text{ Hz}}$$

in Normal AM $\rightarrow BW = 2f_m = 200$

$$\Rightarrow \boxed{f_m = 100}$$

4] Evaluate the efficiency of the modulated scheme

Ans: $\eta = \frac{\mu^2}{2 + \mu^2} \times 100\%$
 $= \frac{(0.5)^2}{2 + (0.5)^2} \times 100\% \Rightarrow \boxed{\eta = 11.11\%}$

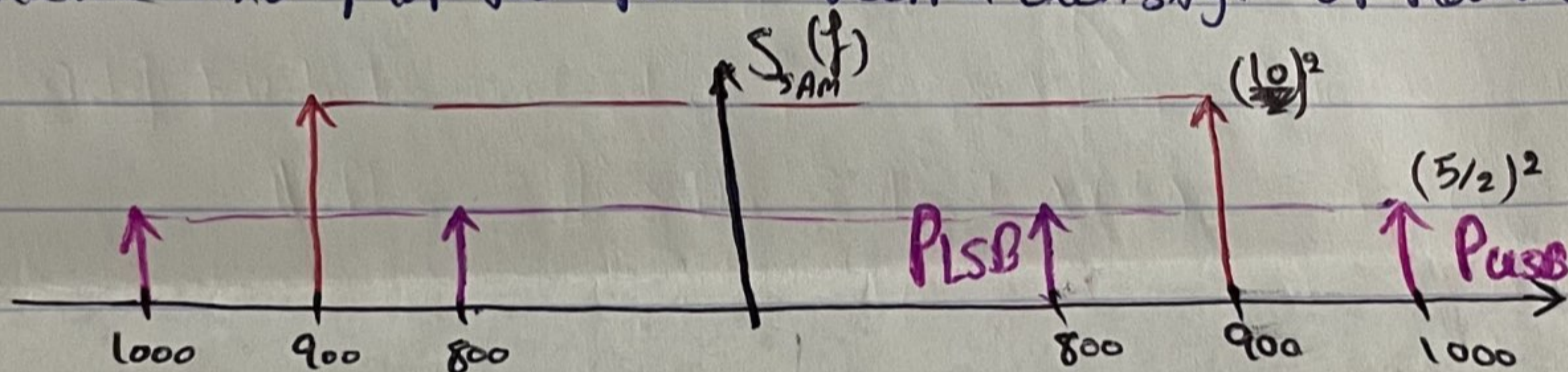
5] Evaluate ~~the~~ Power at Carrier signal.

Ans: $P_c = \frac{(20)^2}{2} \Rightarrow P_c = 200 \text{ W}$

6] Evaluate the P_{USB} (Power at USB).

Ans: $P_{USB} = \frac{(5)^2}{2} \rightarrow P_{USB} = 12.5 \text{ W}$

7] Evaluate and plot the Power Spectral Density of modulated signal.



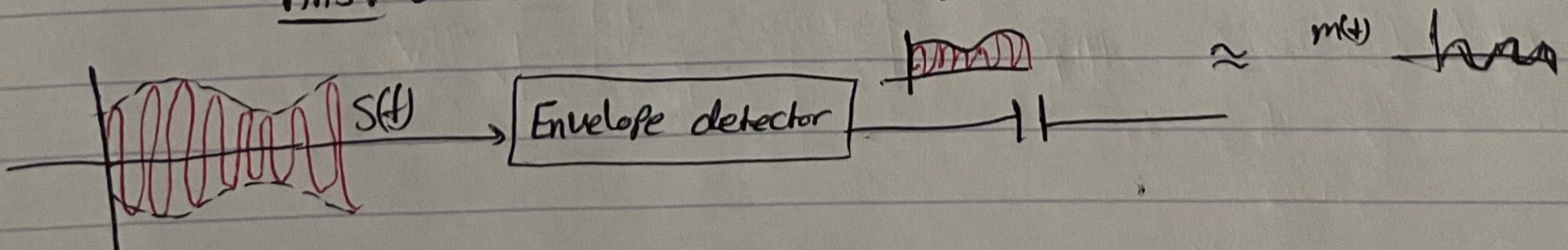
$$S_{SAM}(f) = 10^2 (\delta(f-900) + \delta(f+900)) + \left(\frac{5}{2}\right)^2 (\delta(f-800) + \delta(f+800)) + \left(\frac{5}{2}\right)^2 (\delta(f-1000) + \delta(f+1000))$$

$$P_c = (10)^2 + (10)^2 \Rightarrow \boxed{P_c = 200 \text{ W}}$$

$$P_{USB} = \left(\frac{5}{2}\right)^2 + \left(\frac{5}{2}\right)^2 \Rightarrow \boxed{P_c = 12.5 \text{ W}}$$

8] Draw the ~~the~~ block diagram of demodulator used to recover $m(t)$ from $s(t)$

Ans: to recover $m(t)$ from $s(t) \Rightarrow$ we can use envelope detector.

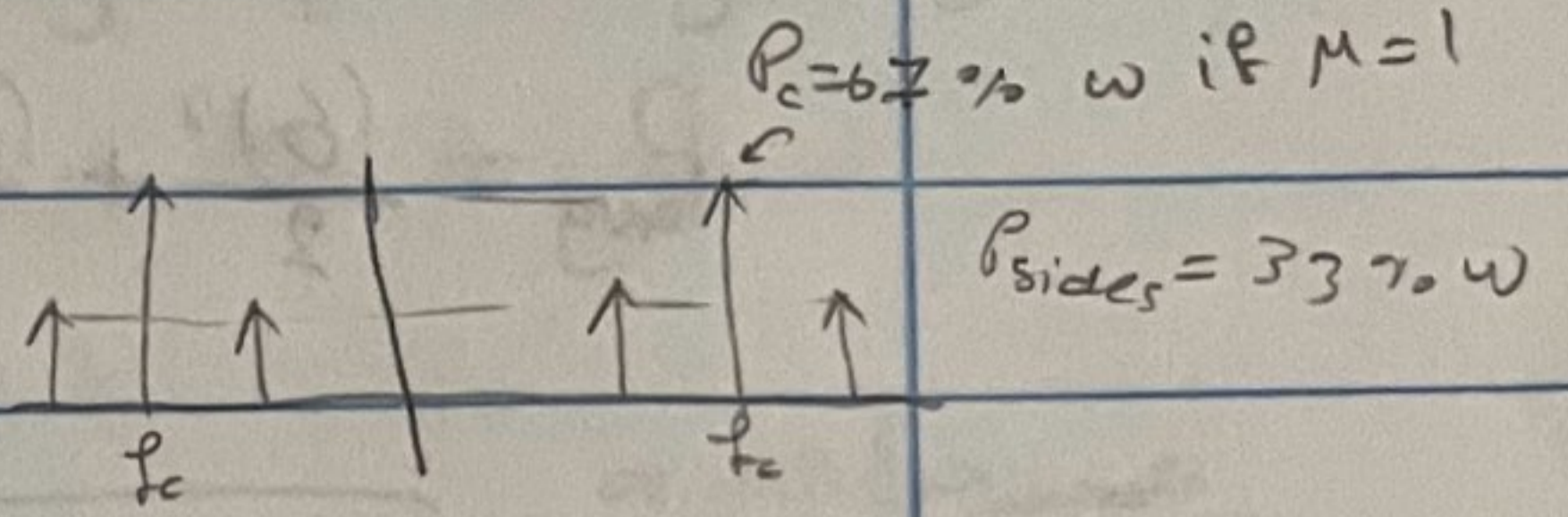


(L8)

Normal AM: DSB-Fc "Double side-band full carrier".

modulated signal for DSB-Fc

$$S_{AM}(t) = A_c (1 + k_a m(t)) \cos(2\pi f_c t)$$



- To improve the efficiency \rightarrow DSB-Fc \rightarrow DSB-SC Carrier is suppressed

modulated signal for DSB-SC can be expressed as

$$S_{DSB-SC}(t) = m(t) c(t) \quad \begin{array}{c} m(t) \\ \downarrow \\ \otimes \\ \uparrow \\ c(t) \end{array}$$

Example Consider the modulating signal $m(t)$ is multitone

which can be expressed as

$$m(t) = 2 \cos(30\pi t) + 4 \cos(60\pi t) : \text{base band signal}$$

and the carrier signal is given by.

$$c(t) = 6 \cos(600\pi t) \rightarrow f_c = 300$$

where $m(t)$ and $c(t)$ are applied to DSB-SC modulator.

II Write the expression of modulated signal in time domain.

Ans: modulated signal for DSB-SC express as

$$\begin{aligned} S_{DSB-SC}(t) &= m(t) c(t) = [2 \cos(30\pi t) + 4 \cos(60\pi t)] [6 \cos(600\pi t)] \\ &= 12 \cos(30\pi t) \cos(600\pi t) + 24 \cos(60\pi t) \cos(600\pi t) \\ &= 6 [\cos(630\pi t) + \cos(570\pi t)] + 12 [\cos(660\pi t) + \cos(540\pi t)] \end{aligned}$$

$$\Rightarrow S_{DSB-SC}(t) = 6 \cos(630\pi t) + 6 \cos(570\pi t) + 12 \cos(660\pi t) + 12 \cos(540\pi t)$$

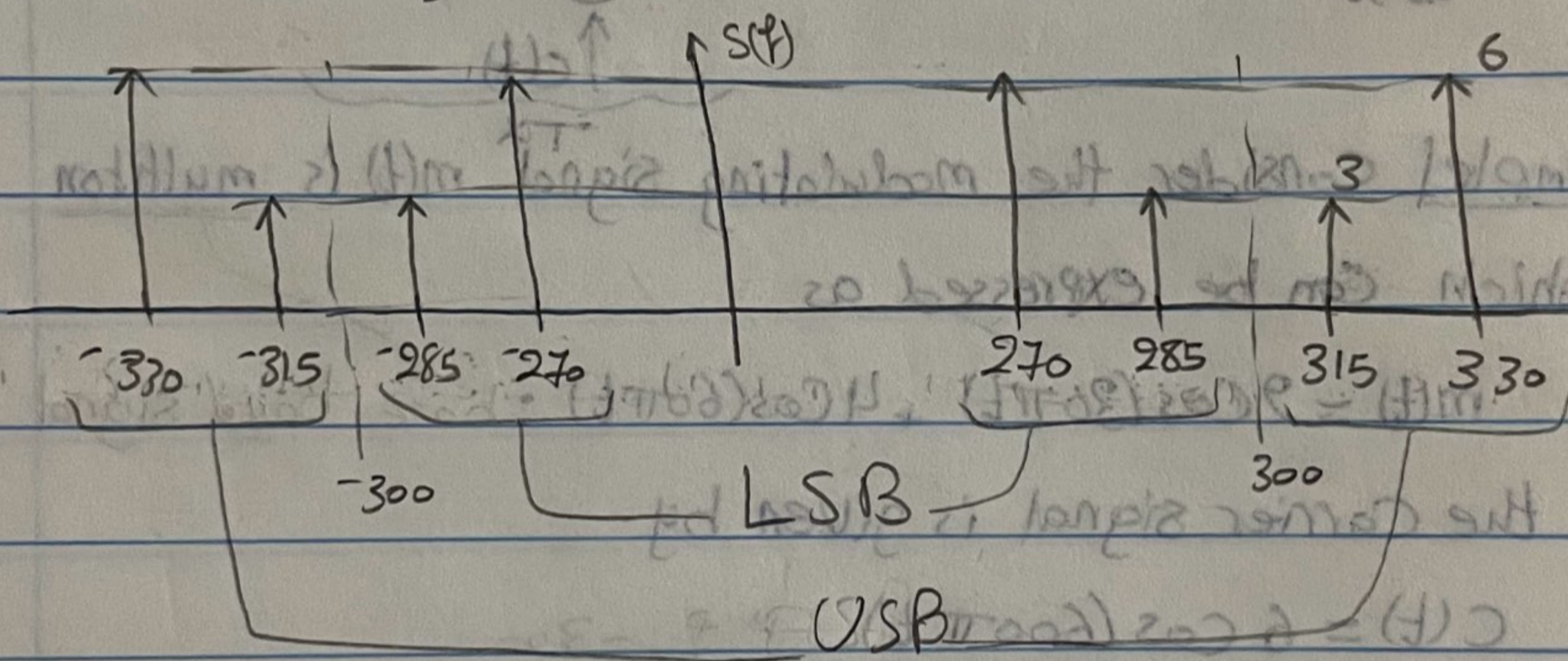
2] Evaluate the average power for modulated signal.

$$P_{avg} = \frac{(6)^2}{2} + \frac{(6)^2}{2} + \frac{(12)^2}{2} + \frac{(12)^2}{2}$$

$$\Rightarrow P_{avg} = 180 \text{ W}$$

3] Evaluate and plot the spectrum of modulated.

$$S(f) = 3[\delta(f-315) + \delta(f+315)] + 3[\delta(f-285) + \delta(f+285)] \\ + 6[\delta(f-330) + \delta(f+330)] + 6[\delta(f-270) + \delta(f+270)]$$



$$M = \frac{P_{sides}}{P_r} = \frac{P_{sides}}{P_{sides}} \times 100\% \Rightarrow M = 100\%$$

4] Evaluate the P_{USB} .

$$\rightarrow \text{Time domain: } P_{USB} = \frac{6^2}{2} + \frac{12^2}{2}$$

$$\rightarrow \text{Freq domain: } P_{USB} = 3^2 + 6^2 + 3^2 + 6^2$$

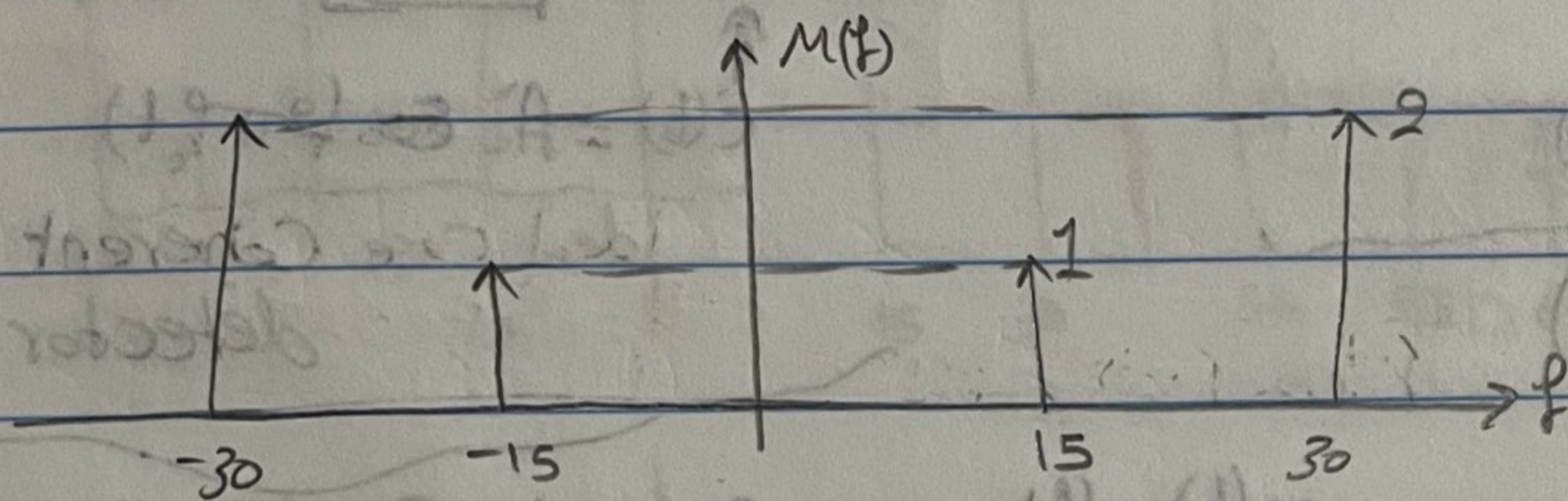
Note:- $M = 100\%$
 %
 DSB-SC

5] Evaluate the BW for modulating signal [message signal] & carrier signal.

- For modulating signal.

$$m(t) = 2 \cos(30\pi t) + 4 \cos(60\pi t) \quad [\text{base band signal}]$$

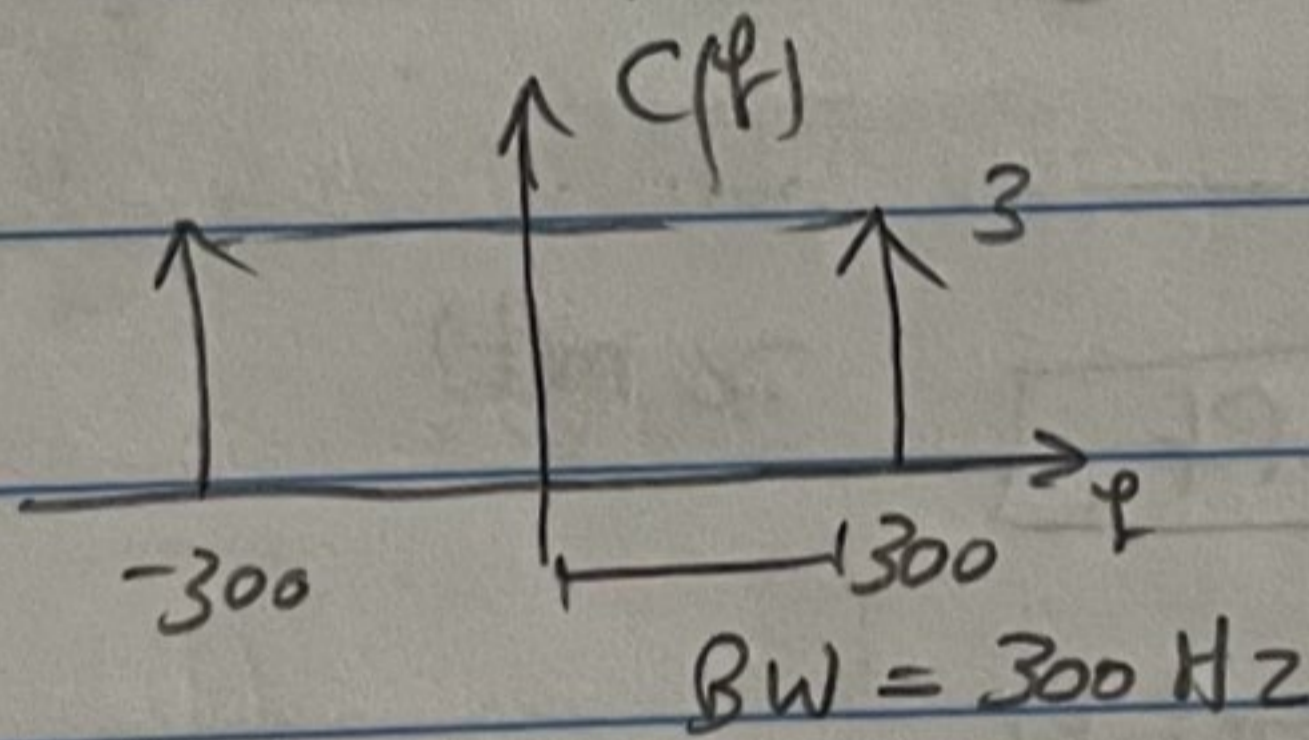
$$M(f) = \delta(f-15) + \delta(f+15) + 2\delta(f-30) + 2\delta(f+30)$$



$$BW = 30 \text{ Hz}$$

- For carrier signal.

$$c(t) = 6 \cos(600\pi t) \rightarrow C(f) = 3\delta(f-300) + 3\delta(f+300)$$



$$BW = 300 \text{ Hz}$$

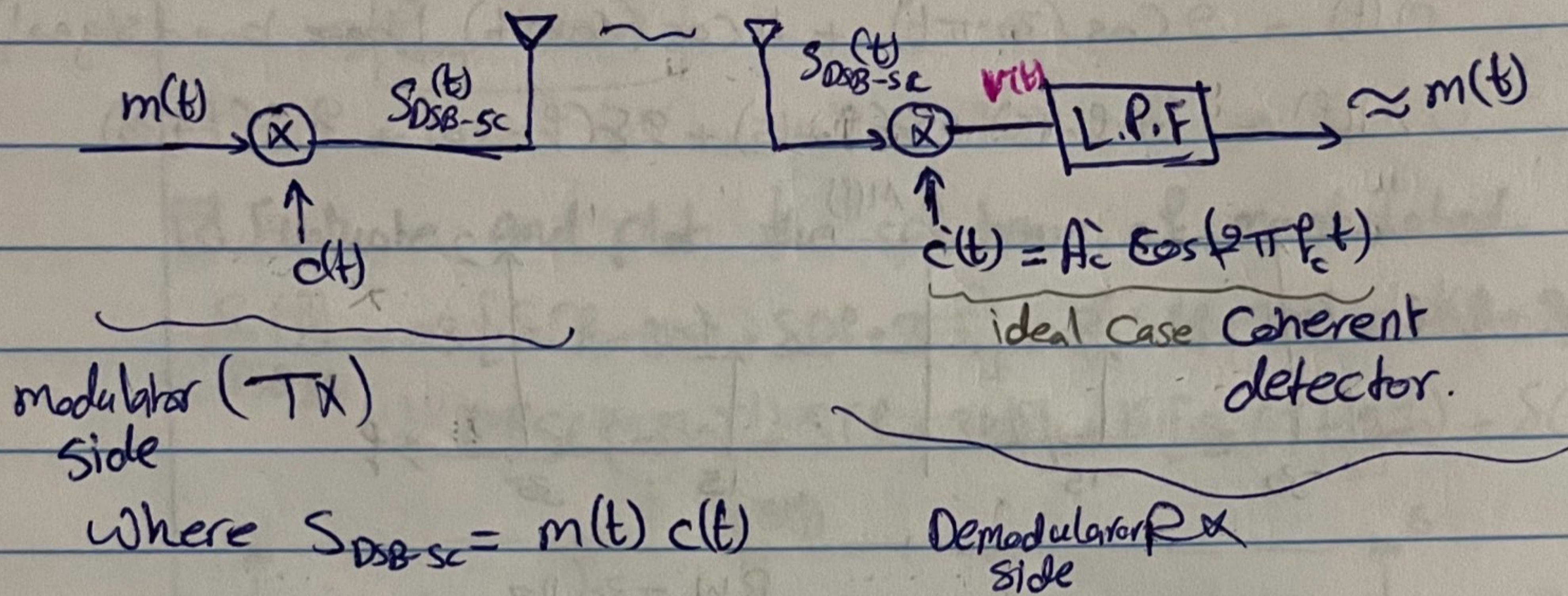
6] Evaluate the BW of modulated signal.

$$BW = 330 - 270 \Rightarrow \boxed{BW = 60 \text{ Hz}} = 2f_{\text{max}}$$

For modulated signal.

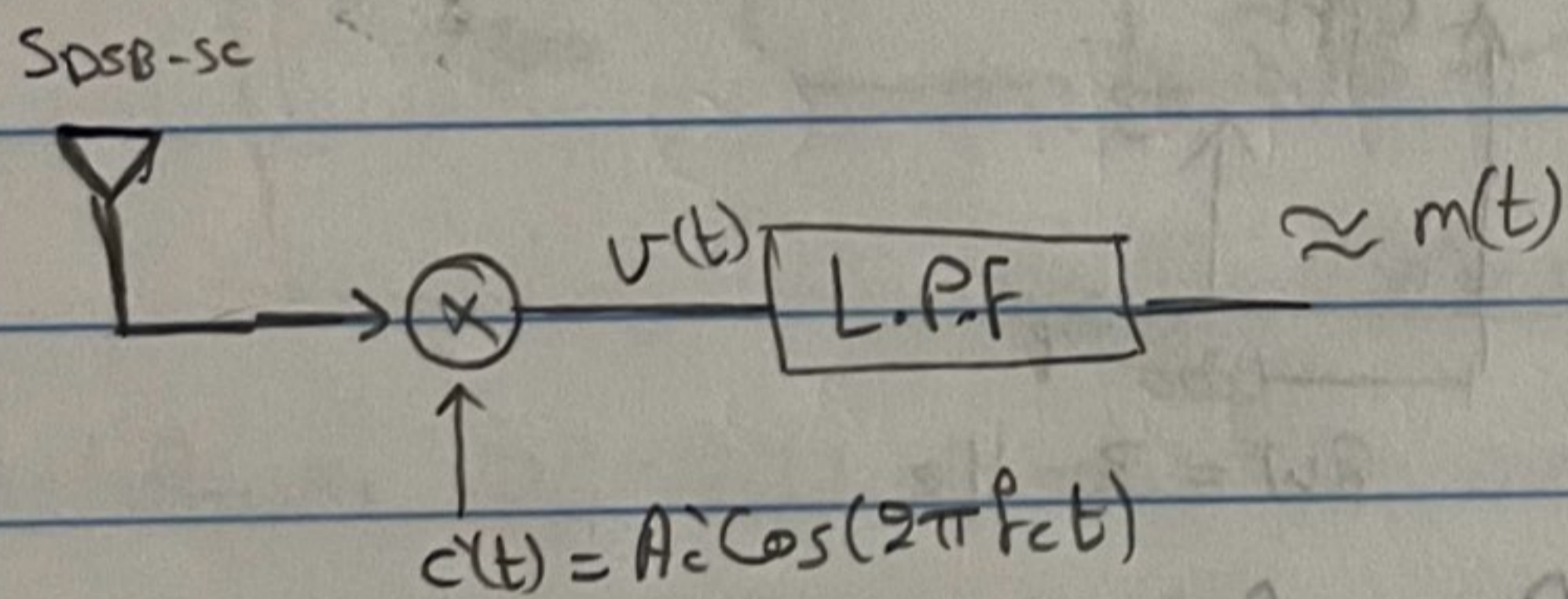
Demodulation Schemes (Rx) $\left\{ \begin{array}{l} \text{Coherent } (f_c, \theta_c \rightarrow \text{Constant}) \\ \text{Non Coherent } (f_c, \theta_c \rightarrow \text{Not-Constant}) \end{array} \right.$

• Block diagram for DSB-SC modulator & demodulator.



⇒

□ Draw block diagram for coherent detector.



$$v(t) = S_{DSB-SC}(t) c'(t) = m(t) c(t) c'(t)$$

$$= m(t) \cdot A_c \cos(2\pi f_c t) \cdot A_c \cos(2\pi f_c t)$$

$$= A_c A_c m(t) \cos^2(2\pi f_c t)$$

$$= \frac{A_c A_c}{2} m(t) \left[\frac{1}{2} + \frac{1}{2} \cos(4\pi f_c t) \right]$$

$$= \frac{1}{2} \cdot 6 \cdot A_c \left[2 \cos(30\pi t) + 4 \cos(60\pi t) \right] \left[\frac{1}{2} + \frac{1}{2} \cos(1200\pi t) \right]$$

$$= 3 A_c \cos(30\pi t) + 6 A_c \cos(60\pi t) + \frac{3 A_c \cos(30\pi t) \cos(1200\pi t)}{\frac{1}{2} \cos(1230\pi t) + \frac{1}{2} \cos(1170\pi t)}$$

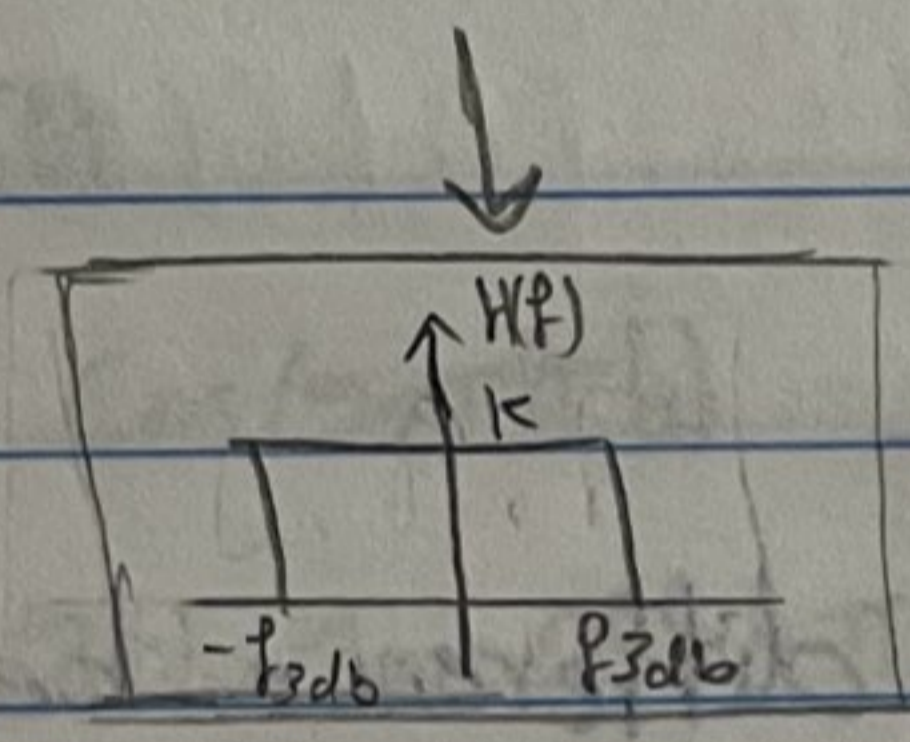
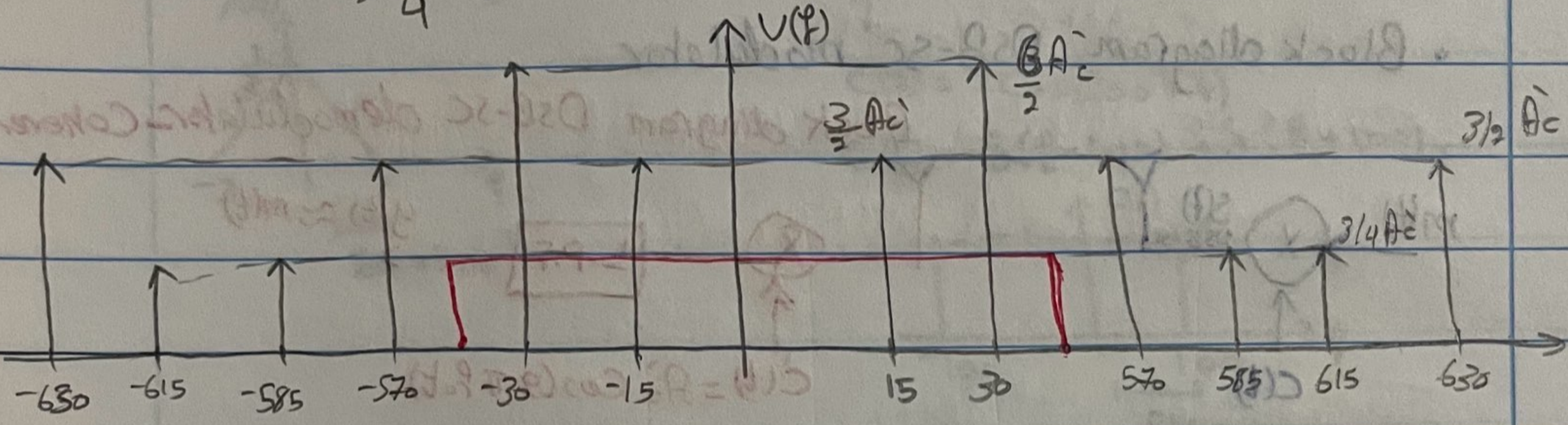
$$+ 6 A_c \cos(60\pi t) \cos(1200\pi t) \left[\frac{1}{2} \cos(1260\pi t) + \frac{1}{2} \cos(1140\pi t) \right]$$

(P.1)

$$T(s) = \frac{3A_c}{2} \left[\delta(\omega - 15) + \delta(\omega + 15) \right] + \frac{6}{2} A_c \left[\delta(\omega - 30) + \delta(\omega + 30) \right]$$

$$+ \frac{3A_c}{2} \left[\delta(\omega - 615) + \delta(\omega + 615) + \delta(\omega + 585) + \delta(\omega - 585) \right]$$

$$+ \frac{3}{2} \frac{6A_c}{4} \left[\delta(\omega - 630) + \delta(\omega + 630) + \delta(\omega - 570) + \delta(\omega + 570) \right]$$

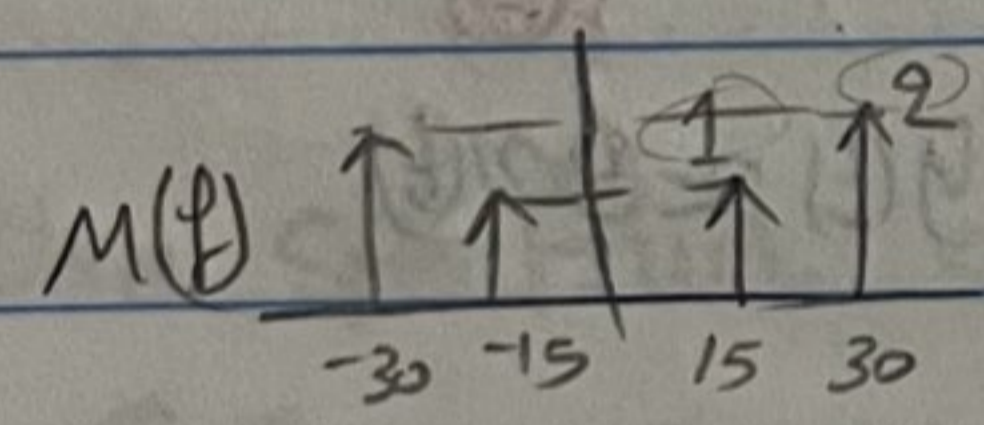


$$30 \leq f_{3db} < 570 \text{ Hz}$$

$$K = \frac{\text{Amp out}}{\text{Amp in}}$$

$$y(t) \approx m(t)$$

$$K_1 = \frac{1}{\frac{3}{2} A_c}, \quad K_2 = \frac{2}{\frac{6}{2} A_c}$$



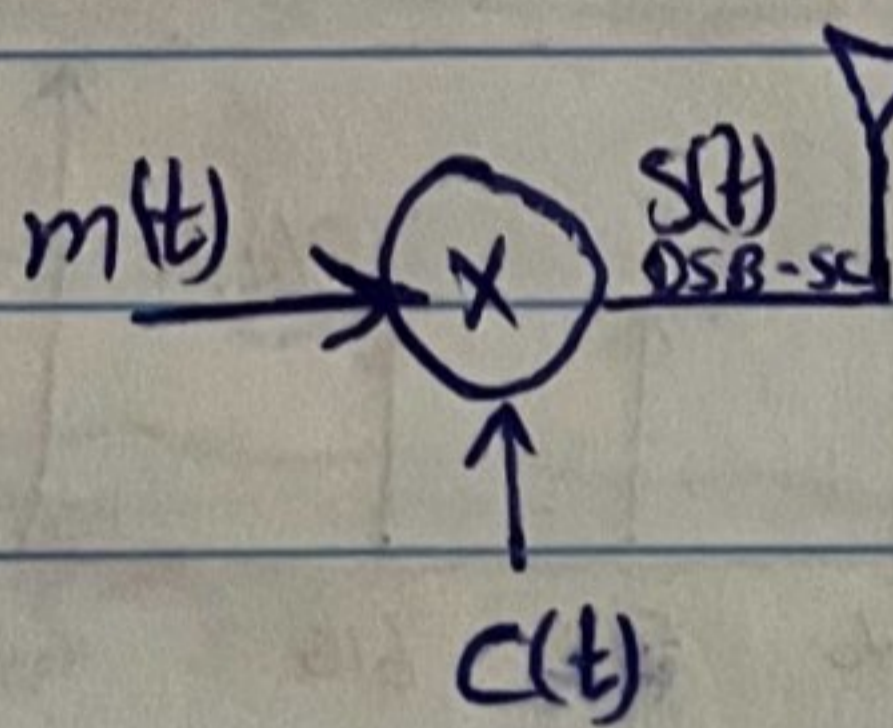
$$\Rightarrow K_1 = \frac{2}{3 A_c}, \quad K_2 = \frac{2}{3 A_c}$$

$$\Rightarrow K = \frac{2}{3} A_c$$

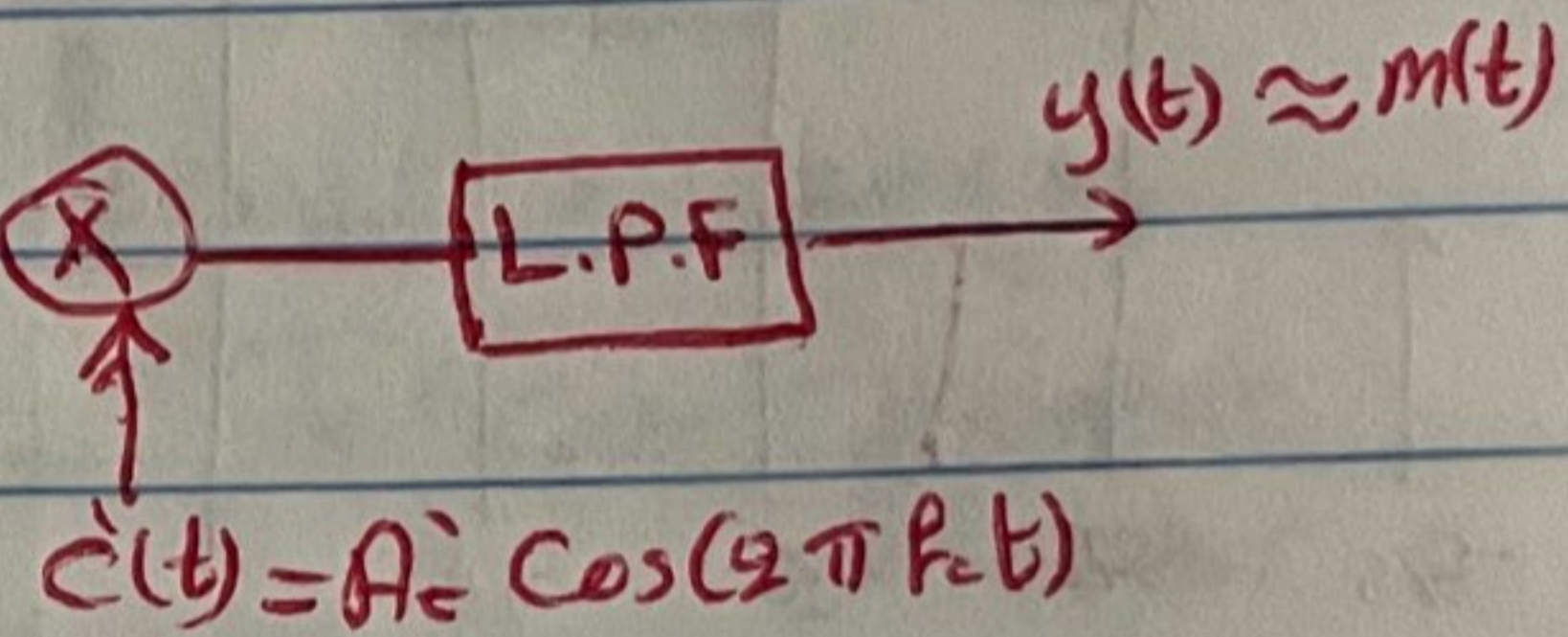
(L9)

Let message signal "modulating signal" $m(t) = \text{sinc}^2(3t)$ and carrier signal $c(t) = A_c \cos(2\pi f_c t)$, are applied on DSB-SC modulator.

• Block diagram DSB-SC modulator

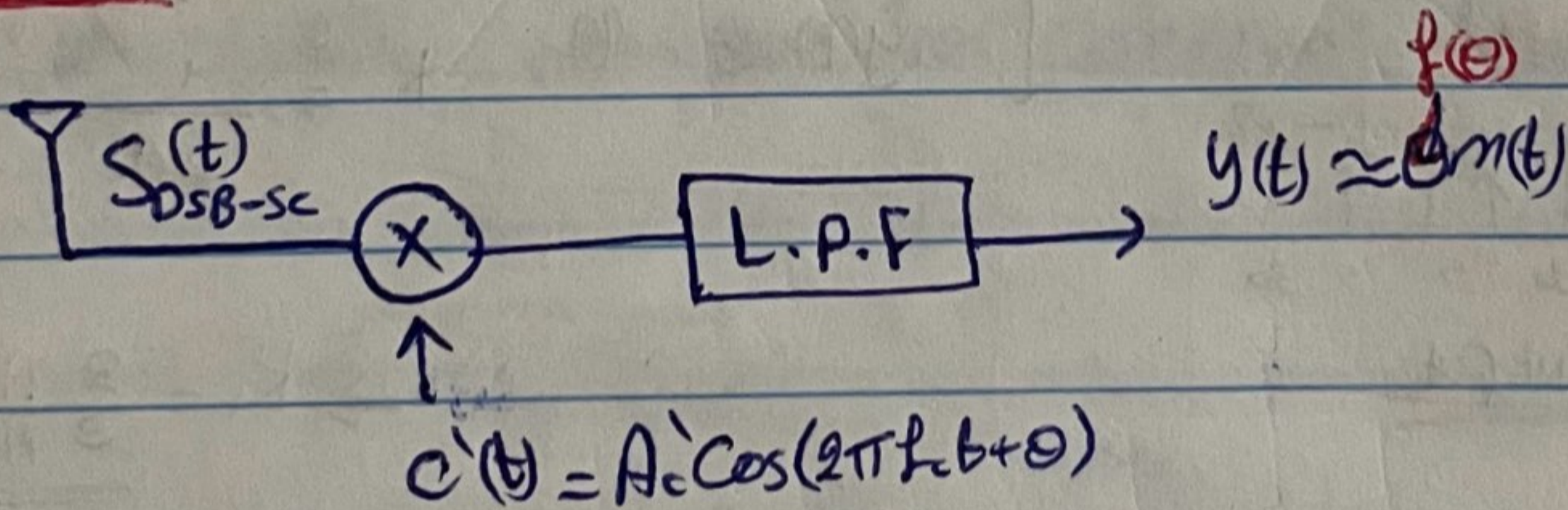


Block diagram DSB-SC demodulator - Coherent

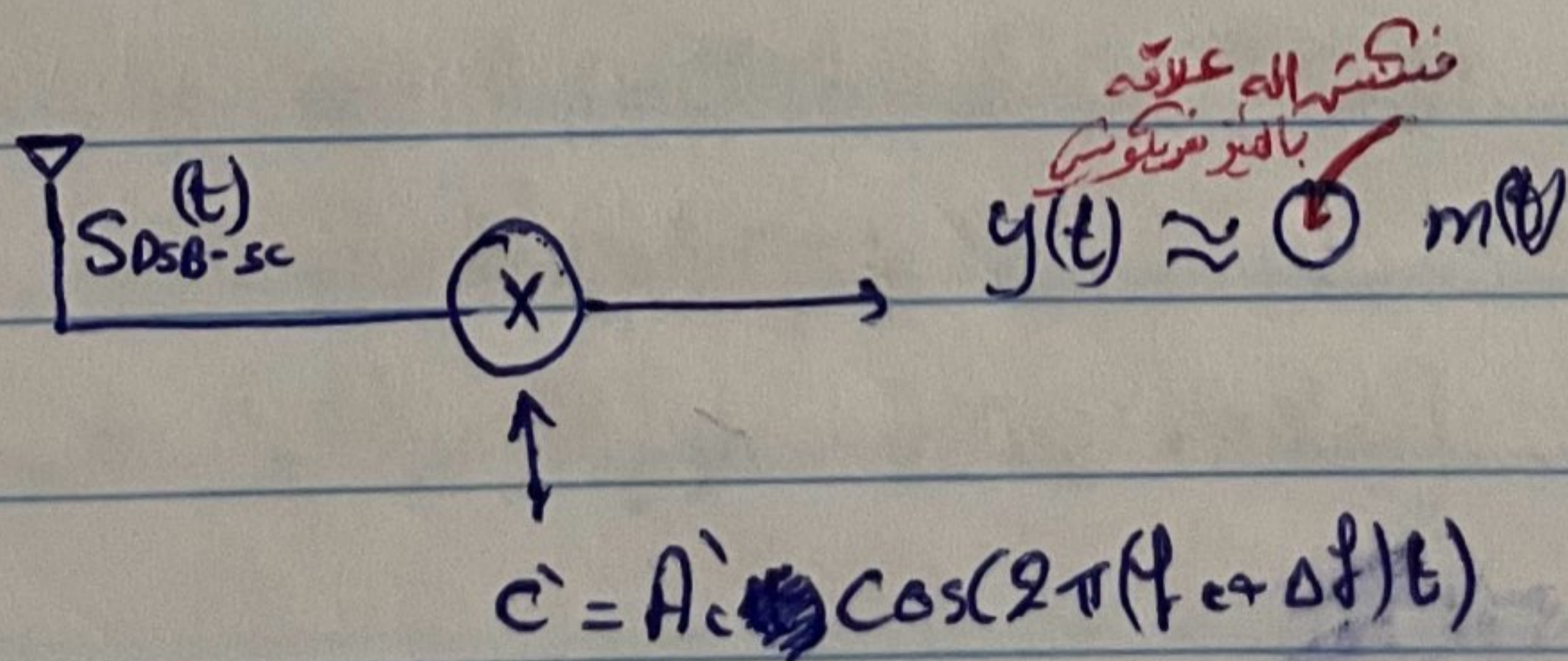


• Non-Coherent detection.

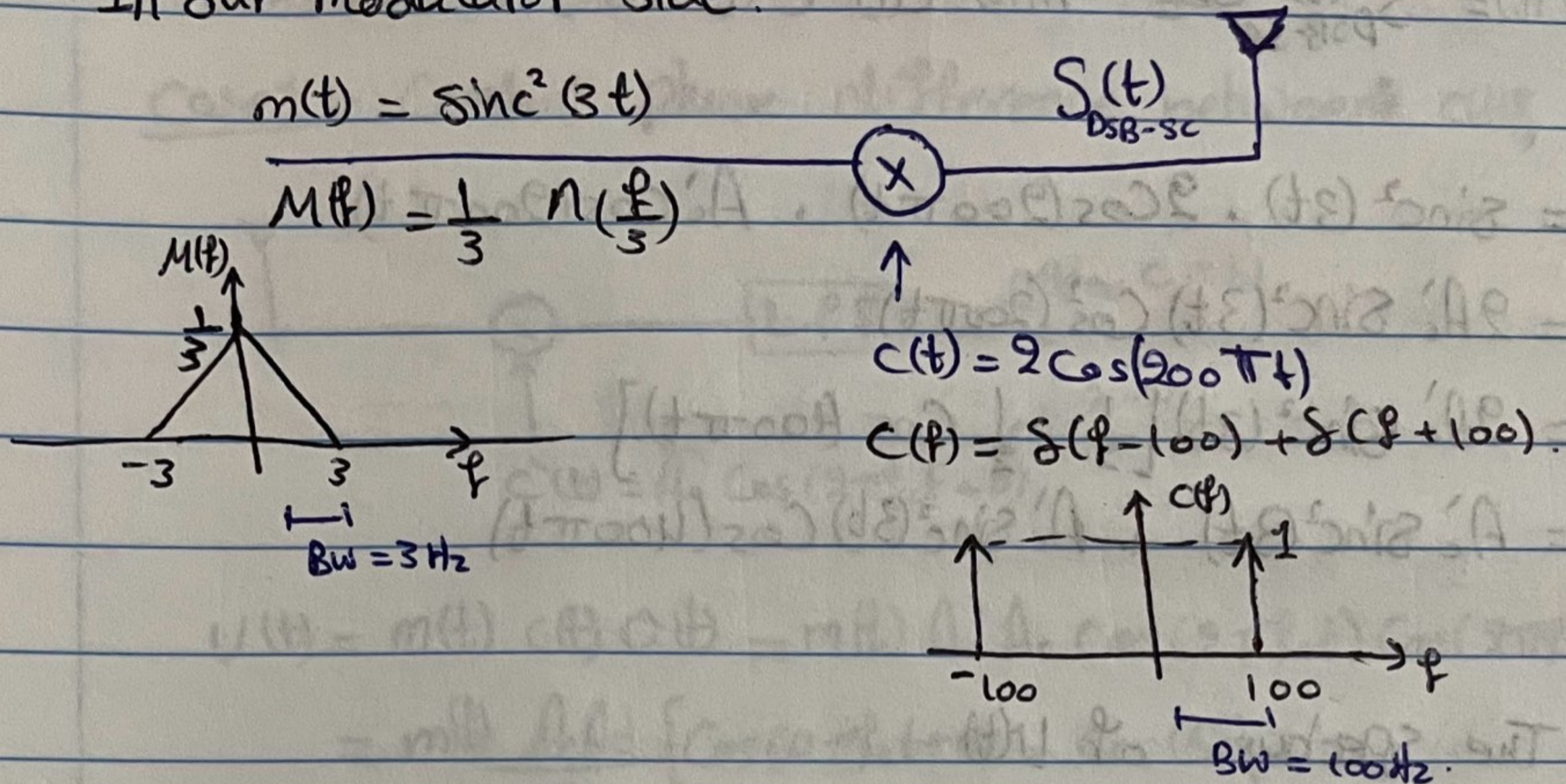
Case 1: Constant phase difference between $c(t)$ and $c'(t)$



Case 2: Constant frequency difference between $c(t)$ and $c'(t)$.



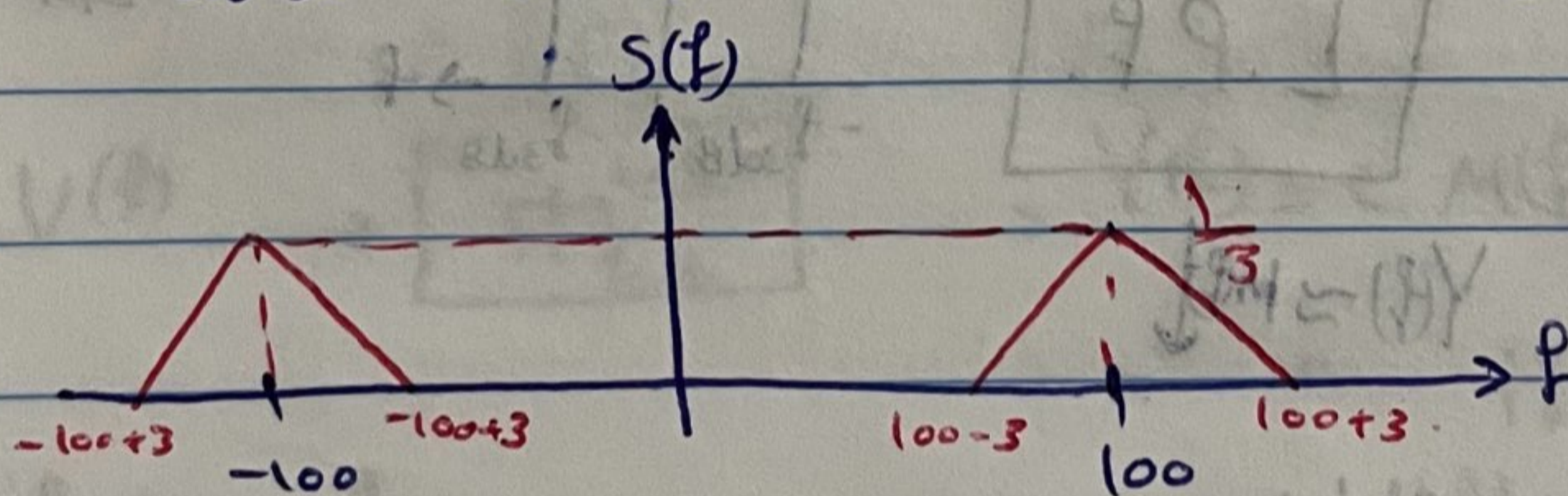
In our modulator side.



$$\begin{aligned}
 S_{\text{DSB-SC}}(t) &= m(t)c(t) \\
 &= 2m(t)\cos(200\pi t) \\
 &= 2\text{sinc}^2(3t)\cos(200\pi t)
 \end{aligned}$$

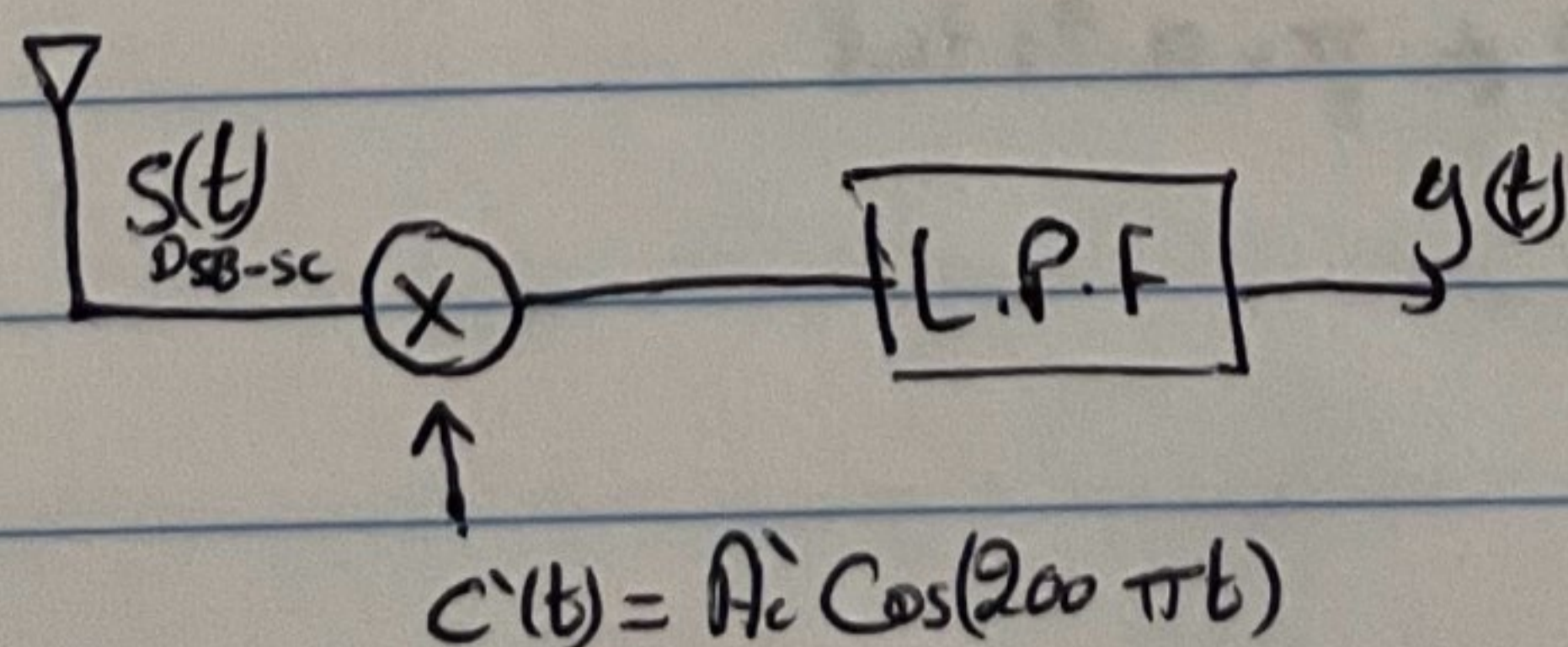
→ The spectrum of modulated signal can be given by.

$$S_{\text{DSB-SC}}(f) = \frac{2}{2} \cdot \frac{1}{3} \Lambda\left(\frac{1}{3}(f-100)\right) + \frac{2}{2} \cdot \frac{1}{3} \Lambda\left(\frac{1}{3}(f+100)\right)$$



- our Demodulator.

• Coherent Detector.



$$v(t) = S_{DSB-SC}(t) c(t) = m(t) c(t) c'(t)$$

$$= \text{sinc}^2(3t) \cdot 2\cos(200\pi t) \cdot A_c \cos(200\pi t)$$

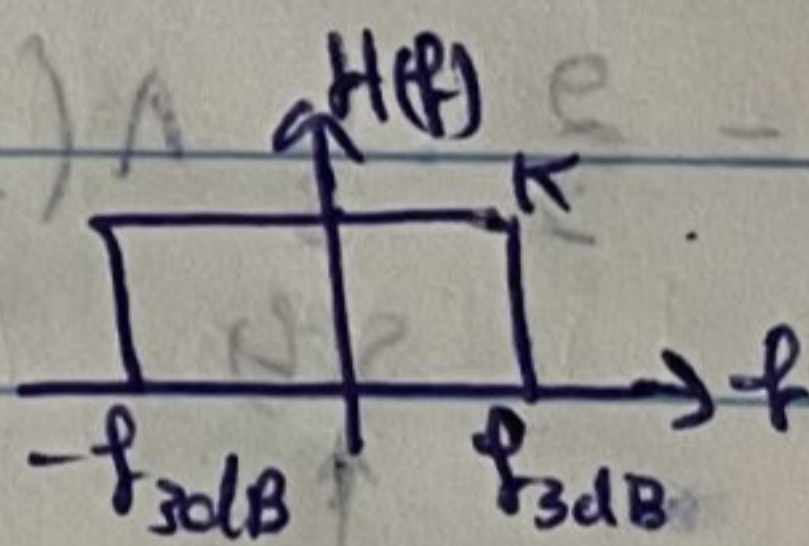
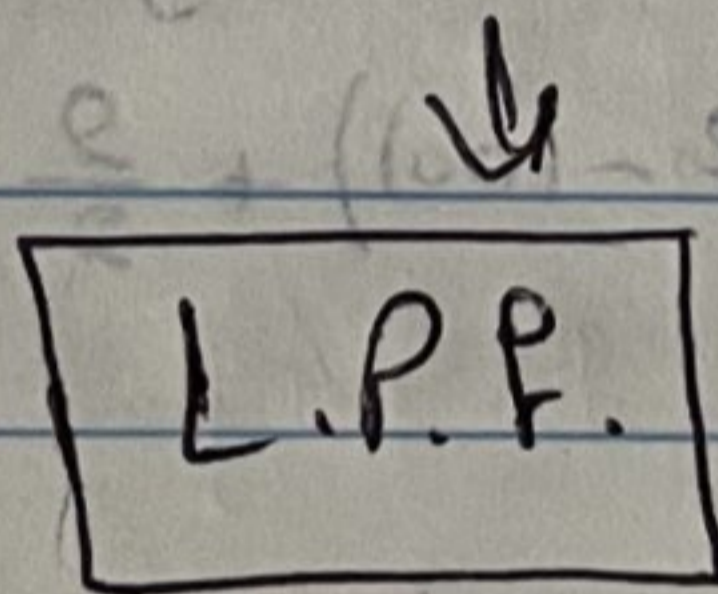
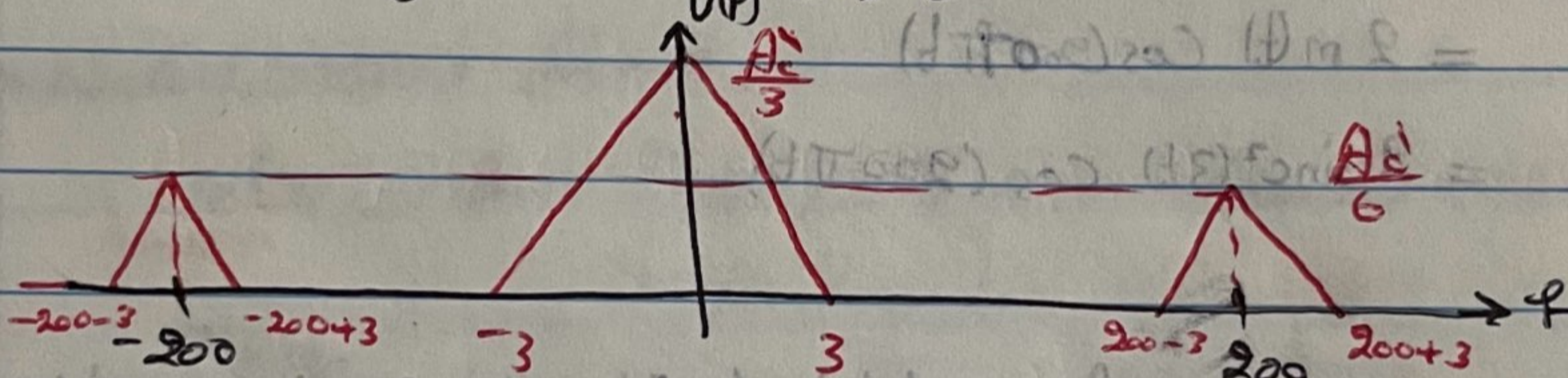
$$= 2A_c \text{sinc}^2(3t) \cos^2(200\pi t)$$

$$= 2A_c \text{sinc}^2(3t) \left[\frac{1}{2} + \frac{1}{2} \cos(400\pi t) \right]$$

$$= A_c \text{sinc}^2(3t) + A_c \text{sinc}^2(3t) \cos(400\pi t)$$

• The spectrum of $v(t)$

$$V(f) = \frac{A_c}{3} \Lambda\left(\frac{f}{3}\right) + \frac{A_c}{3 \cdot 2} \left[\Lambda\left(\frac{1}{3}(f-200)\right) + \Lambda\left(\frac{1}{3}(f+200)\right) \right]$$



$$Y(f) \approx \text{HPF}$$

To Evaluate gain

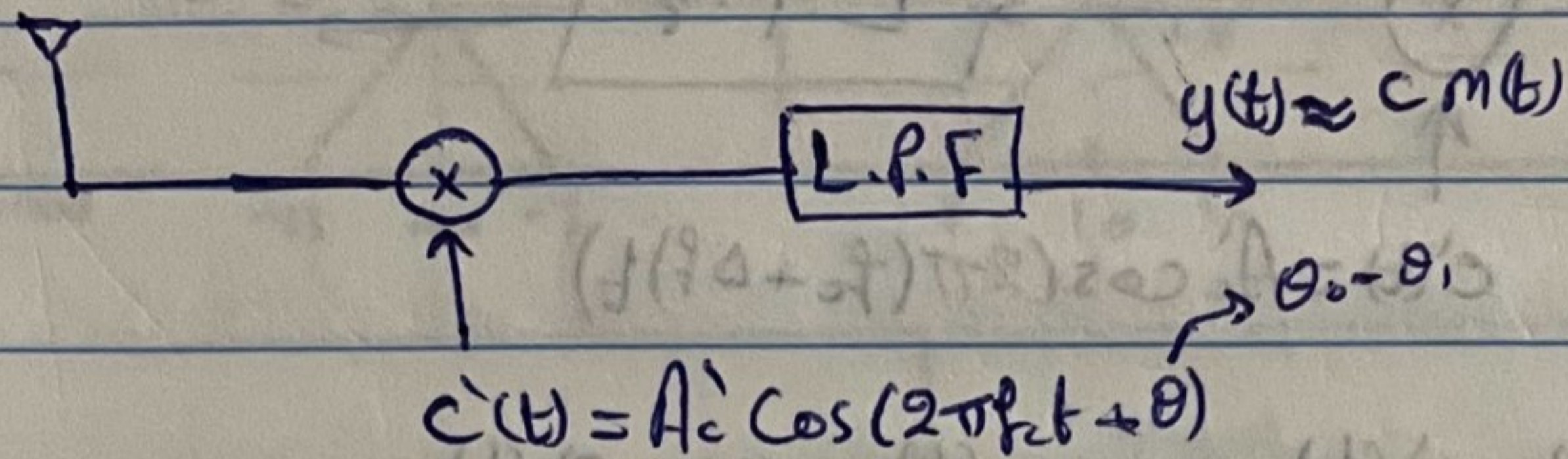
$$\frac{A_c \cdot k}{3} = \frac{1}{3} \Rightarrow \boxed{k = \frac{1}{A_c}}$$

$$3 \leq f_{3dB} < 200 - 3$$

[L(10)].

Non-Coherent detector.

Case 1:- Constant phase difference between $c(t)$ & $c'(t)$

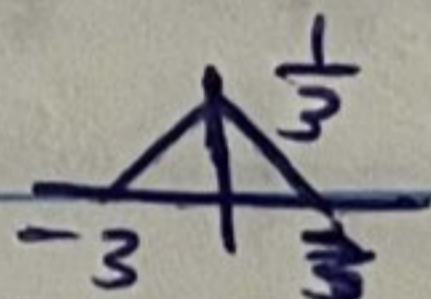


$$V(t) = m(t) c(t) c'(t) = m(t) A_c A_{c'} \cos(2\pi f_c t) \cos(2\pi f_{c'} t + \theta)$$

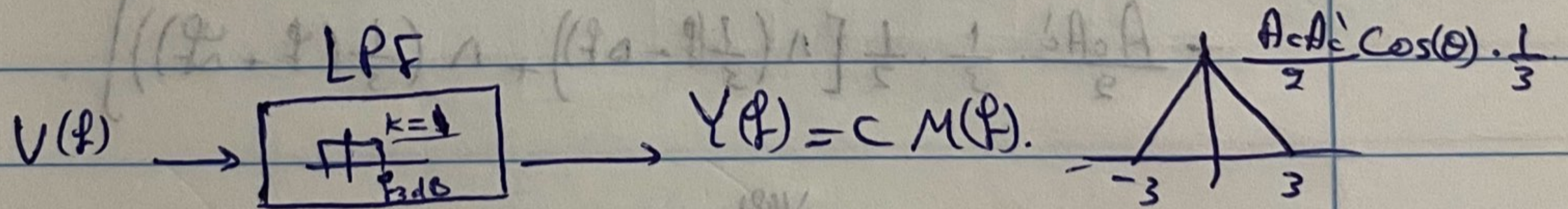
$$= m(t) \frac{A_c A_{c'}}{2} [\cos(4\pi f_c t + \theta) + \cos(\theta)]$$

$$= \frac{A_c A_{c'}}{2} m(t) \cos(\theta) + \frac{A_c A_{c'}}{2} m(t) \cos(4\pi f_c t + \theta)$$

Since, $m(t) = \text{sinc}^2(3t)$



$$\Rightarrow V(t) = \frac{A_c A_{c'}}{2} \text{sinc}^2(3t) \cos(\theta) + \frac{A_c A_{c'}}{2} \text{sinc}^2(3t) \cos(4\pi f_c t + \theta)$$



if $K = \frac{2}{A_c A_{c'}}$

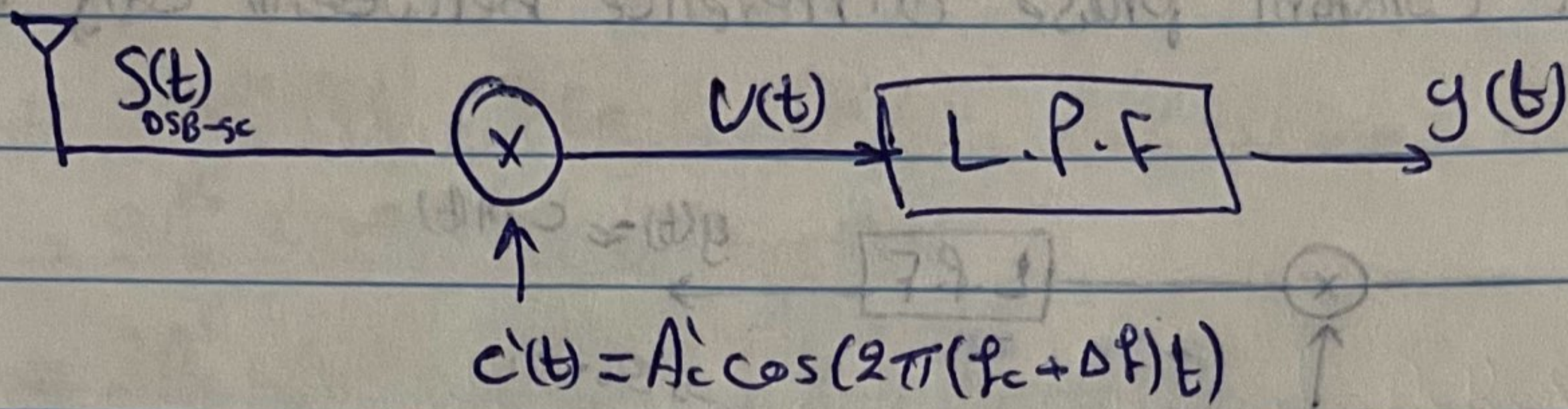
if $K=1$
 $y(t) = \frac{A_c A_{c'}}{2} \cos(\theta) \text{sinc}^2(3t)$
 $= \frac{A_c A_{c'}}{2} \cos(\theta) m(t)$

$\Rightarrow y(t) = \cos(\theta) m(t)$

\Rightarrow We have original $m(t) \rightarrow \theta=0$

but if $\theta = \frac{\pi}{2} \Rightarrow y(t) = 0$

Case 2: Constant frequency difference between $c(t)$ & $c'(t)$



$$V(t) = S(t)_{DSB-SC} c'(t) = m(t) c(t) c'(t)$$

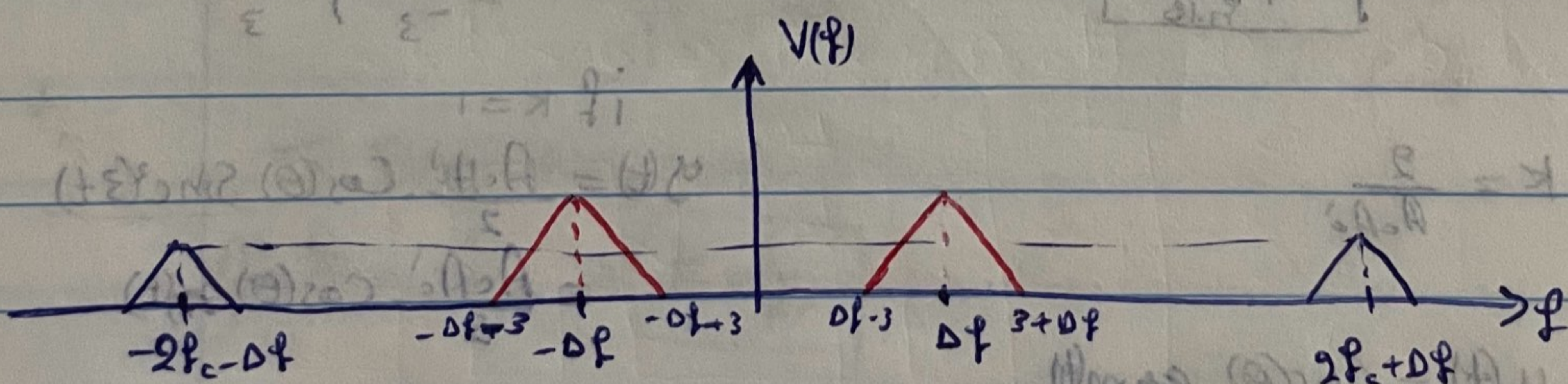
$$= m(t) A_c A_c' \cos(2\pi f_c t) \cos(2\pi (f_c + \Delta f) t)$$

$$= \frac{A_c A_c'}{2} m(t) [\cos(4\pi f_c t + 2\pi \Delta f t) + \cos(2\pi \Delta f t)]$$

$$= \frac{A_c A_c'}{2} m(t) \cos(4\pi f_c t + 2\pi \Delta f t) + \frac{A_c A_c'}{2} m(t) \cos(2\pi \Delta f t)$$

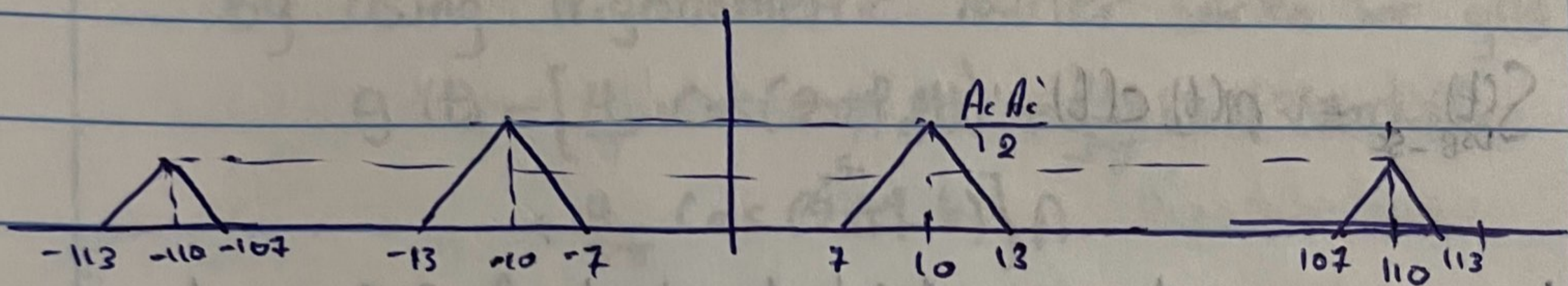
$$V(f) = \frac{A_c A_c'}{2} \cdot \frac{1}{3} \cdot \frac{1}{2} \left[\Lambda\left(\frac{1}{3}(f - (2f_c + \Delta f))\right) + \Lambda\left(\frac{1}{3}(f + (2f_c + \Delta f))\right) \right]$$

$$+ \frac{A_c A_c'}{2} \cdot \frac{1}{3} \cdot \frac{1}{2} \left[\Lambda\left(\frac{1}{3}(f - \Delta f)\right) + \Lambda\left(\frac{1}{3}(f + \Delta f)\right) \right]$$

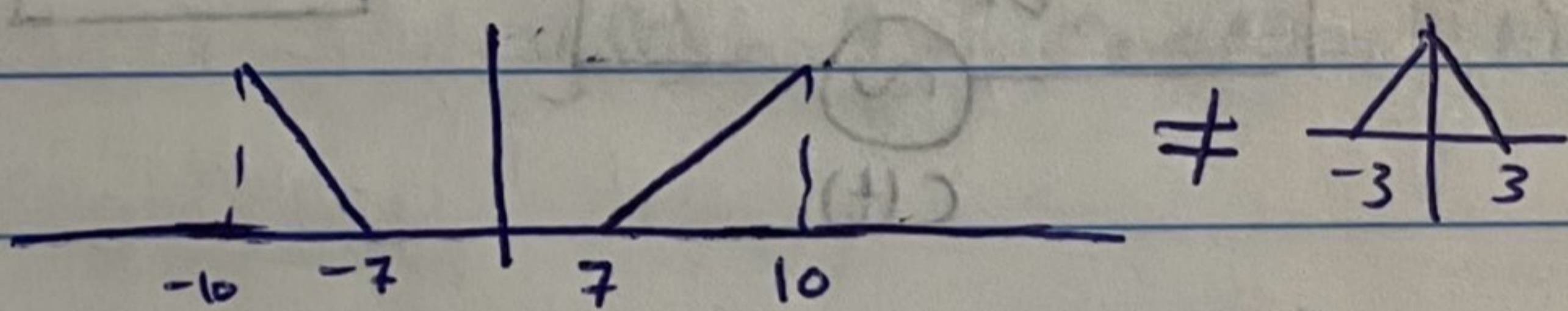
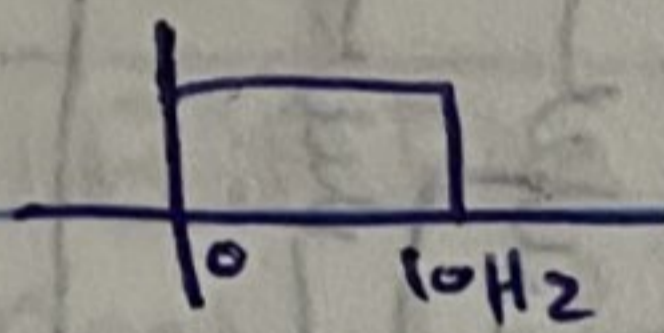


L.P.F

Now, let $\Delta f = 10$ and $f_c = 50$



L.P.F



B.P.F

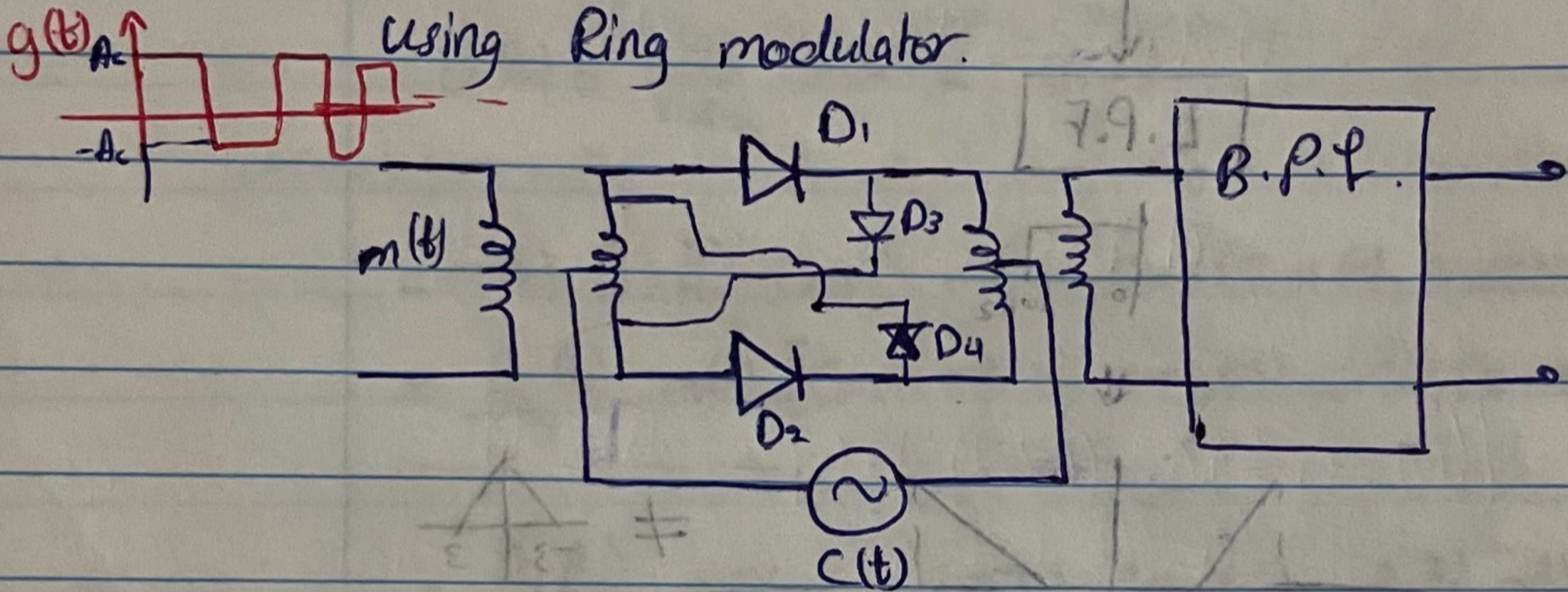
B.P.F

≡ Generat DSB-SC modulated signal.

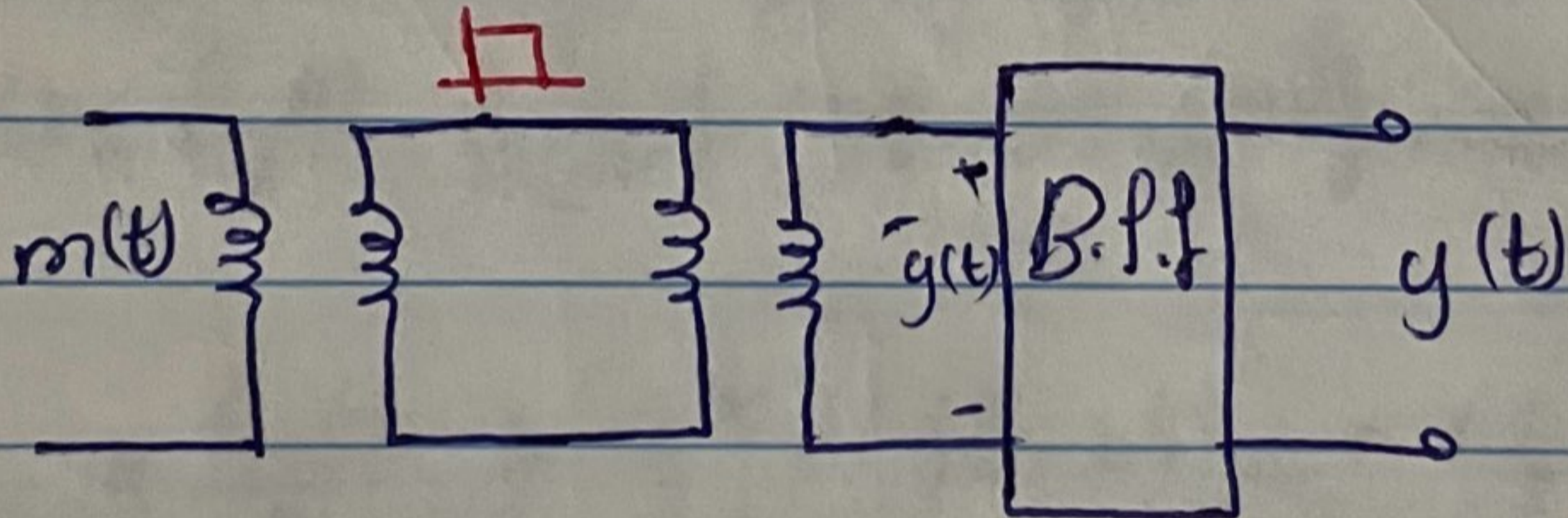
$$S_{DSB-SC}(t) = m(t) c(t)$$

We can generate modulated signal of DSB-SC by

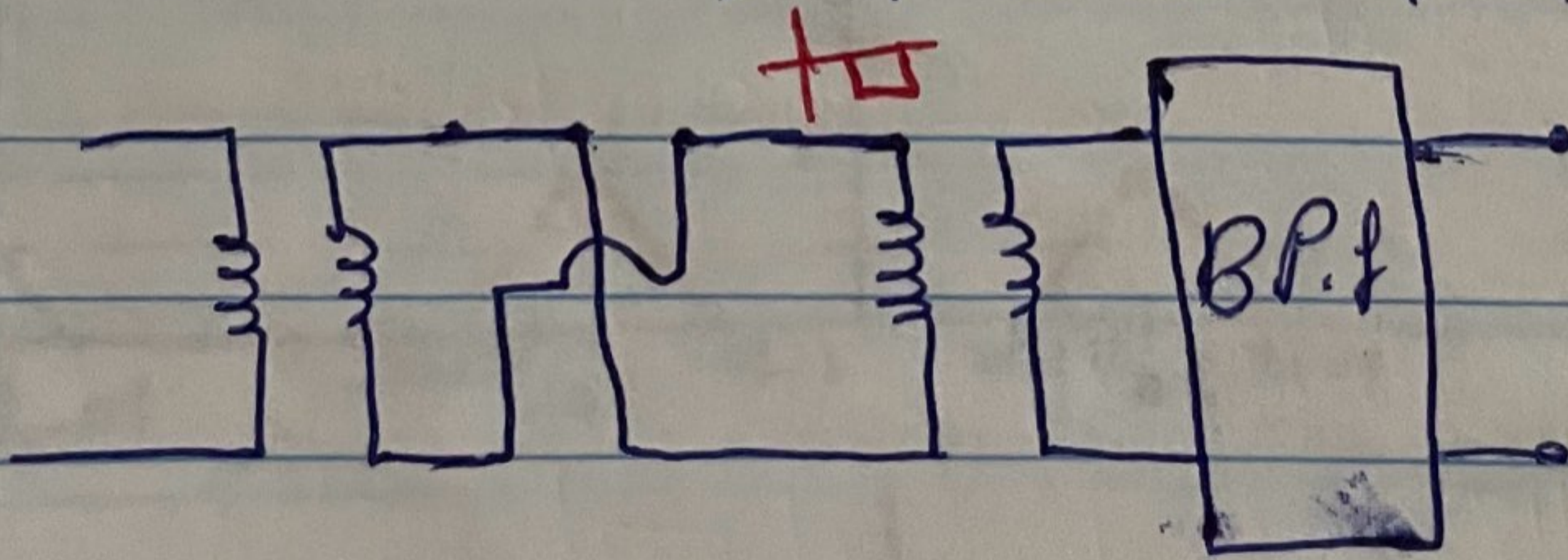
using Ring modulator.



• $c(t) > 0 \rightarrow D_1$ and D_2 on, D_3 and D_4 off.



• $c(t) < 0 \rightarrow D_1$ and D_2 off, D_3 and D_4 on.

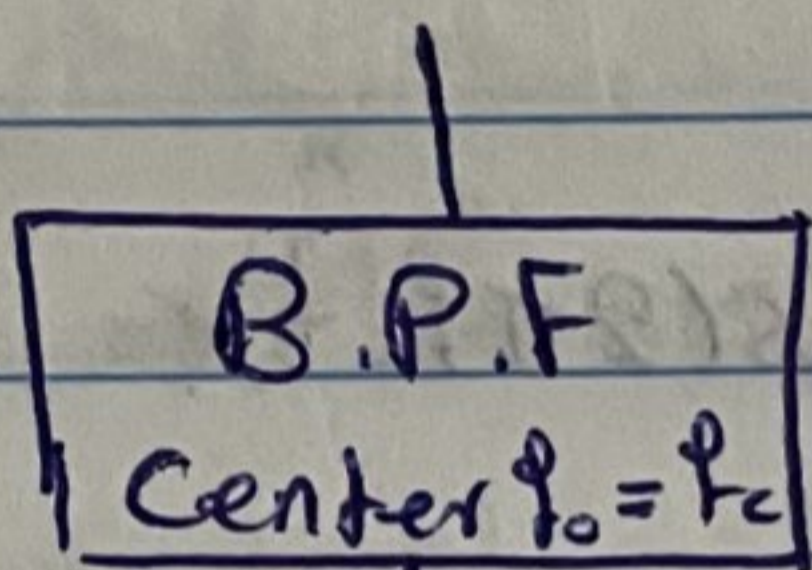


$$\tilde{y}(t) = m(t) g(t)$$

by using Trigonometric Fourier Series for $g(t)$

$$g(t) = \left[\frac{4}{\pi} \cos(2\pi f_c t) + \frac{4}{3\pi} \cos(3(2\pi f_c t)) + \frac{4}{5\pi} \cos(5(2\pi f_c t)) \right] A_c$$

$$\tilde{y}(t) = m(t) \left[\frac{4}{\pi} \cos(2\pi f_c t) + \frac{4}{3\pi} \cos(3(2\pi f_c t)) + \frac{4}{5\pi} \cos(5(2\pi f_c t)) \right] A_c$$



$$y(t) = \frac{4}{\pi} A_c \cos(2\pi f_c t) m(t)$$

≡ SSB-SC i. single side band.

In double side band, the modulated signal can be expressed as

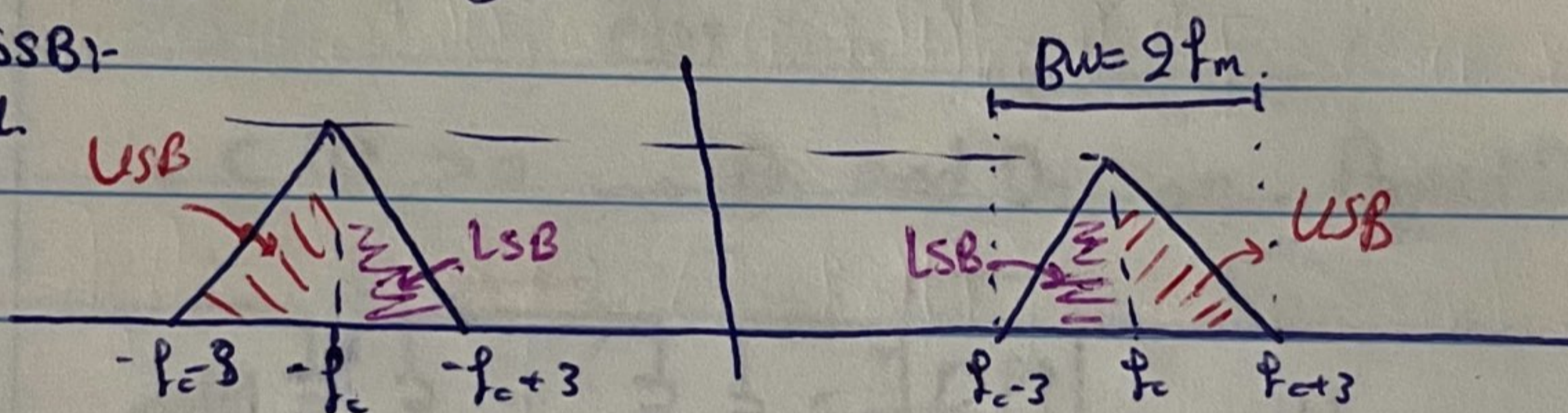
$$S_{DSB-SC}(t) = m(t) c(t)$$

Let $m(t) = \text{sinc}^2(3t)$

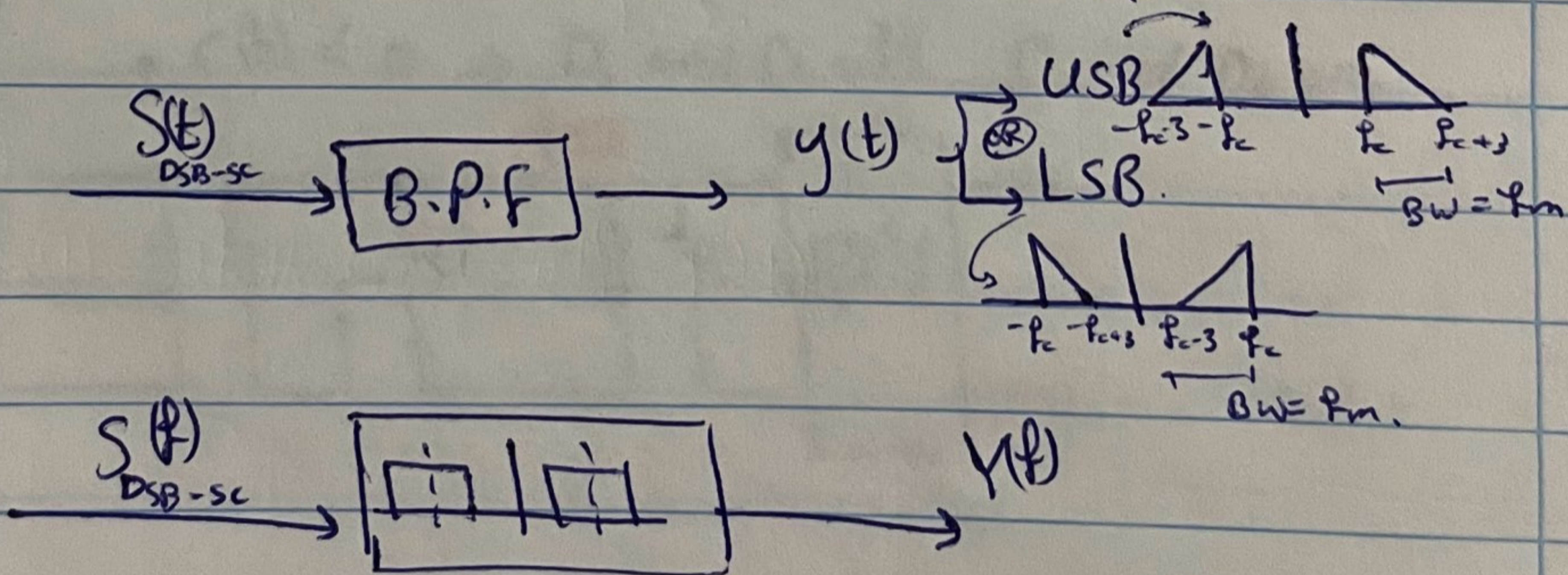
$$S(t)_{DSB-SC} = A_c \text{sinc}^2(3t) \cos(2\pi f_c t)$$

$$S(f)_{DSB-SC} = \frac{A_c}{2} \cdot \frac{1}{3} \left[\Lambda\left(\frac{1}{3}(f-f_c)\right) + \Lambda\left(\frac{1}{3}(f+f_c)\right) \right]$$

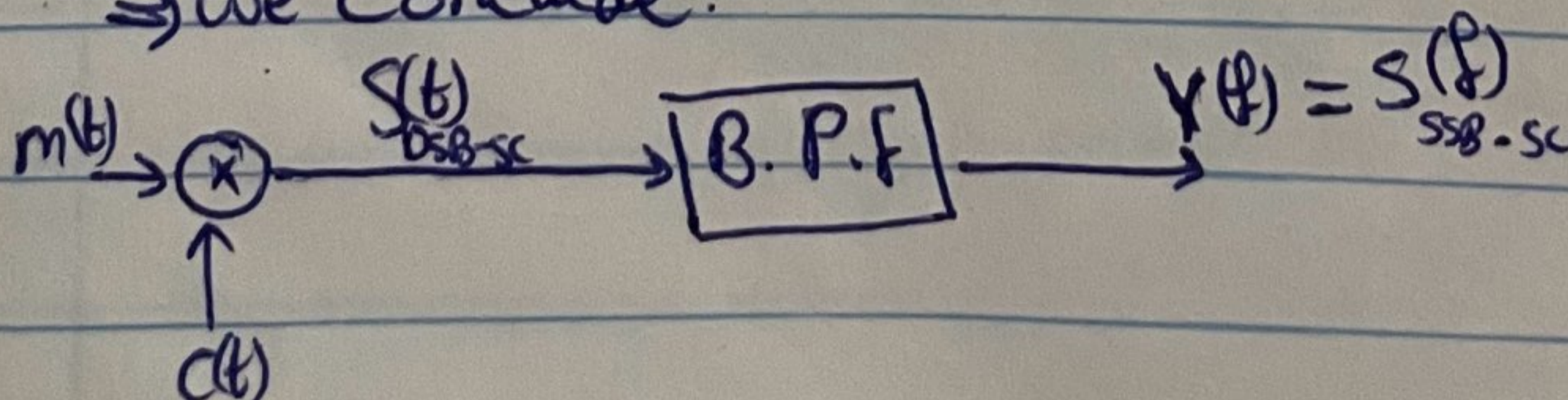
III
Generation of SSB-
Filtering Method



- To decrease the BW from $2f_m$ to f_m



⇒ we conclude.



2] Generation SSB signal: phase shift method.

SSB-SC modulated signal can be expressed as.

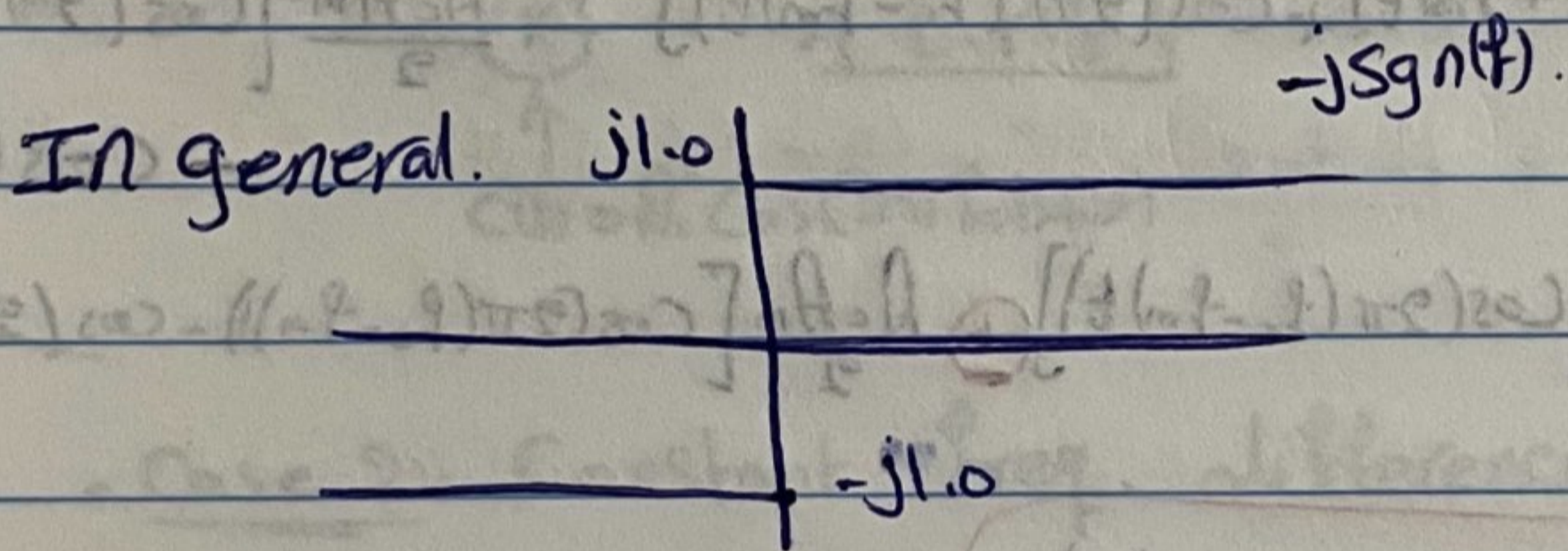
$$s(t) = A_c m(t) \cos(\omega_c t) \pm A_c \hat{m}(t) \sin(\omega_c t)$$

\swarrow USB \searrow LSB

$\hat{m}(t)$ ← Hilbert transform of $m(t)$

Now, Let $m(t) = A_m \cos(2\pi f_m t)$; $c(t) = A_c \cos(2\pi f_c t)$.

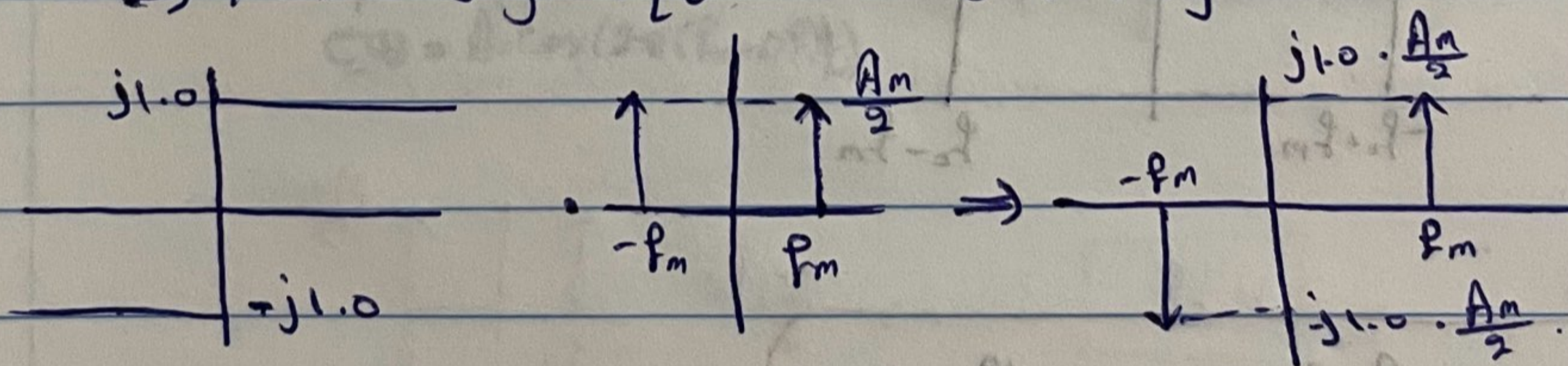
$$\hat{m}(t) = \frac{1}{\pi t} * m(t) \Rightarrow \hat{M}(f) = -j \operatorname{sgn}(f) M(f)$$



+ $\operatorname{sgn} \Rightarrow$ Lower Side band
 - $\operatorname{sgn} \Rightarrow$ Upper Side band

Since $m(t) = A_m \cos(2\pi f_m t) \Rightarrow M(f) = \frac{A_m}{2} [\delta(f - f_m) + \delta(f + f_m)]$.

$$\Rightarrow \hat{M}(f) = -j \operatorname{sgn}(f) [\delta(f - f_m) + \delta(f + f_m)]$$



$$\Rightarrow \hat{M}(f) = [j \delta(f - f_m) + j \delta(f + f_m)] \cdot \frac{A_m}{2}$$

$$= \frac{A_m}{j2} \delta(f - f_m) - \frac{A_m}{j2} \delta(f + f_m)$$

$$\hat{m}(t) = \frac{A_m}{j2} [e^{j2\pi f_m t} - e^{-j2\pi f_m t}] \Rightarrow \boxed{A_m \sin(2\pi f_m t)}$$

$\hat{m}(t)$

$$S_{SSB}(t) = A_c A_m \cos(2\pi f_m t) \cos(2\pi f_c t) \pm A_c A_m \sin(2\pi f_m t) \sin(2\pi f_c t)$$

Remember.

$$\cos(\alpha + \beta) = \cos(\alpha) \cos(\beta) - \sin(\alpha) \sin(\beta)$$

$$\cos(\alpha - \beta) = \cos(\alpha) \cos(\beta) + \sin(\alpha) \sin(\beta)$$

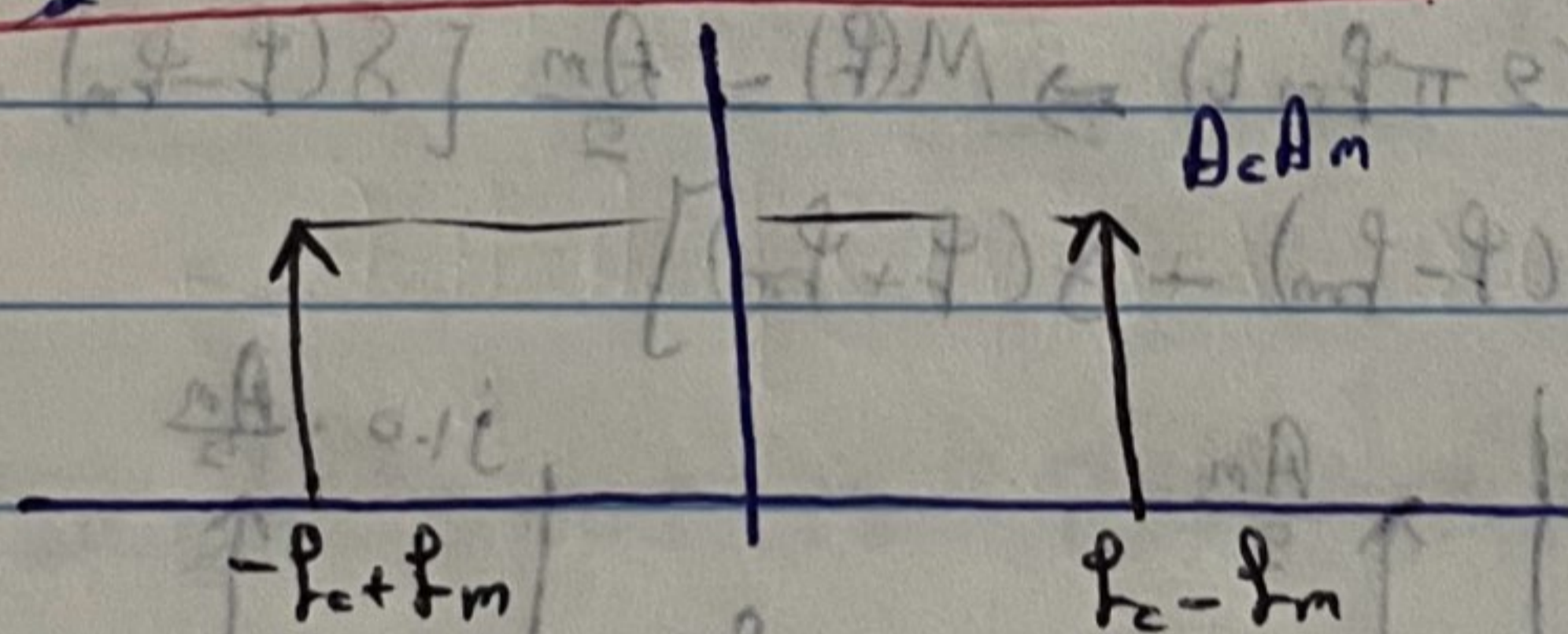
$$\cos(\alpha) \cos(\beta) = \frac{1}{2} \cos(\alpha + \beta) + \frac{1}{2} \cos(\alpha - \beta)$$

$$\sin(\alpha) \sin(\beta) = \frac{1}{2} \cos(\alpha - \beta) - \frac{1}{2} \cos(\alpha + \beta)$$

$$\rightarrow = \frac{A_c A_m}{2} [\cos(2\pi(f_c + f_m)t) + \cos(2\pi(f_c - f_m)t)] \pm \frac{A_c A_m}{2} [\cos(2\pi(f_c - f_m)t) - \cos(2\pi(f_c + f_m)t)]$$

$$S(t) = \frac{A_c A_m}{2} [\cos(2\pi(f_c + f_m)t) + \cos(2\pi(f_c - f_m)t)] \pm \frac{A_c A_m}{2} [\cos(2\pi(f_c - f_m)t) - \cos(2\pi(f_c + f_m)t)]$$

$$\rightarrow S_{LSB} = \frac{A_c A_m}{2} \cos(2\pi(f_c - f_m)t)$$

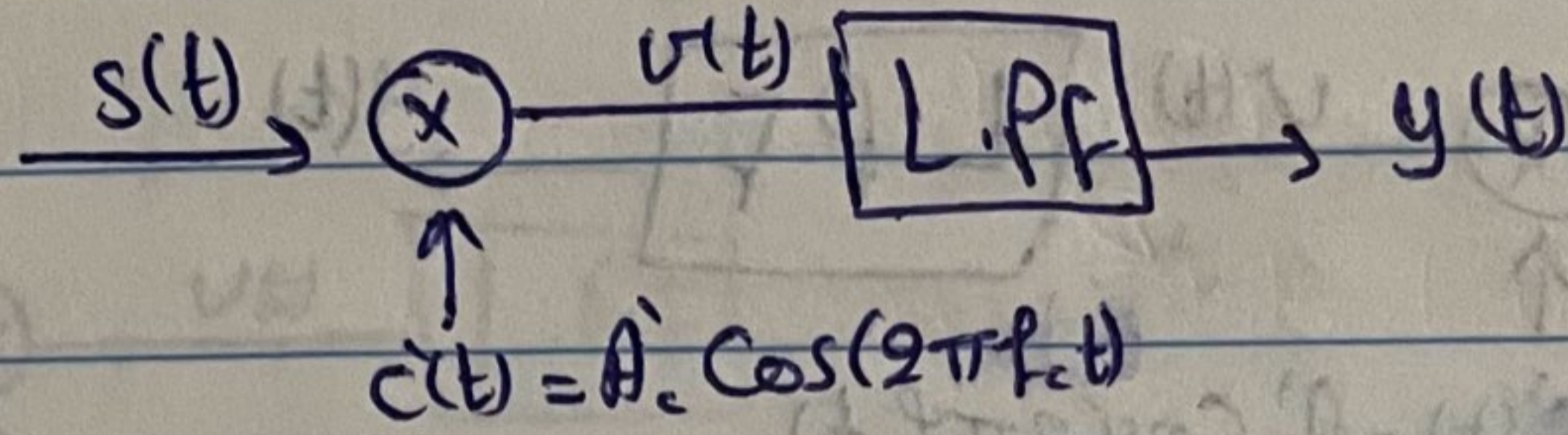


$$S_{USB}(t) = A_c A_m \cos(2\pi(f_c + f_m)t)$$

(L11)

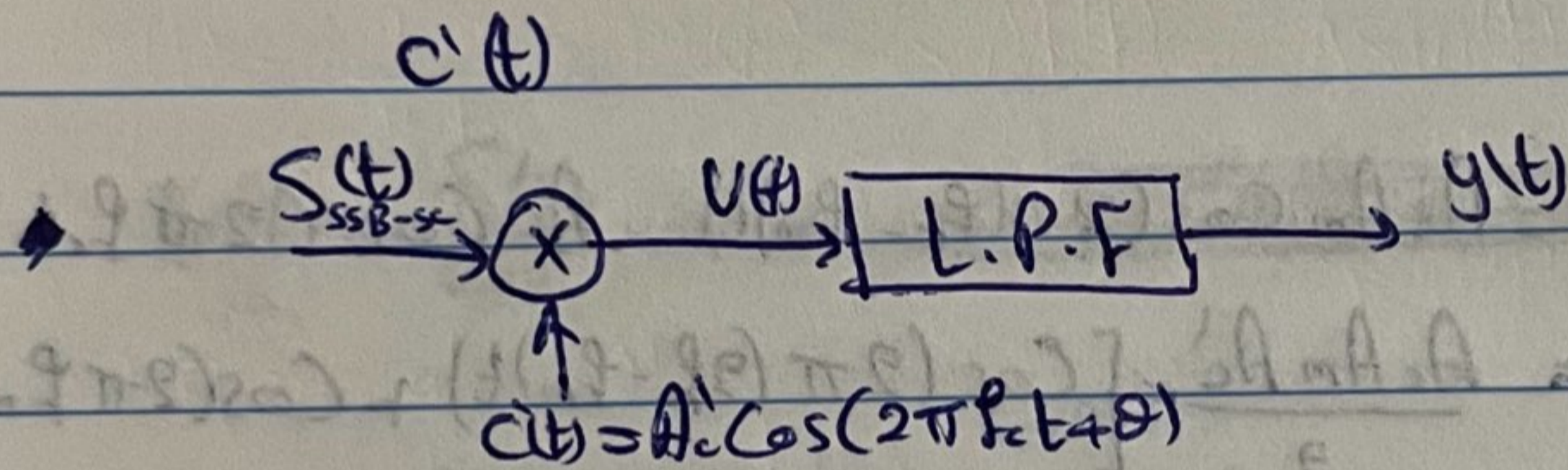
Demodulation of SSB-SC.

↓
Coherent

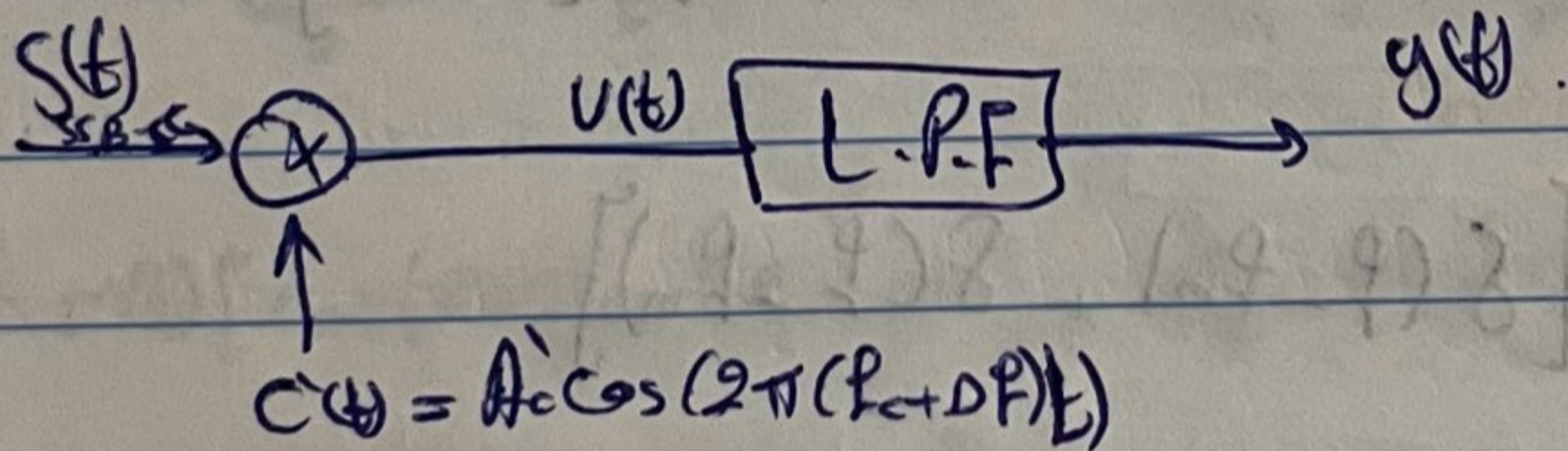


→ Non-Coherent

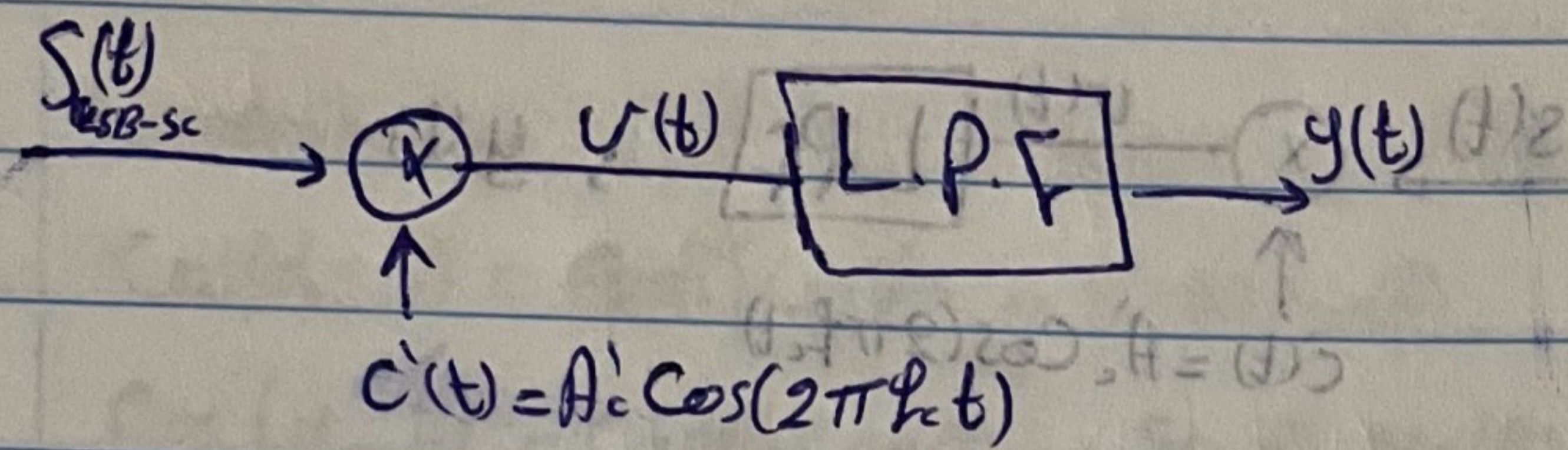
• Case 1: Constant phase difference between $c(t)$ and $c'(t)$



• Case 2: Constant freq. difference between $c(t)$ & $c'(t)$



Coherent Detector.



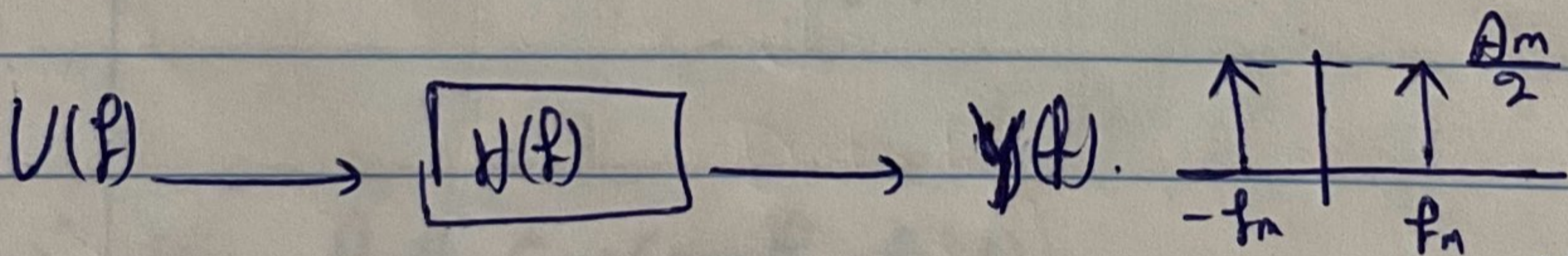
Let $m(t) = A_m \cos(2\pi f_m t)$.

$\Rightarrow S(t)_{USB-SC} = A_c A_m \cos(2\pi (f_c - f_m)t)$

$$V(t) = S(t)_{USB-SC} \cdot C'(t) = A_c A_m \cos(2\pi (f_c - f_m)t) \cdot A_c' \cos(2\pi f_c t)$$

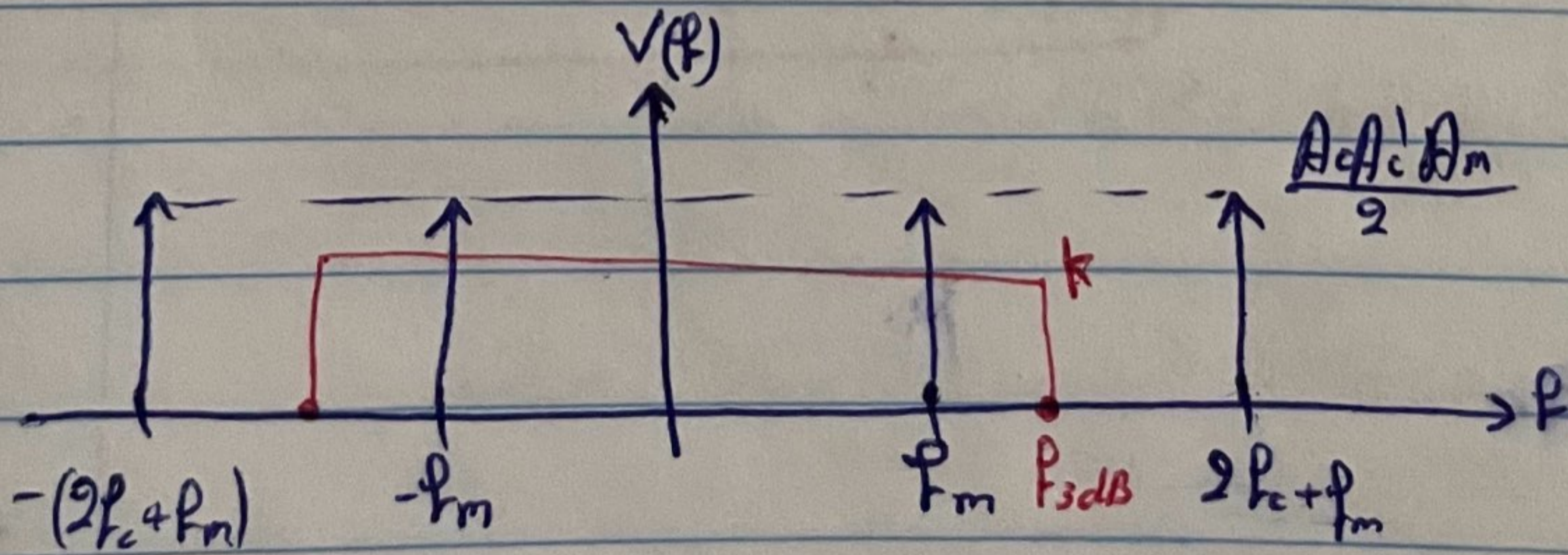
$$= \frac{A_c A_m A_c'}{2} [\cos(2\pi (2f_c - f_m)t) + \cos(2\pi f_m t)]$$

$$\rightarrow V(f) = \frac{A_c A_m A_c'}{4} [\delta(f - (2f_c - f_m)) + \delta(f + (2f_c - f_m))] + \frac{A_c A_m A_c'}{4} [\delta(f - f_m) + \delta(f + f_m)]$$



$$Y(f) = \frac{A_m}{2} [\delta(f - f_m) + \delta(f + f_m)]$$

$$y(t) = A_m \cos(2\pi f_m t)$$



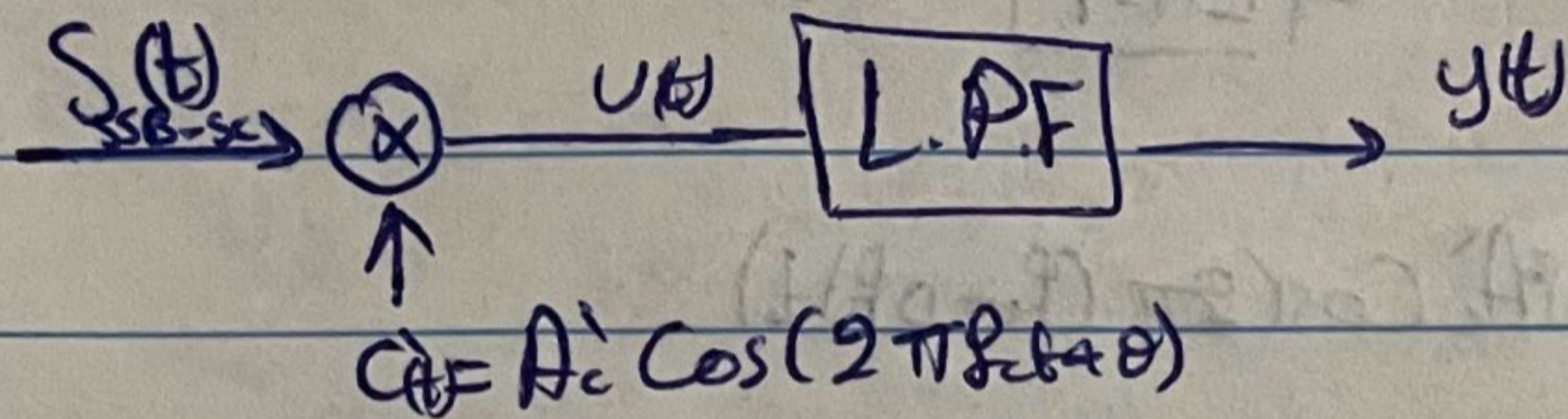
$$BW = f_m$$

$$f_m \leq P_{3dB} < 2f_c + f_m$$

$$(K) \left(\frac{A_c A_c' A_m}{A_c} \right) = \frac{A_m}{2} \Rightarrow \boxed{K = \frac{2}{A_c A_c'}}$$

≡ Non-Coherent Detector.

- Case 1:- Phase Constant difference between $c(t)$ & $c'(t)$.



$$S_{USB}(t) = A_c m(t) \cos(\omega_c t) - A_c \hat{m}(t) \sin(\omega_c t)$$

$$v(t) = \underbrace{S(t)}_{u_{SB}} \cdot \underbrace{c'(t)}_{A_c \cos(\omega_c t + \theta)}$$

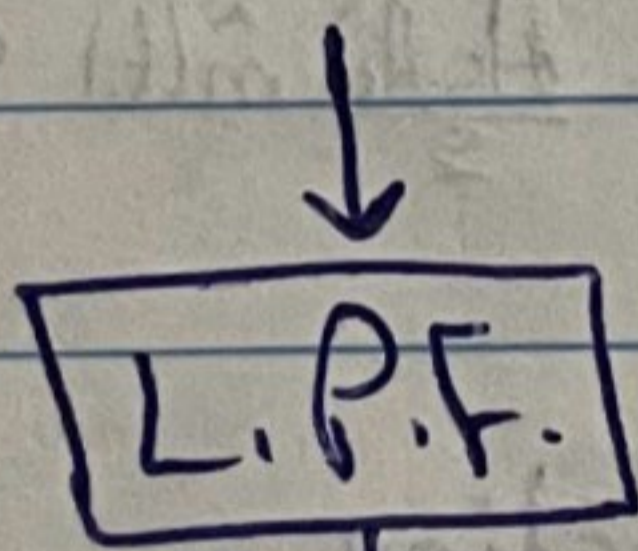
$$= [A_c m(t) \cos(\omega_c t) - A_c \hat{m}(t) \sin(\omega_c t)] [A_c \cos(\omega_c t + \theta)]$$

$$= A_c A_c m(t) \cos(\omega_c t) \cos(\omega_c t + \theta) - A_c A_c \hat{m}(t) \sin(\omega_c t) \cos(\omega_c t + \theta)$$

$$= \frac{A_c A_c}{2} m(t) [\cos(2\omega_c t + \theta) + \cos(\theta)] - \frac{A_c A_c}{2} \hat{m}(t) [\sin(2\omega_c t + \theta) + \sin(-\theta)]$$

$$\bullet \sin(\alpha) \cos(\beta) = \frac{1}{2} \sin(\alpha + \beta) + \frac{1}{2} \sin(\alpha - \beta)$$

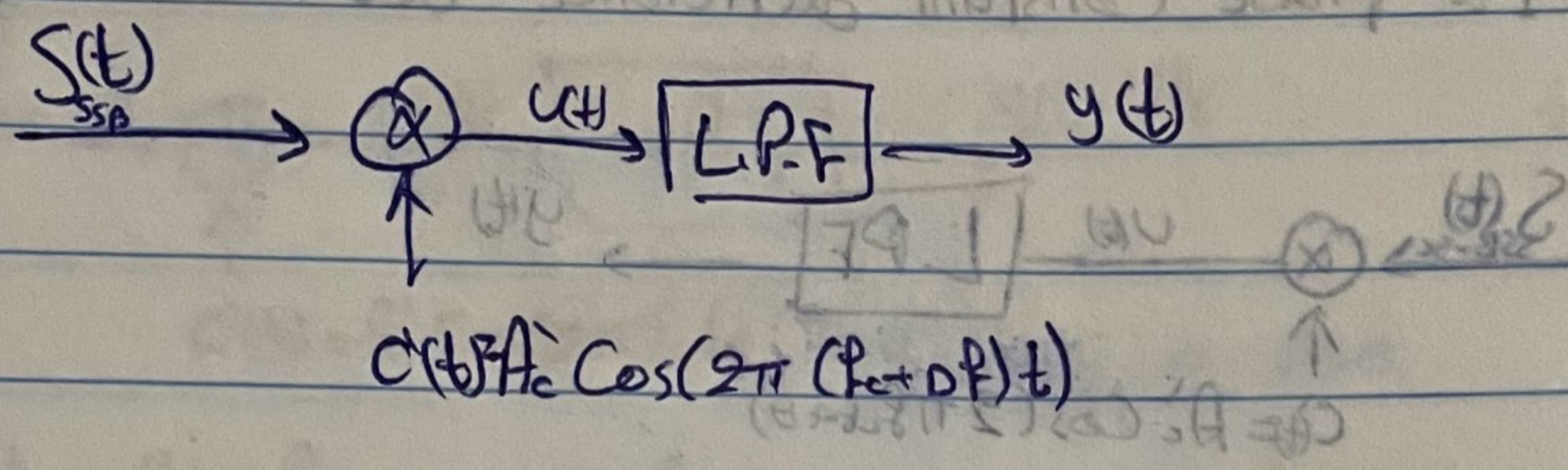
$$v(t) = \frac{A_c A_c}{2} m(t) [\cos(2\omega_c t + \theta) + \cos(\theta)] - \frac{A_c A_c}{2} \hat{m}(t) [\sin(2\omega_c t + \theta) + \sin(-\theta)]$$



$$y(t) = \frac{A_c A_c}{2} m(t) \cos(\theta) + \frac{A_c A_c}{2} \hat{m}(t) \sin(\theta)$$

↓
Distortion

Case 2: Constant freq. difference between $c(t)$ & $c'(t)$



$$S(t)_{USB} = A_c m(t) \cos(\omega_c t) - A_c \hat{m}(t) \sin(\omega_c t)$$

$$V(t) = S_{USB}(t) C'(t) = [A_c m(t) \cos(\omega_c t) - A_c \hat{m}(t) \sin(\omega_c t)] [A_c \cos(2\pi(f_c + \Delta f)t)]$$

$$= A_c A_c m(t) \cos(\omega_c t) \cos(2\pi(f_c + \Delta f)t) - A_c A_c \hat{m}(t) \sin(\omega_c t) \cos(2\pi(f_c + \Delta f)t)$$

$$V(t) = \frac{A_c A_c}{2} m(t) [\cos(2\pi(2f_c + \Delta f)t) + \cos(2\pi \Delta f t)] + \frac{A_c A_c}{2} \hat{m}(t) [\sin(2\pi(2f_c + \Delta f)t) - \sin(2\pi \Delta f t)]$$

↓
L.P.F.

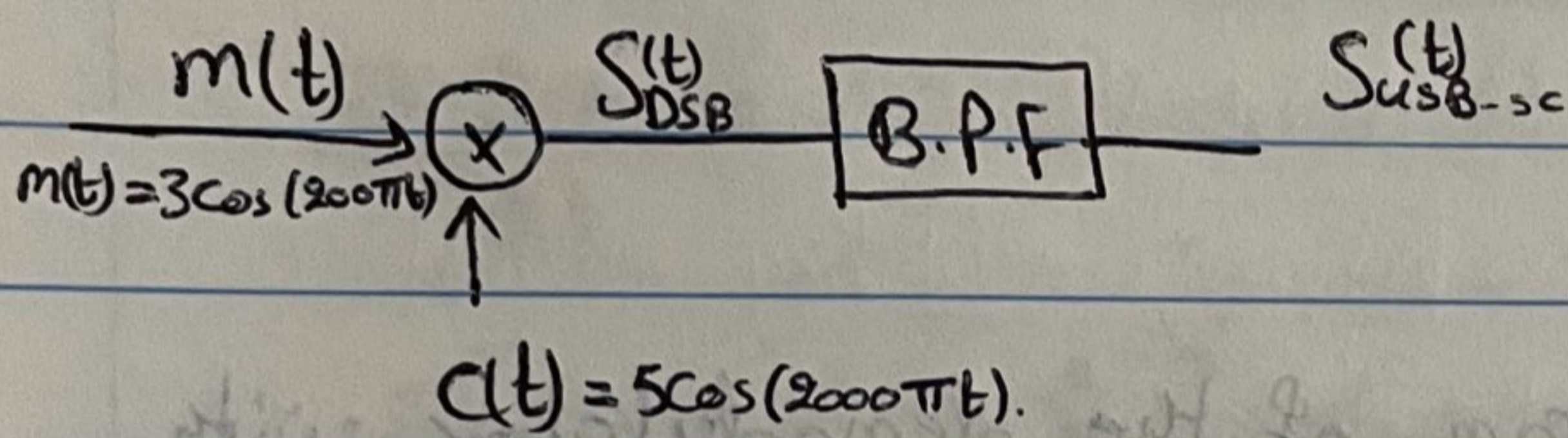
$$y(t) = \frac{A_c A_c}{2} m(t) \cos(2\pi \Delta f t) - \frac{A_c A_c}{2} \hat{m}(t) \sin(2\pi \Delta f t)$$

↓
Distortion.

Example The message signal $m(t) = 3 \cos(2000\pi t)$ along with carrier signal $c(t) = 5 \cos(2000\pi t)$ are applied to modulator that generates the upper side band suppressed carrier signal.

III Draw block diagram of modulator.

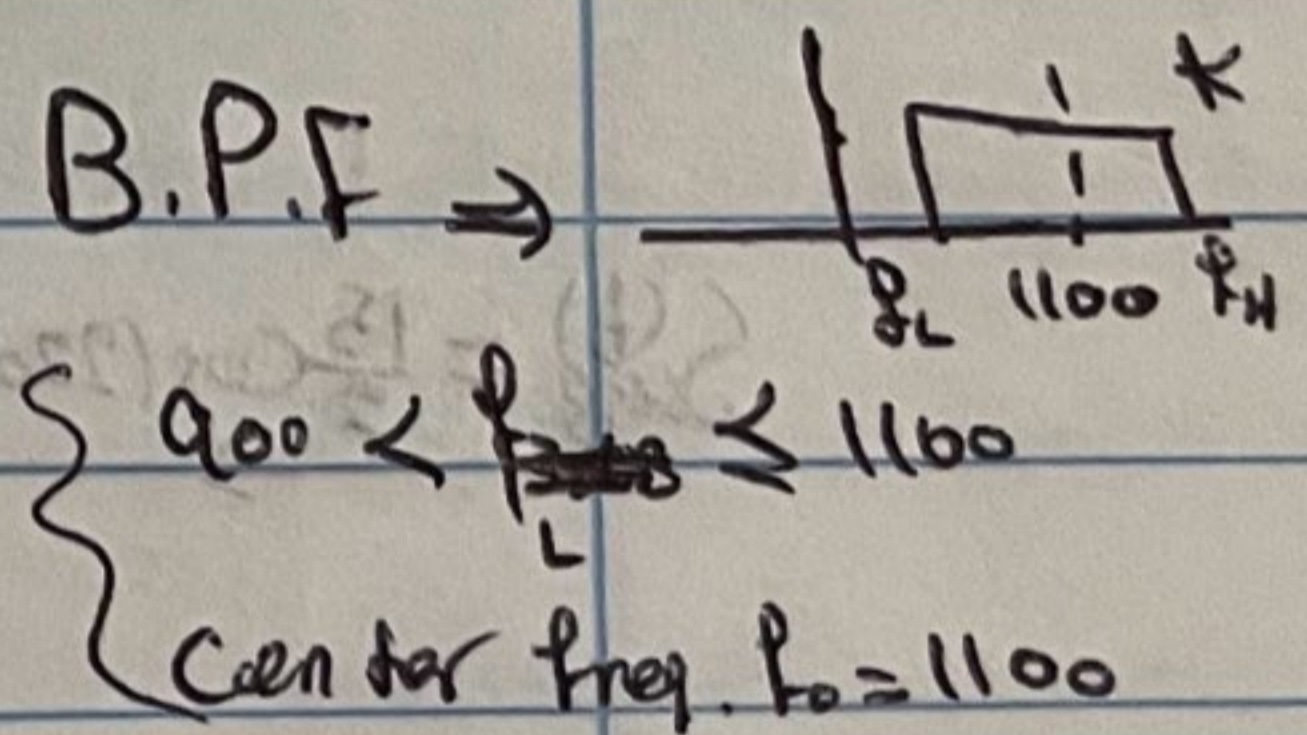
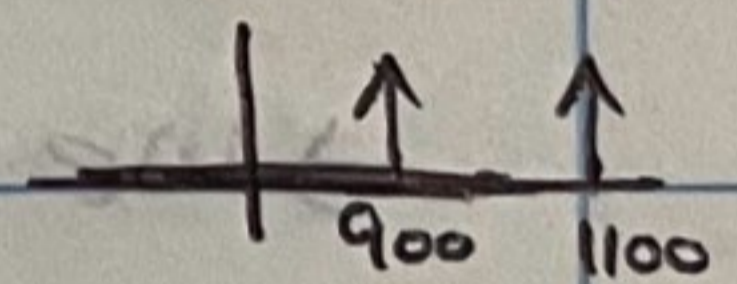
Ans: by using Filtering method.



$$S_{DSB}^{(t)} = m(t) c(t) = 15 \cos(2000\pi t) \cos(2000\pi t)$$

$$= \frac{15}{2} [\cos(4200\pi t) + \cos(1800\pi t)]$$

\uparrow \uparrow
 USB LSB



after B.P.F.

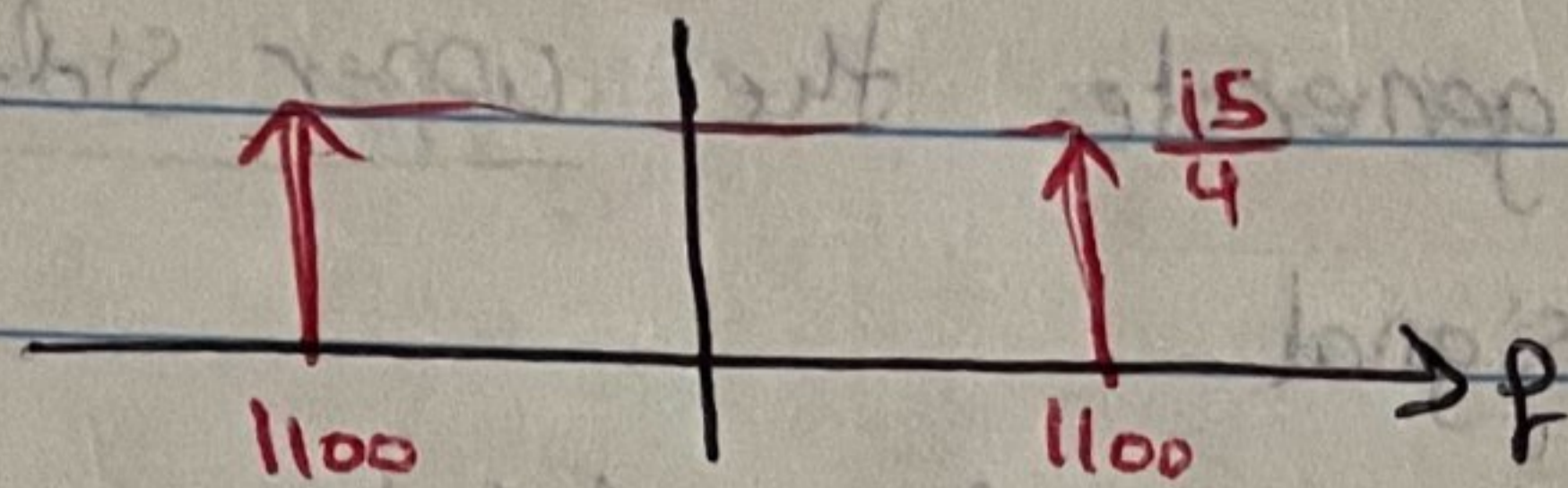
$$\Rightarrow S_{USB}^{(t)} = \frac{15}{2} \cos(4200\pi t)$$

IV write expression of modulation signal in time domain.

$$S_{USB}^{(t)} = \frac{15}{2} \cos(4200\pi t)$$

3) Evaluate and plot the spectrum of modulated signal.

$$S_{USB}(f) = \frac{15}{4} [\delta(f-1100) + \delta(f+1100)]$$



4) Evaluate the BW of modulated signal

$$B = 200 \text{ Hz}$$

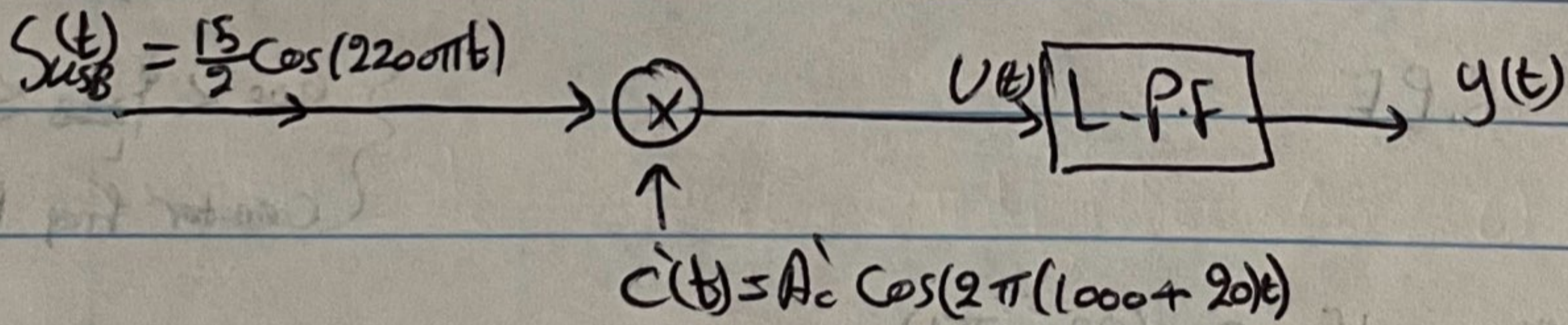
Pass band signal.

$$C(t) \rightarrow 1000$$

$$1100 - 1000 = 100$$

5) Draw block diagram of the demodulator with freq. distortion (\$\Delta f = 20 \text{ Hz}\$), specifying the details at each block.

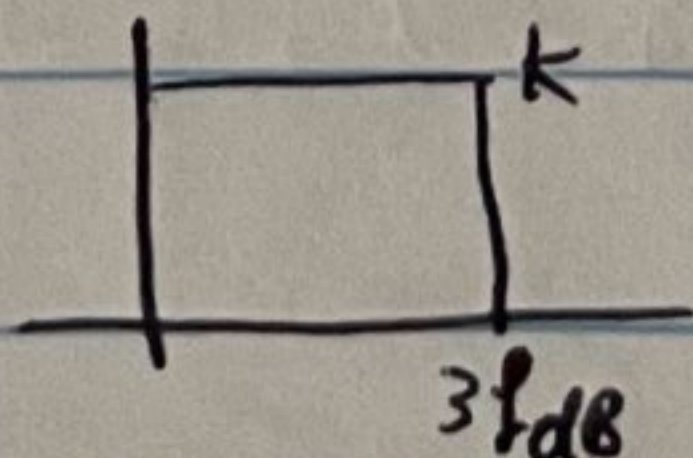
\$\Rightarrow\$ we have non-coherent detector with constant freq. difference between \$C(t)\$ & \$c(t)\$



$$U(t) = S_{USB}(t) C'(t) \Rightarrow \frac{15}{2} \cos(2200\pi t) \cdot A_c \cos(2\pi(1000+20)t)$$

$$= \frac{15}{2} \cdot \frac{A_c}{2} [\cos(2\pi(2f_c + \Delta f + f_m)t) + \cos(2\pi(f_m + \Delta f)t)]$$

\$\downarrow\$ L.P.F. \$\Delta f + 2f_c + f_m > f_{3dB} \geq f_m + \Delta f\$



$$\Rightarrow y(t) = \frac{15}{4} A_c \cos(2\pi(f_m + \Delta f)t) \neq m(t) \text{ [Distortion]}$$

L12

Continuous Communication System.

- Carrier signal.

$$c(t) = \underbrace{A_c}_{\text{Amp}} \cos(\underbrace{\phi(t)}_{\text{Angle}})$$

$$\frac{\partial \phi(t)}{\partial t} = \omega_i$$

$$\frac{\partial \phi_i(t)}{\partial t} = 2\pi f_i \quad \text{[Instantaneous freq.]}$$

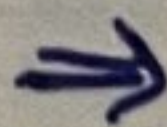
$$\Rightarrow f_i = \frac{1}{2\pi} \frac{\partial \phi_i(t)}{\partial t} \quad \text{①}$$

In FM:

$$f_i = f_c + K_f m(t) \quad \text{②}$$

$$\frac{1}{2\pi} \frac{\partial \phi_i(t)}{\partial t} = f_c + K_f m(t)$$

$$\begin{aligned} \Rightarrow \phi_i(t) &= \int_0^t 2\pi f_c \, d\tau + 2\pi K_f \int_0^t m(\tau) \, d\tau \\ &= 2\pi f_c t + 2\pi K_f \int_0^t m(\tau) \, d\tau \end{aligned}$$



≡ FM modulated signal.

$$S_{FM}(t) = A_c \cos(2\pi f_c t + 2\pi k_f \int_0^t m(\tau) d\tau) \quad \text{--- ③}$$

where, k_f : frequency sensitivity.

Now, Let $m(t) = A_m \cos(2\pi f_m t)$ --- ④

Remember:- $f_i = f_c + k_f m(t)$

→ $f_i - f_c = k_f m(t) \rightarrow \Delta f = k_f m(t)$ freq. deviation.

$$\Delta f_{\max} = k_f |m(t)|_{\max}$$

In our example.

$$\Delta f_{\max} = k_f A_m$$

By substituting ④ in ③.

$$\Rightarrow S_{FM}(t) = A_c \cos(2\pi f_c t + 2\pi k_f \int_0^t A_m \cos(2\pi f_m \tau) d\tau)$$

$$= A_c \cos(2\pi f_c t + \frac{2\pi k_f A_m}{2\pi f_m} \sin(2\pi f_m t))$$

$$= A_c \cos(2\pi f_c t + \frac{\Delta f_{\max}}{f_m} \sin(2\pi f_m t))$$

→ β : modulation index.

$$S_{FM}(t) = A_c \cos(\alpha t + \beta \sin(\beta t))$$

In general;

- $\cos(\alpha + \beta) = \cos(\alpha)\cos(\beta) - \sin(\alpha)\sin(\beta)$

- $\sin(\alpha)\sin(\beta) = \frac{1}{2}\cos(\alpha - \beta) - \frac{1}{2}\cos(\alpha + \beta)$

$$\Rightarrow S_{FM}(t) = A_c [\cos(2\pi f_c t) \cos(\beta \sin(2\pi f_m t)) - \sin(2\pi f_c t) \sin(\beta \sin(2\pi f_m t))]$$

- Remember, let $x(\theta) = \sin(\theta)$, if θ very small

$$\Rightarrow \sin(\theta) \approx \theta$$

$y(\theta) = \cos(\theta)$, if θ very small

$$\Rightarrow \cos(\theta) \approx 1$$

If $\beta \ll 1$ very small. (Narrow band).

$$\Rightarrow S_{FM}(t) = A_c [\cos(2\pi f_c t) - \sin(2\pi f_c t) \beta \sin(2\pi f_m t)]$$

$$= A_c [\cos(2\pi f_c t) - \frac{\beta}{2} \cos(2\pi(f_c - f_m)t) + \frac{\beta}{2} \cos(2\pi(f_c + f_m)t)]$$

If we compare $S_{FM}(t)$ in narrow band with $S_{AM}(t)$, we

can conclude.

$$S_{FM}(t) = A_c \cos(2\pi f_c t) - \frac{A_c \beta}{2} \cos(2\pi(f_c - f_m)t) + \frac{A_c \beta}{2} \cos(2\pi(f_c + f_m)t)$$

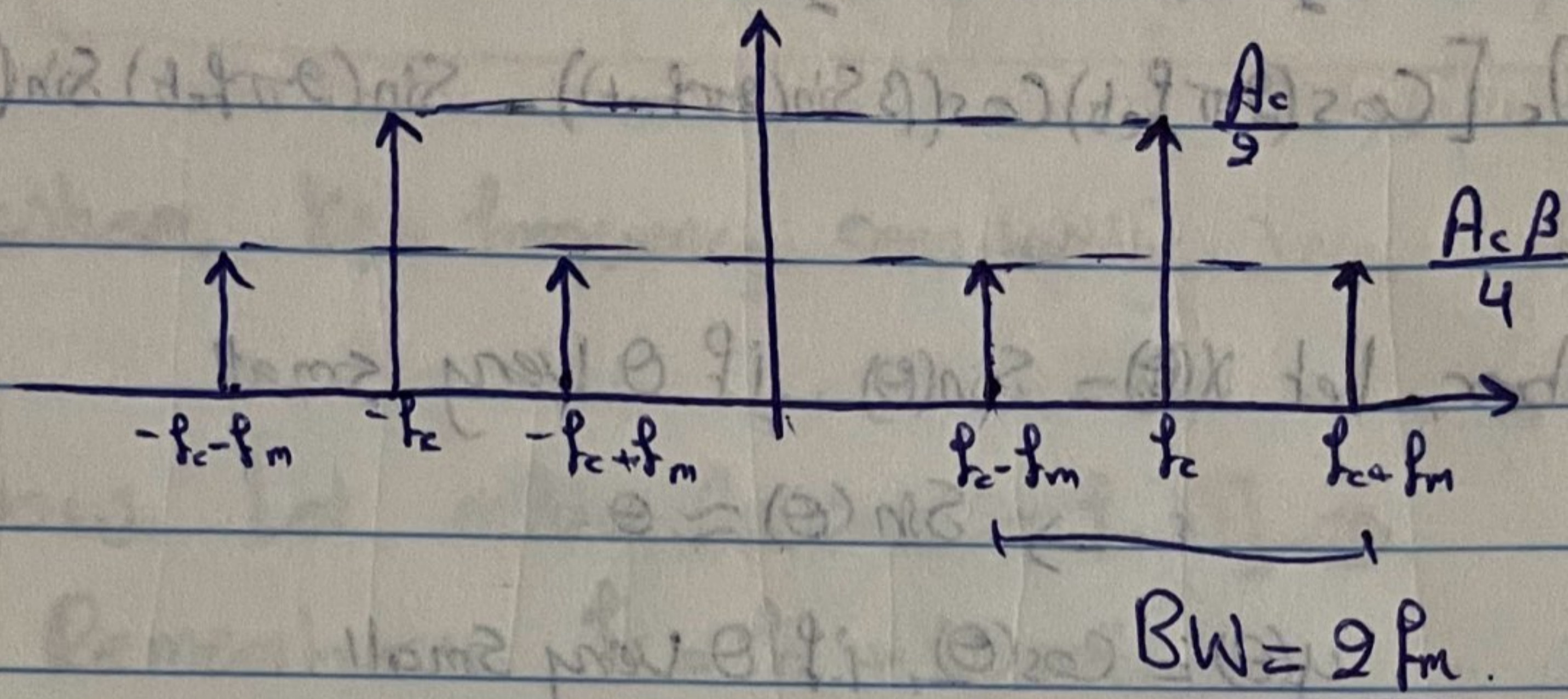
and.

$$S_{AM}(t) = A_c \cos(2\pi f_c t) + \frac{A_c \mu}{2} \cos(2\pi(f_c + f_m)t) + \frac{A_c \mu}{2} \cos(2\pi(f_c - f_m)t)$$

→

In FM :-

$$P_c = \frac{A_c^2}{2}, \quad P_{\text{sides}} = \frac{(A_c \beta)^2}{2} \cdot 2, \quad BW = 2f_m$$



Now, if $\beta \gg 1$. "wide band"

$$S_{\text{FM}}(t) = A_c \cos(2\pi f_c t + \beta \sin(2\pi f_m t)) \leftarrow \text{periodic signal.}$$

$$= \text{Re} \left\{ A_c e^{j(2\pi f_c t)} \cdot e^{j\beta \sin(2\pi f_m t)} \right\} \quad \text{--- (5)}$$

Periodic signal

$$e^{j\beta \sin(2\pi f_m t)} = \sum_{n=-\infty}^{\infty} C_n e^{j2\pi n f_m t}$$

$$C_n = \frac{1}{T_m} \int_{T_m} e^{j\beta \sin(2\pi f_m t)} e^{-j2\pi n f_m t} dt$$

$$= \sum_{n=-\infty}^{\infty} J_n(\beta) e^{j2\pi n f_m t} \quad \text{--- (6)}$$

$J_n(\beta)$: Bessel function.

Some Properties of $J_n(x)$:

$$5 - \sum_{n=-\infty}^{\infty} (J_n(x))^2 = 1, \text{ for all } x.$$

$$1 - J_n(x) = (-1)^n J_{-n}(x)$$

$$2 - J_n(x) = (-1)^n J_n(-x)$$

$$3 - J_{n-1}(x) + J_{n+1}(x) = \frac{2n}{x} J_n(x)$$

4 - For small value of x

$$J_n(x) \approx \frac{x^n}{2^n n!}$$

$$J_0(x) = 1$$

$$J_1(x) = \frac{x}{2}$$

$$\Rightarrow S_{FM}(t) = \text{Re} \left\{ A_c e^{j2\pi f_c t} \cdot \sum_{n=-\infty}^{\infty} J_n(\beta) e^{-j2\pi n f_m t} \right\}$$

$$= \text{Re} \left\{ A_c \sum_{n=-\infty}^{\infty} J_n(\beta) e^{j2\pi (f_c - n f_m) t} \right\}$$

$$S_{FM}(t) = A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \cos(2\pi (f_c - n f_m) t)$$

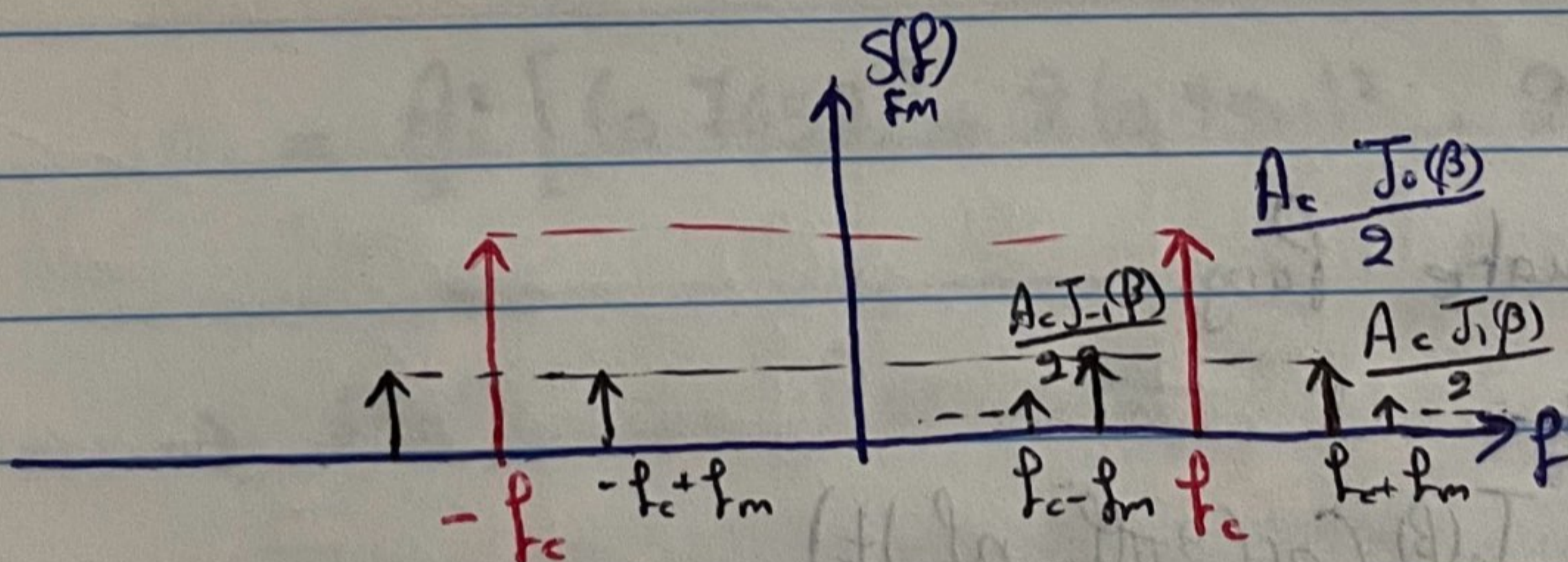
- To evaluate total power.

$$P_T = \frac{A_c^2}{2} \sum_{n=-\infty}^{\infty} J_n^2(\beta) \Rightarrow P_T = \frac{A_c^2}{2}$$

Since.

$$S_{FM}(t) = A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \cos(2\pi (f_c - n f_m) t)$$

$$S_{FM}(f) = \frac{A_c}{2} \sum_{n=-\infty}^{\infty} J_n(\beta) [\delta(f - f_c + n f_m) + \delta(f + f_c + n f_m)]$$



$$BW = 2n f_m$$

Carrier Power:

$$P_c = 2 \cdot \left(\frac{A_c}{2} J_0(\beta) \right)^2 \Rightarrow P_c = \frac{A_c^2}{2} J_0^2(\beta)$$

[13]

if $\beta = 0.2$.

$$P_{avg} = \frac{A_c^2}{2} [J_0^2(0.2) + 2J_1^2(\beta) + \dots]$$
$$= \frac{A_c^2}{2} [(0.99)^2 + 2(0.00498)^2] \times 100\%$$

$$\Rightarrow n=1 \Rightarrow BW = (2)(1) f_m$$

$$\Rightarrow BW = 2 f_m.$$

if $\beta = 1$.

$$J_0(1) = 0.7652, J_1(1) = 0.4401, J_2(1) = 0.1149$$

$$J_3(1) = 0.0195, J_4(1) = 0.002477.$$

$$P_{avg} = \frac{A_c^2}{2} [J_0^2(1) + 2J_1^2(1) + 2J_2^2(1) + \dots]$$

$$= \frac{A_c^2}{2} [(0.7652)^2 + 2(0.4401)^2 + 2(0.1149)^2]$$

$$\Rightarrow n=2 \rightarrow BW = (2)(2) f_m$$

$$\Rightarrow BW = 4 f_m.$$

- at 98% Power band width \Rightarrow using Carson's Rule.

• $BW = 2(\beta + 1) f_m$ •

\equiv Generation of an FM signal

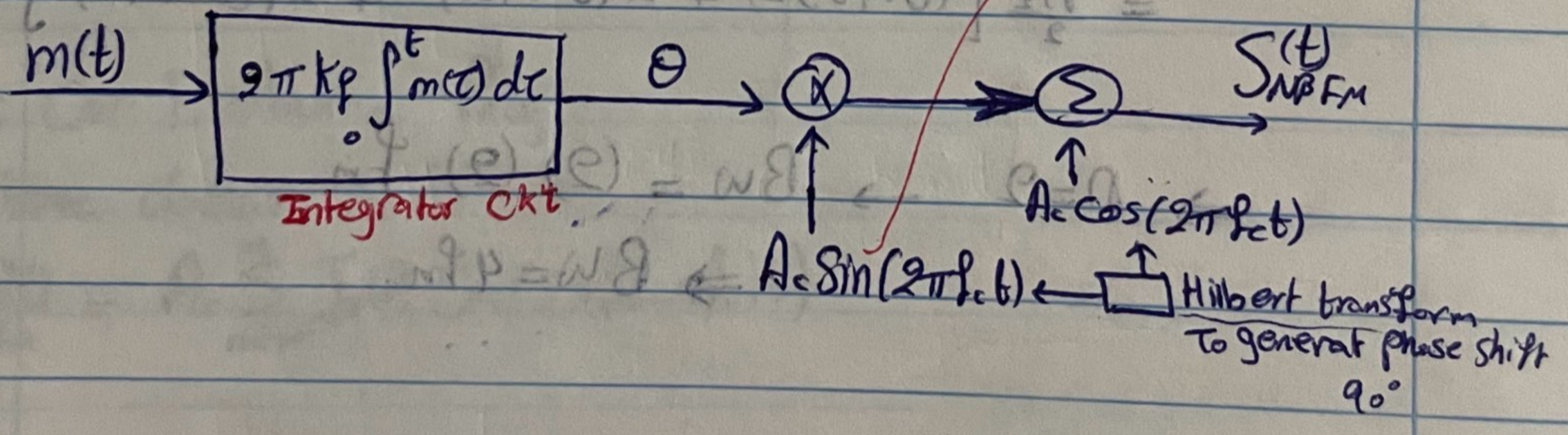
$S_{FM}(t) = A_c \cos(2\pi f_c t + \underbrace{2\pi k_f \int_0^t m(\tau) d\tau}_{\theta})$

• if $m(t) = A_m \cos(2\pi f_m t)$

$\hookrightarrow S_{FM}(t) = A_c \cos(2\pi f_c t) \cos(\beta \sin(2\pi f_m t)) - A_c \sin(2\pi f_c t) \sin(\beta \sin(2\pi f_m t))$

In NBFM

$S_{FM}(t) = A_c \cos(2\pi f_c t) - A_c \beta \sin(2\pi f_m t) \sin(2\pi f_c t)$



In NBFM.

$$S_{FM}(t) = A_c \cos(2\pi f_c t + \beta \sin(2\pi f_m t))$$

$$= A_c \cos(2\pi f_c' t + \beta' \sin(2\pi f_m t)) \rightarrow A_c \cos(2\pi f_c t + \beta \sin(2\pi f_m t))$$

NBFM

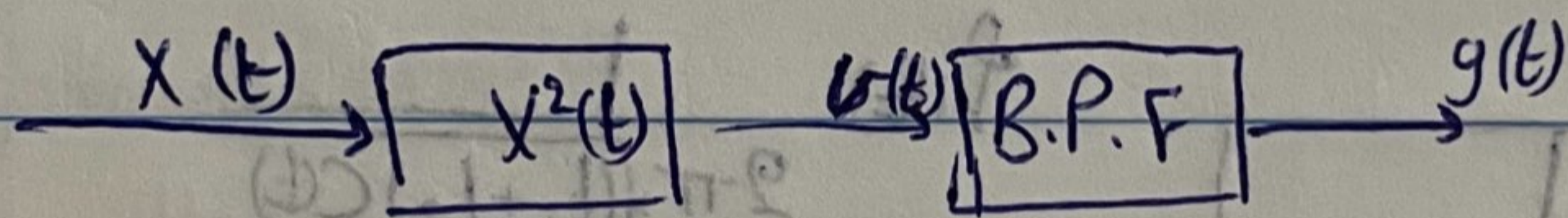
WBFM

$$f_c = n f_c'$$

$$\beta = n \beta'$$

= Frequency Multiplier.

Example The Square Law device



$$\text{Let } X(t) = A_c \cos(\phi(t)) = A_c \cos(2\pi f_c' t + \beta' \sin(2\pi f_m t))$$

$$V(t) = (A_c \cos(\phi(t)))^2 = A_c^2 \cos^2(\phi(t))$$

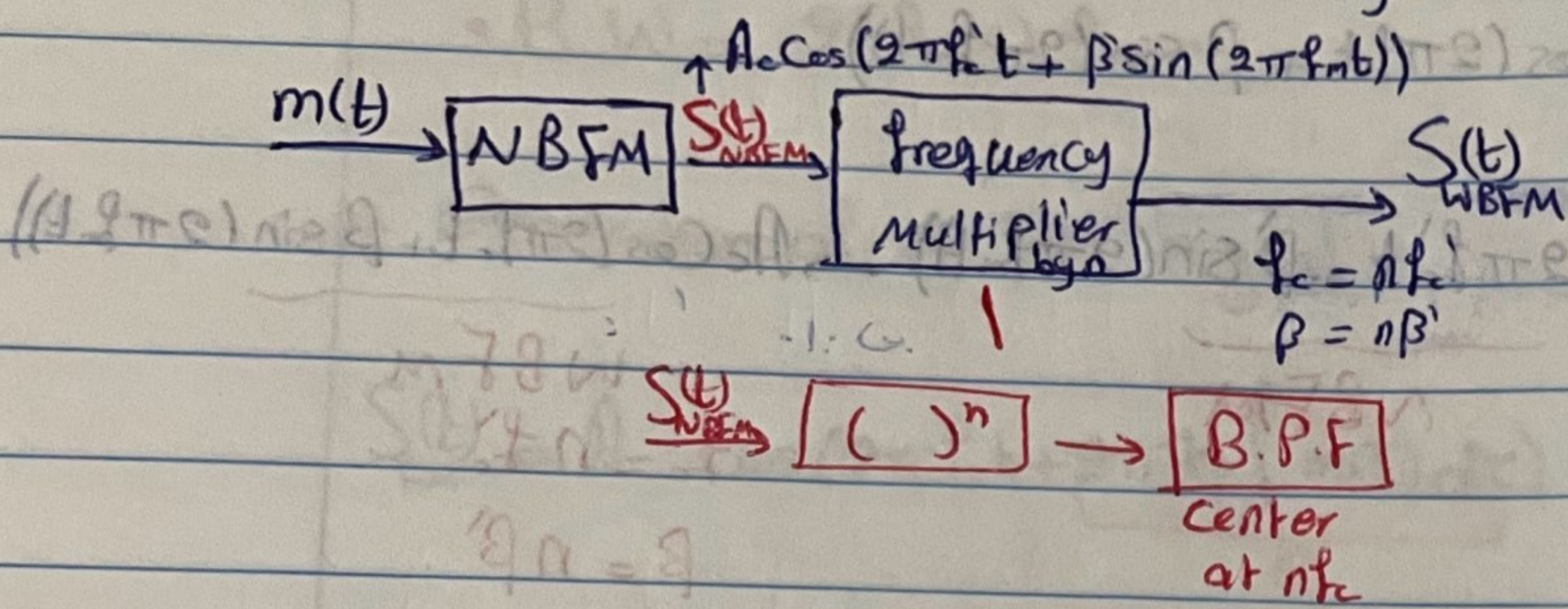
$$= \frac{A_c^2}{2} + \frac{A_c^2}{2} \cos(2\phi(t))$$

$$= \frac{A_c^2}{2} + \frac{A_c^2}{2} \cos(2\pi(2f_c')t + (2\beta') \sin(2\pi f_m t))$$

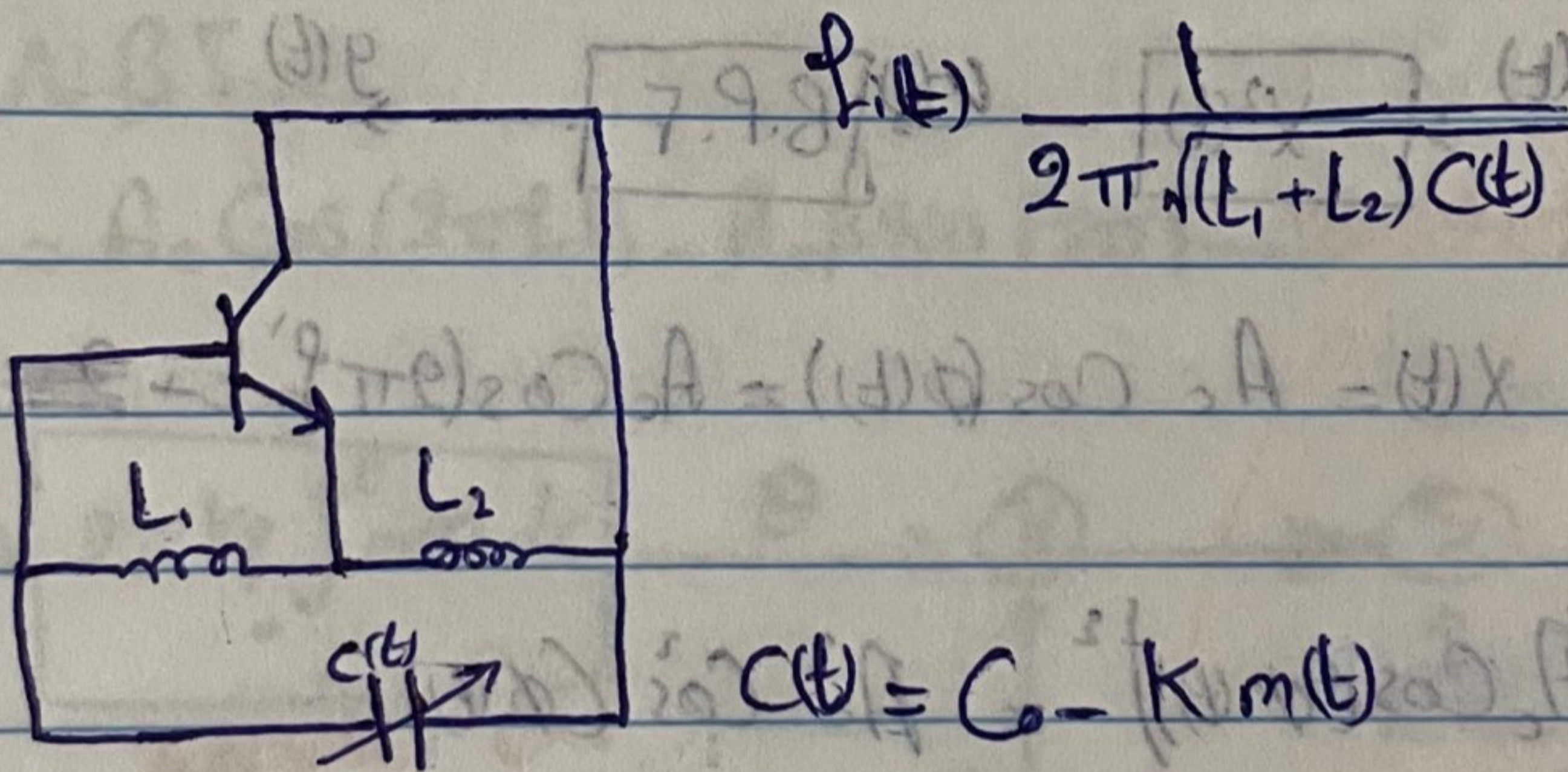
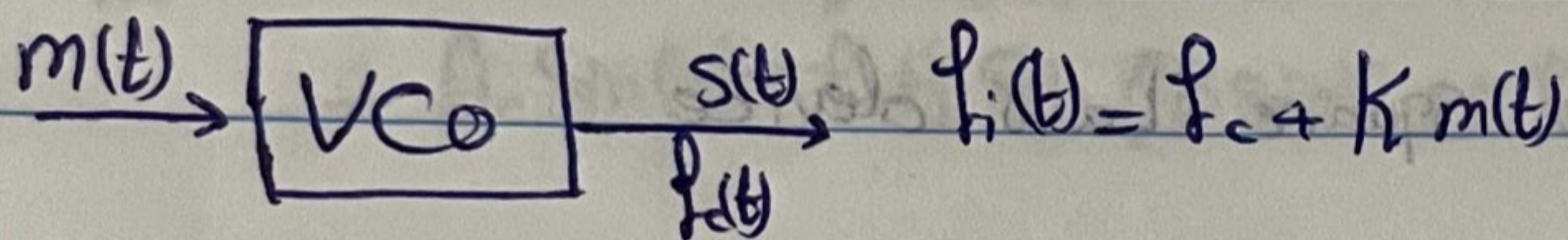
B.P.F.

$$\Rightarrow g(t) = \frac{A_c^2}{2} \cos(2\pi(2f_c')t) + 2\beta' \sin(2\pi f_m t)$$

⇒ Indirect Method for Generating a wideband FM



≡ Direct method



⇒ $f_i(t) = \frac{1}{2\pi \sqrt{(L_1 + L_2) (C_0 - K_f m(t))}}$

7.9.9

$$= \frac{1}{2\pi \sqrt{(L_1 + L_2) C_0 (1 - \frac{K_f m(t)}{C_0})}} = \frac{1}{2\pi \sqrt{(L_1 + L_2) C_0} \cdot \sqrt{1 - \frac{K_f m(t)}{C_0}}}$$



$$f_c(t) = \frac{1}{2\pi \sqrt{(L_1 + L_2) C_0}}$$

$$\Rightarrow f_i(t) = f_c \cdot \left(1 - \frac{K_m(t)}{C_0}\right)^{-1/2}; \text{ if } \frac{K_m(t)}{C_0} \ll 1$$
$$\Rightarrow (1-x)^{-1/2} = 1 + \frac{1}{2}x$$

$$f_i(t) = f_c \left(1 + \frac{K_m(t)}{C_0}\right)$$

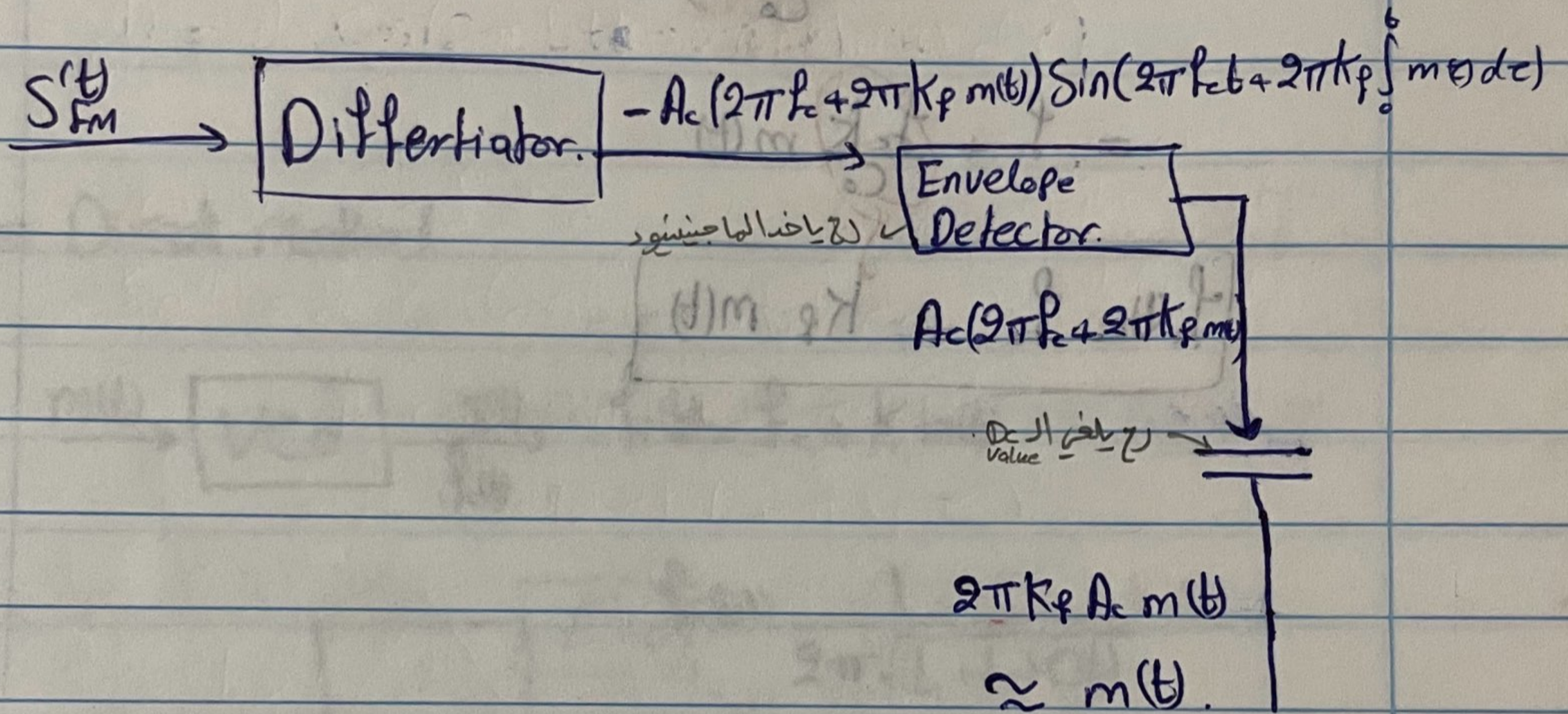
$$= f_c + \frac{f_c K_m(t)}{C_0}$$

$$f_i(t) = f_c + K_f m(t)$$

Demodulation of the FM.

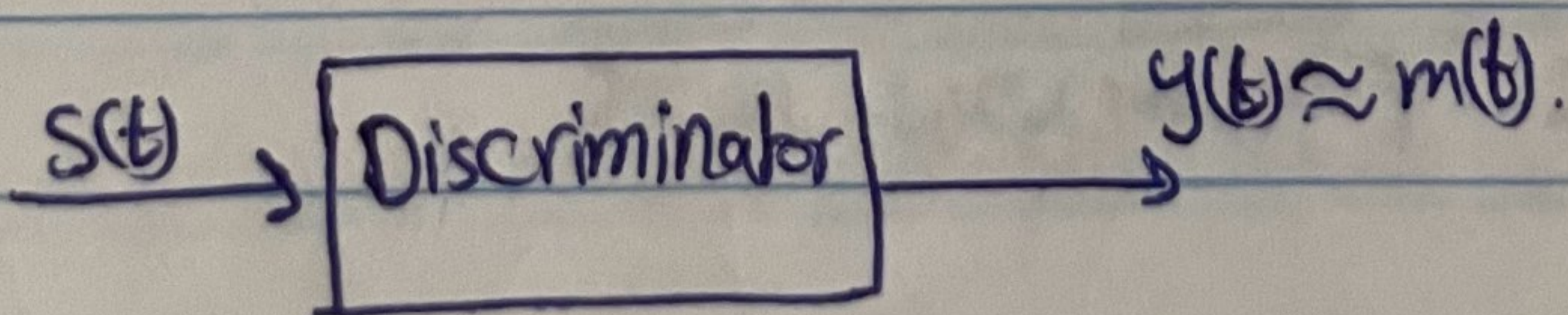
$$S_{FM}(t) = A_c \left(1 + k_f \int_0^t m(\tau) d\tau \right)$$

$$\rightarrow S_{FM}(t) = A_c \cos \left(2\pi f_c t + 2\pi k_f \int_0^t m(\tau) d\tau \right)$$



To demodulate FM \Rightarrow we can use Differentiator following by an envelope detector

- In general, to demodulate FM signal, we can use discriminator



(L14)

Example Consider the message signal $g(t)$.

$$g(t) = \begin{cases} t, & 0 \leq t \leq T \\ 0, & \text{o.w} \end{cases}; T = 2 \text{ sec.}$$

$g(t)$ is applied to an FM modulation with sensitivity $k_f = 2 \text{ Hz/V}$ to produce an FM signal $s(t)$. The unmodulated carrier frequency is 100 Hz , a) Find and plot the instantaneous freq. of $s(t)$ versus time.

$$\begin{aligned} \text{a) } f_i(t) &= f_c + k_f m(t) \\ &= 100 + 2g(t) = \begin{cases} 100 + 2t, & 0 \leq t \leq T \\ 100, & \text{o.w} \end{cases} \end{aligned}$$

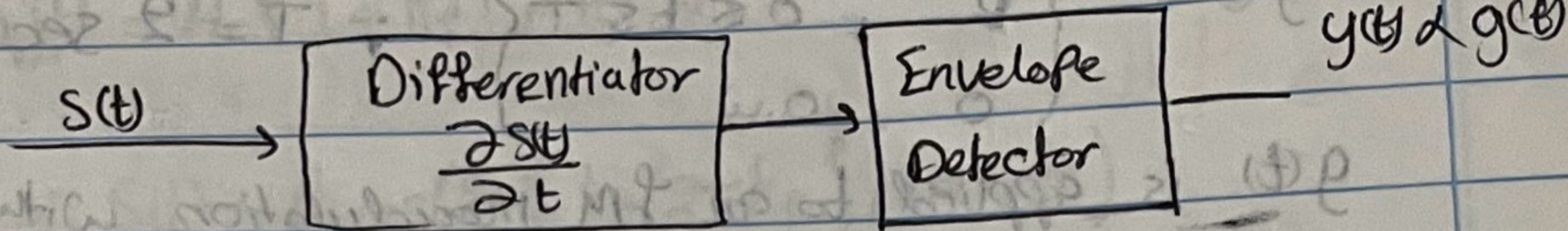
b) Find the peak freq. deviation of $s(t)$.

$$\Delta f = f_i(t) - f_c = k_f m(t)$$

$$\rightarrow (\Delta f)_{\max} = f_i(t)_{\max} - f_c$$

$$= 104 - 100 \Rightarrow 4 \text{ Hz}$$

c) Suggest a method via which $g(t)$ can be recovered from $s(t)$.



$$s_{FM}(t) = A_c \cos(2\pi f_c t + 2\pi k_f \int_0^t m(\tau) d\tau)$$

when $0 \leq t \leq T$

$$\begin{aligned} \rightarrow s_{FM}(t) &= A_c \cos(2\pi f_c t + 2\pi k_f \int_0^t \tau d\tau) \\ &= A_c \cos(2\pi f_c t + \frac{2\pi k_f t^2}{2}) \\ &= A_c \cos(2\pi f_c t + \pi k_f T^2) \end{aligned}$$

In general:

$$s_{FM}(t) = A_c \cos(2\pi f_c t + 2\pi k_f \int_0^t \tau d\tau)$$

$$= A_c \cos(2\pi f_c t + 2\pi k_f t^2)$$

for $t > T$

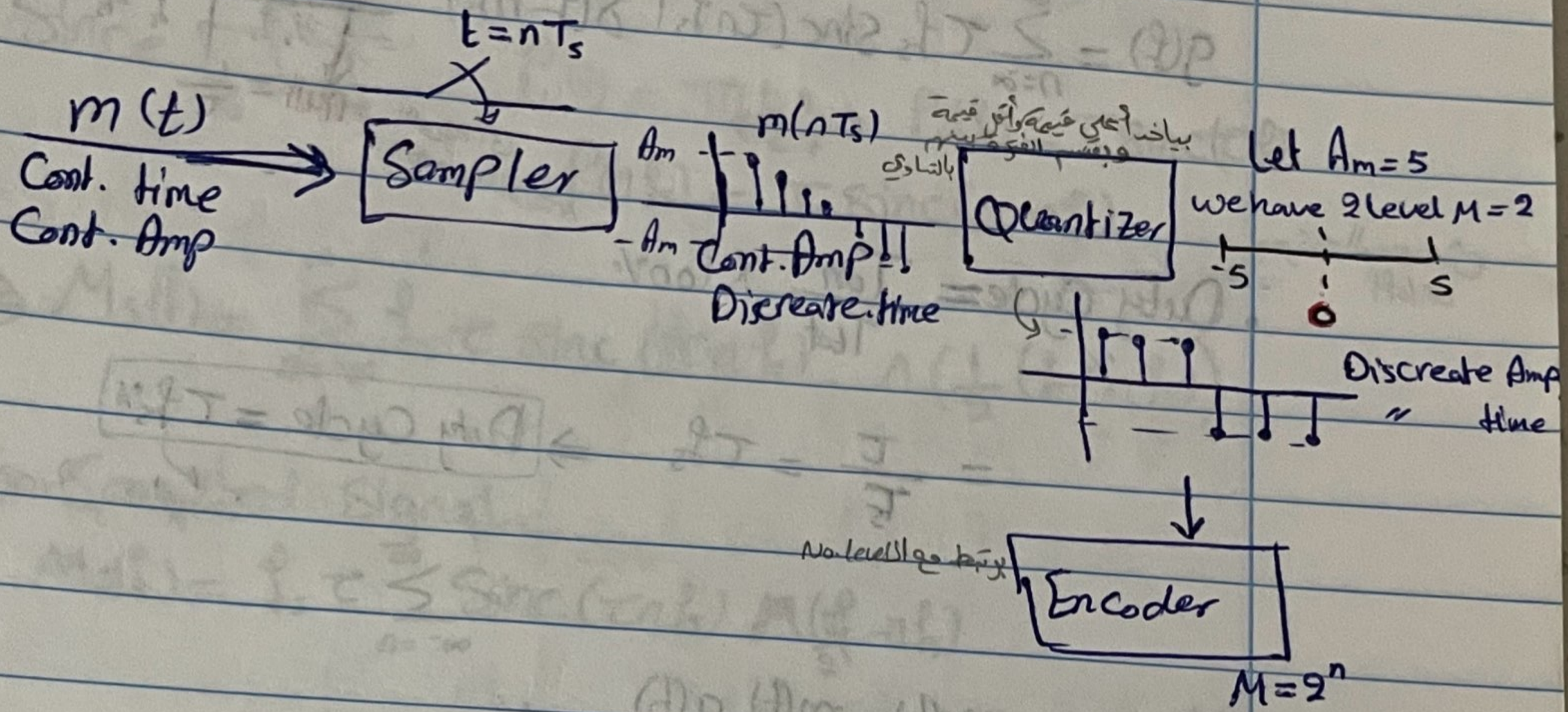
$$s_{FM}(t) = A_c \cos(2\pi f_c t + 4\pi k_f T^2)$$

for $t < 0$

$$s_{FM}(t) = A_c \cos(2\pi f_c t)$$

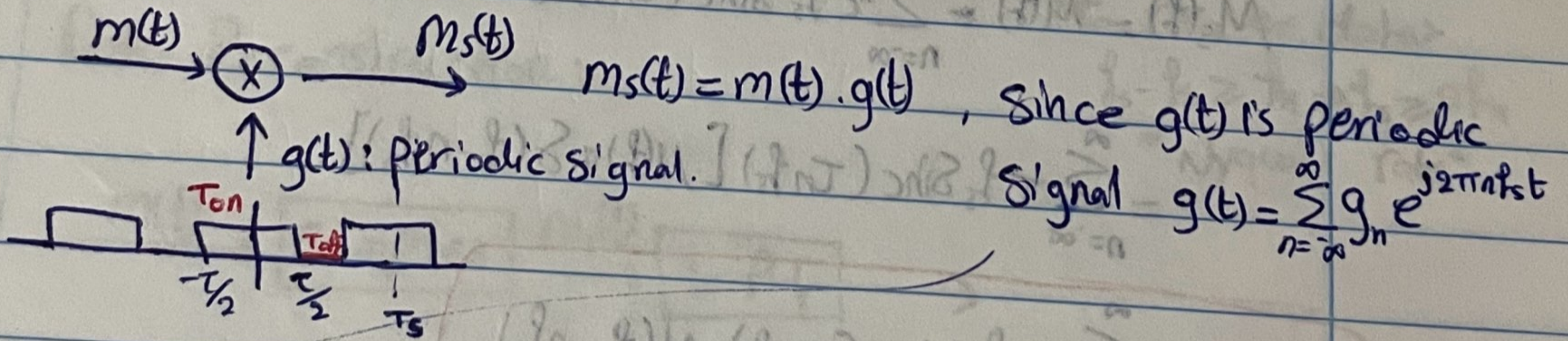
Analog modulation ADC Digital modulation

In ADC

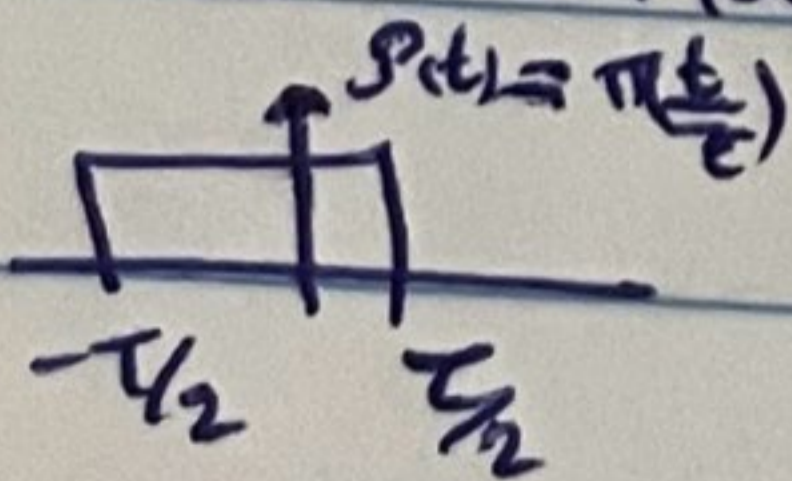


≡ Sampler $t = nT_s$: PAM
Pulse Amp. modulation.

$m(t)$ $t = nT_s$ $m_s(t)$: Sampled signal.



To evaluate g_n .



$$P(f) = \int_{-\tau/2}^{\tau/2} e^{-j2\pi f t} dt = \tau \text{sinc}(\tau f)$$

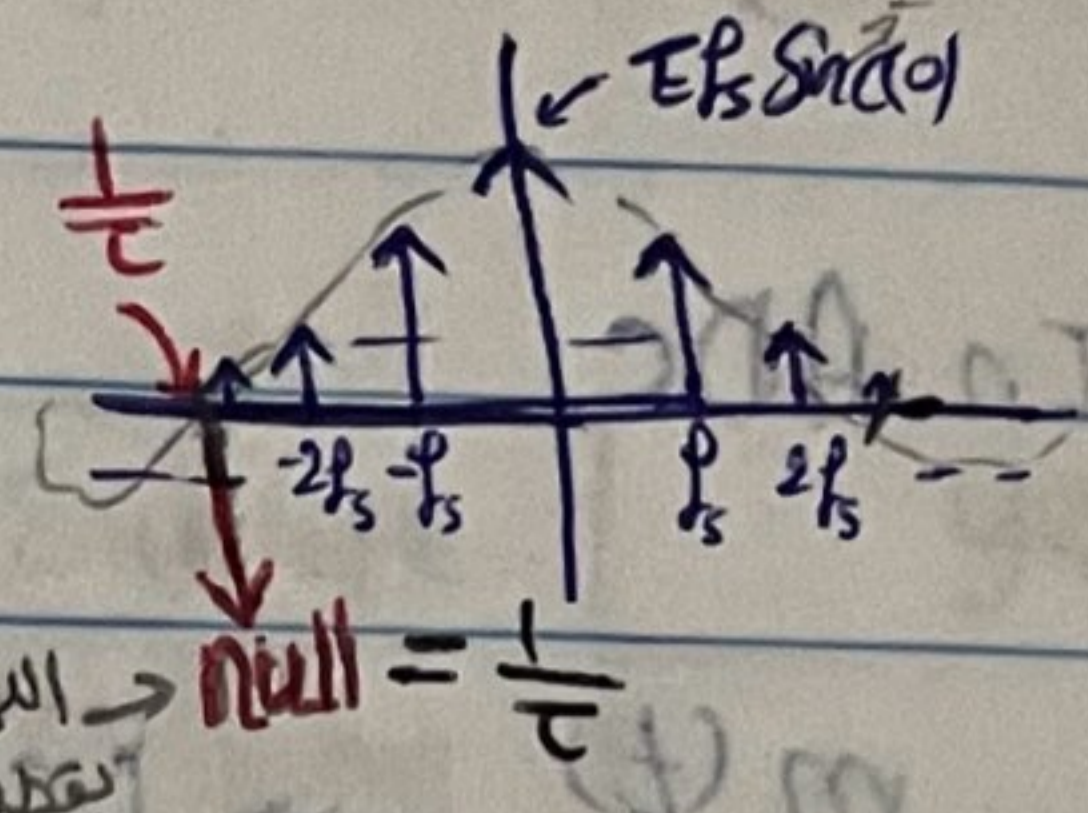
$$P(n f_s) = \tau \text{sinc}(\tau n f_s)$$

$$\Rightarrow \underline{g_n = \int_{-\tau/2}^{\tau/2} P(n f_s) = \tau f_s \text{sinc}(\tau n f_s)}$$

→

$$g(t) = \sum_{n=-\infty}^{\infty} \tau f_s \operatorname{sinc}(\tau n f_s) e^{j2\pi n f_s t}$$

$$g(f) = \sum_{n=-\infty}^{\infty} \tau f_s \operatorname{sinc}(\tau n f_s) \delta(f - n f_s)$$



• Duty Cycle = $\frac{T_{on}}{T_{tot}} \times 100\%$

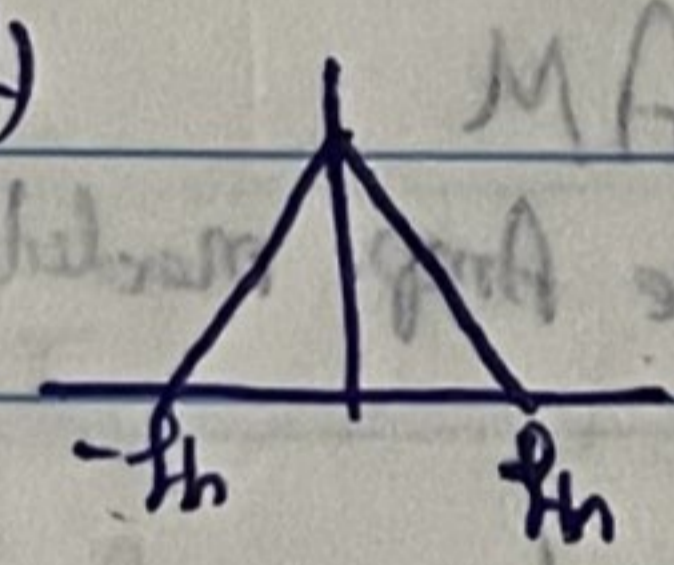
$$= \frac{\tau}{T_s} = \tau f_s \Rightarrow \boxed{\text{Duty Cycle} = \tau f_s \%}$$

Sampling freq

Since $m_s(t) = m(t) g(t)$

$$M_s(f) = M(f) * G(f)$$

Let $M(f)$



$$m(t) = \operatorname{sinc}(\tau f)$$

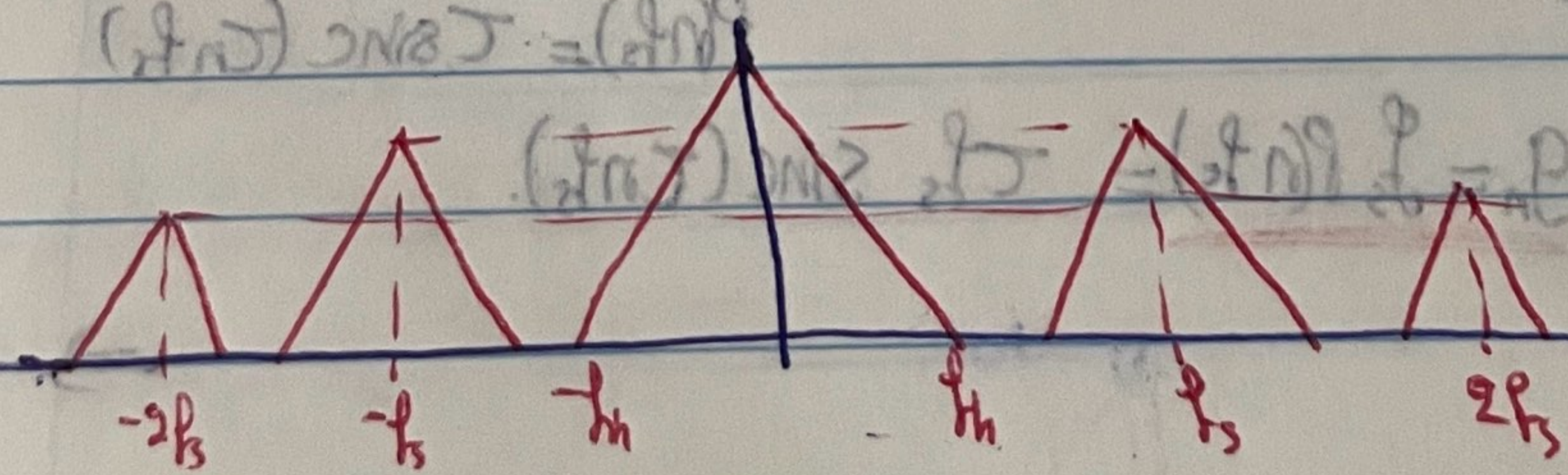
$$M(f) = \frac{1}{\tau} \operatorname{rect}\left(\frac{f}{2f_h}\right)$$

$$M_s(f) = M(f) * \sum_{n=-\infty}^{\infty} \tau f_s \operatorname{sinc}(\tau n f_s) \delta(f - n f_s)$$

$$= \sum_{n=-\infty}^{\infty} \tau f_s \operatorname{sinc}(\tau n f_s) [M(f) * \delta(f - n f_s)]$$

$$M_s(f) = \sum_{n=-\infty}^{\infty} \tau f_s \operatorname{sinc}(\tau n f_s) M(f - n f_s)$$

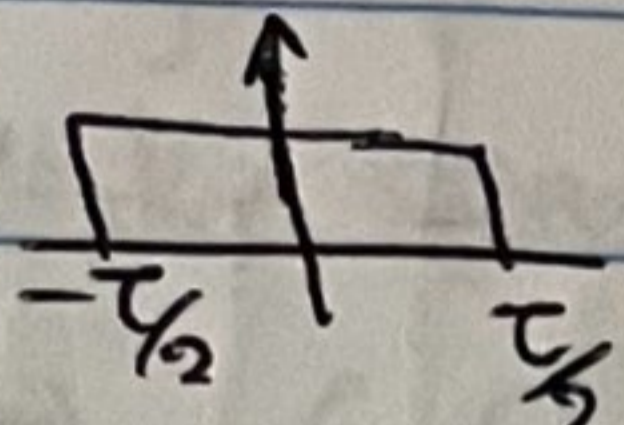
To plot $M_s(f)$



L(15)

Now, Let $m(t) = 2 \text{sinc}^2(2t)$

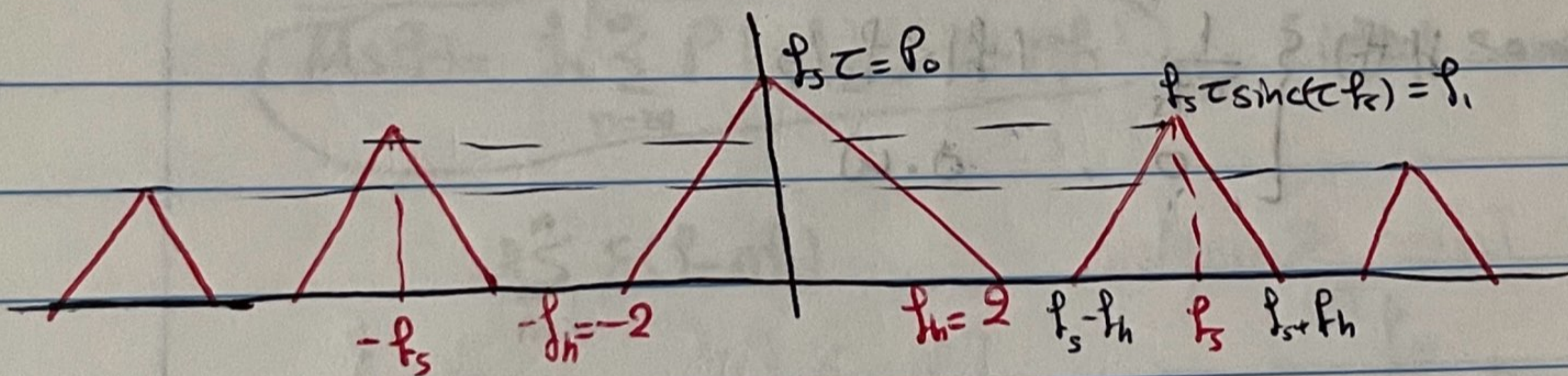
$$\Rightarrow M(f) = 2 \cdot \frac{1}{2} \wedge\left(\frac{f}{2}\right) \Rightarrow M(f) = \wedge\left(\frac{f}{2}\right)$$

Since  $P_i(t) = \pi\left(\frac{t}{\tau}\right) \Rightarrow P_i(f) = \tau \text{sinc}(\tau f)$
 $P(nf_s) = \tau \text{sinc}(\tau n f_s)$

$$\Rightarrow M_s(f) = \sum_{n=-\infty}^{\infty} f_s \tau \text{sinc}(\tau n f_s) \cdot \wedge\left(\frac{1}{2}(f - n f_s)\right)$$

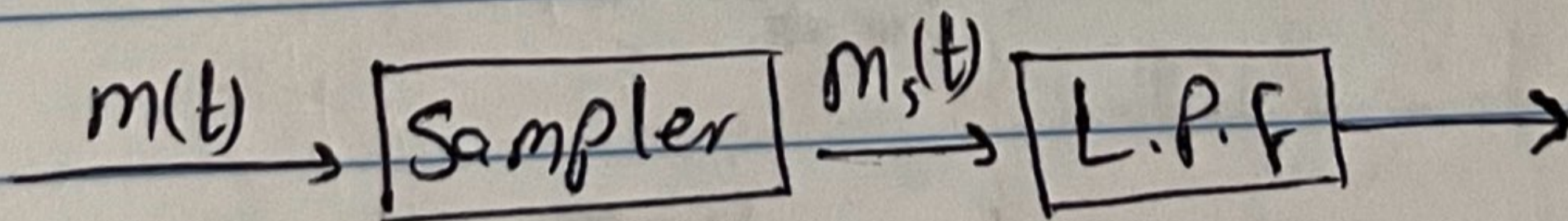
In Sampled Signal.

$$M_s(f) = f_s \tau \sum_{n=-\infty}^{\infty} \text{sinc}(\tau n f_s) \wedge\left(\frac{f - n f_s}{2}\right)$$

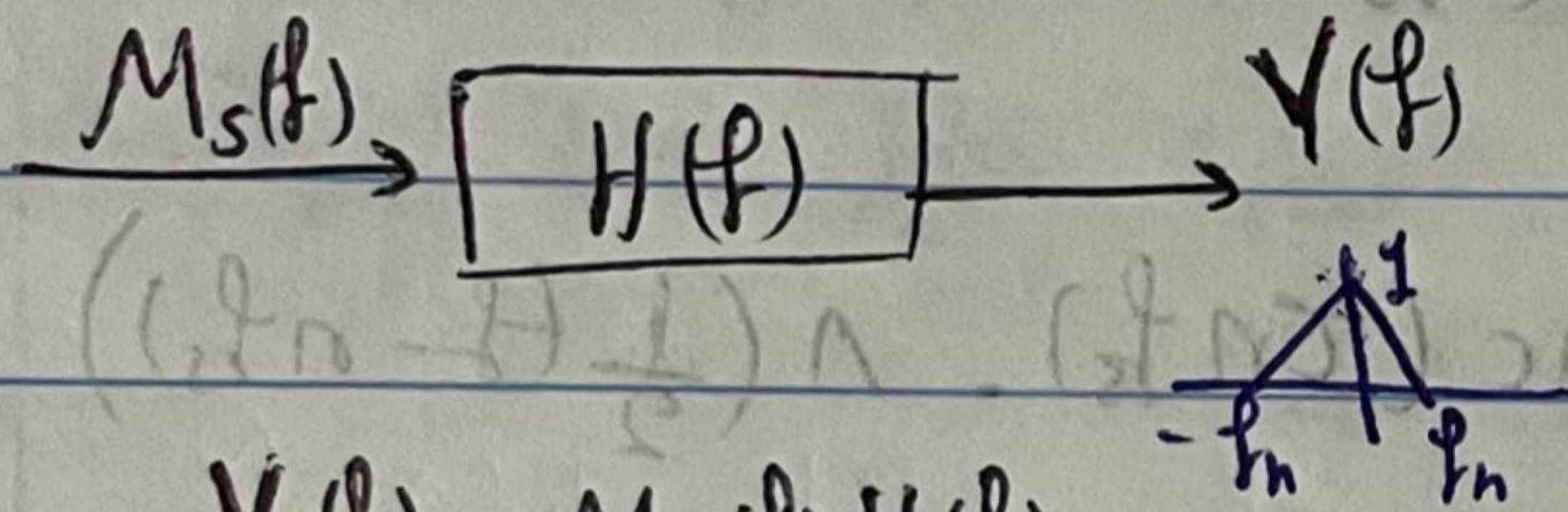
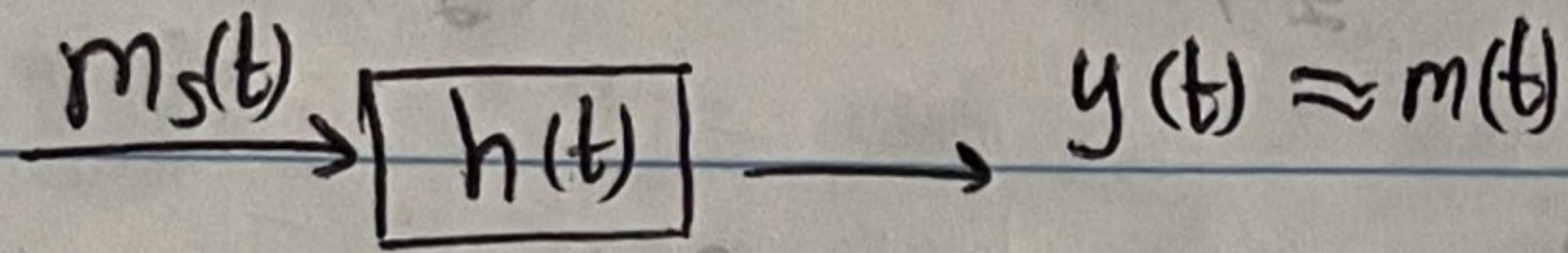


Data Reconstruction:-

To recover data:-
 $f_s - f_h \geq f_h \Rightarrow f_s \geq 2f_h$
 "Nyquist rate".



To recover message signal



و دائما تحققه هذا الشرط

$$H(f) \begin{cases} \frac{1}{P_0} & , |f| \leq f_s/2 \\ 0 & , o.w. \end{cases}$$

$$Y(f) = M_s(f) H(f)$$

$$1 = (P_0)(1) K \Rightarrow K = \frac{1}{P_0} \text{ gain}$$

In our example

$$H(f) \begin{cases} \frac{1}{2P_s} & , |f| \leq f_s/2 \\ 0 & , o.w \end{cases}$$

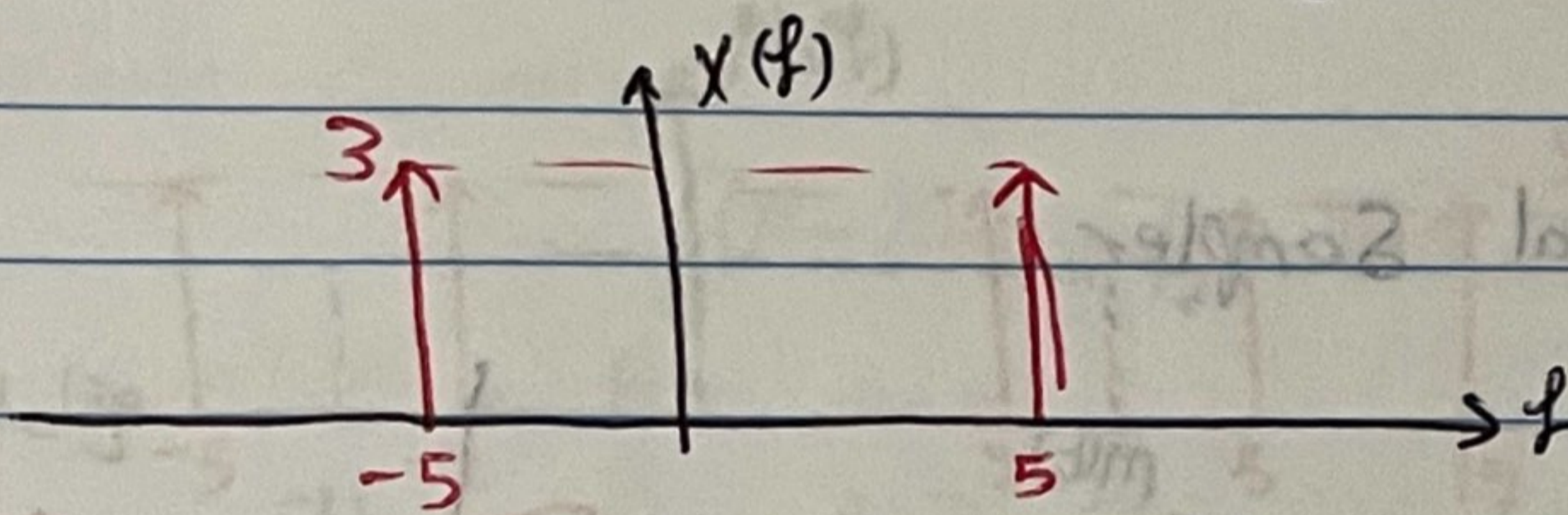
Example] The signal $X(t) = 6 \cos(10\pi t)$ ← Message Signal
← Sampling Signal.

Sampled at 7 Hz and 14 Hz, for each sampled frequency,

a- Plot the spectrum of $X(t)$

$$X(t) = 6 \cos(10\pi t)$$

$$\Rightarrow X(f) = 3 [\delta(f-5) + \delta(f+5)]$$



b- Evaluate and plot the spectrum of sampled signal.

$$M_s(f) = f_s \sum_{n=-\infty}^{\infty} P(nf_s) \delta(f - nf_s) \quad \text{[ideal sampler]}$$

$$f_s \sum_{n=-\infty}^{\infty} \delta(f - nf_s)$$

~~$$\Rightarrow M_s(f) = f_s \sum_{n=-\infty}^{\infty} [3\delta(f-5) + 3\delta(f+5)]$$~~

$$M_s(f) = f_s \sum_{n=-\infty}^{\infty} [3[\delta(f-5-nf_s) + \delta(f+5-nf_s)]]$$

at $f_s = 7$ Hz.

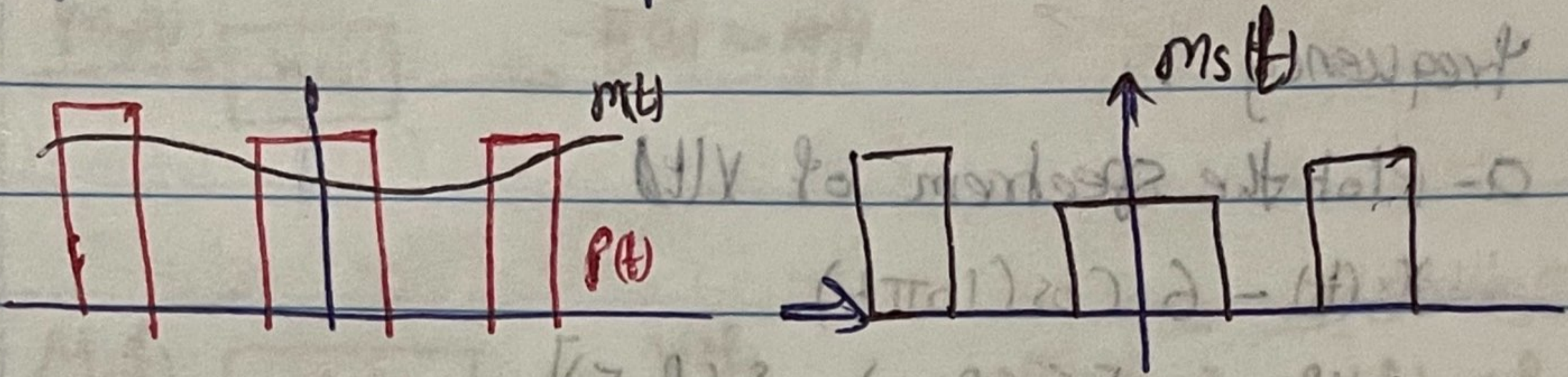
$$M_s(f) = 7 \sum_{n=-\infty}^{\infty} [3\delta(f-5-7n) + 3\delta(f+5-7n)]$$

we can not recover the message signal.

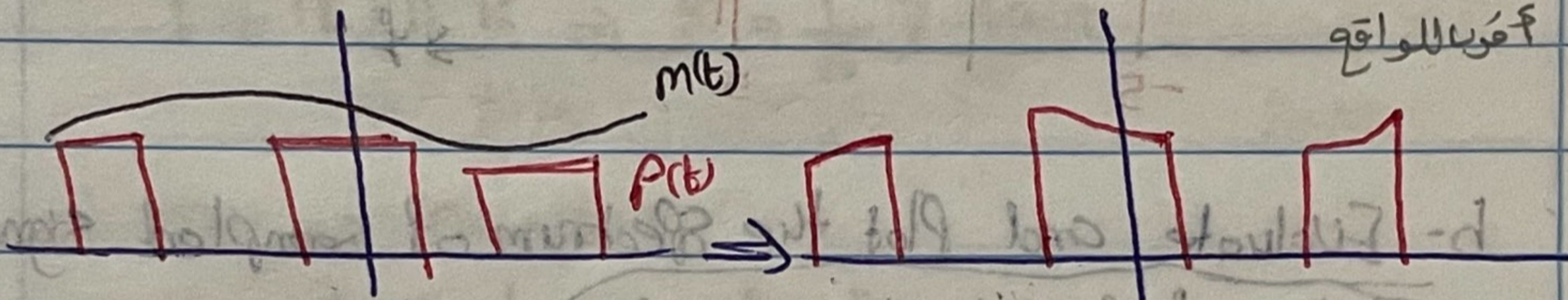
since $f_s < 2f_m$.

Types of Sampler:-

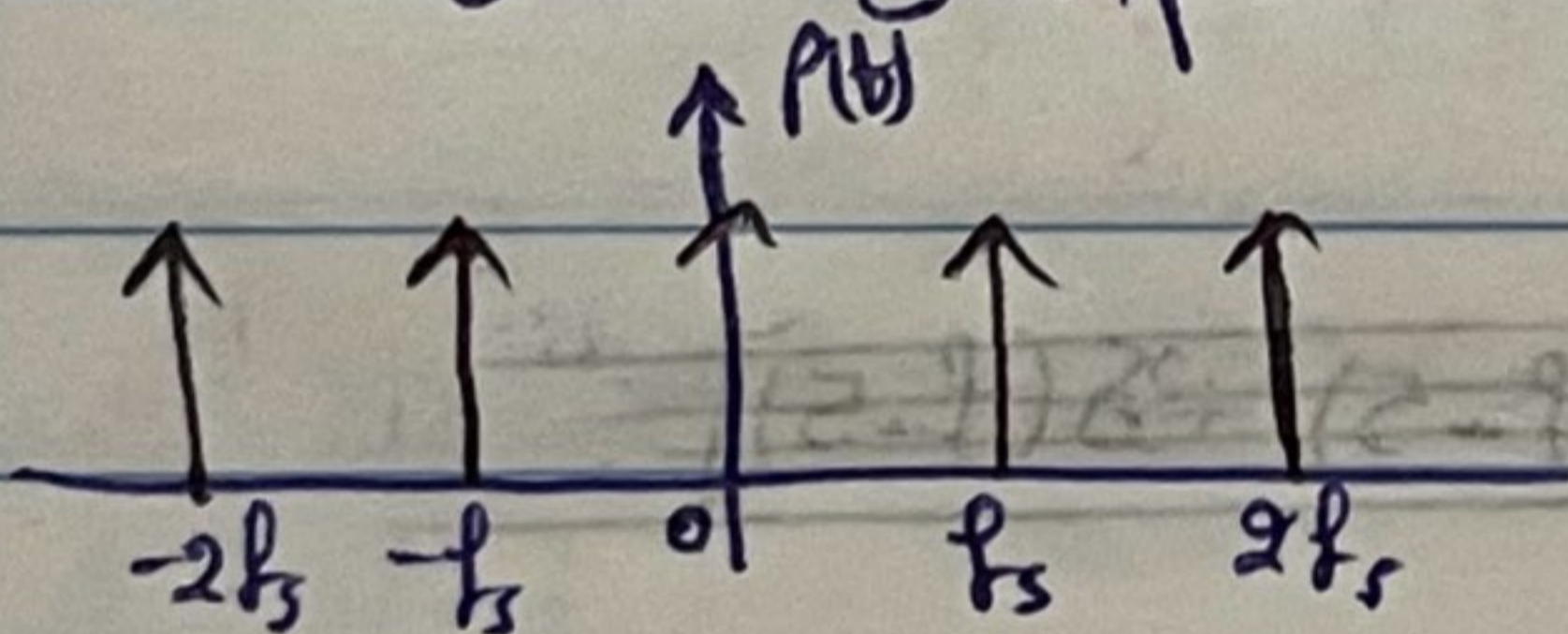
1. Flat Top Sampler



2. Natural Sampler



3. Ideal Sampler



$$P(\omega) = \sum_{n=-\infty}^{\infty} P_n e^{j2\pi n f_s t} ; P_n = \delta_s$$

For ideal sampler, the sampled signal.

$$M_s(f) = \delta_s \sum_{n=-\infty}^{\infty} M(f - n f_s)$$

when $M(f) = \Lambda\left(\frac{f}{2}\right)$

$$H(f) = \begin{cases} \frac{1}{f_s}, & |f| \leq f_s/2 \\ 0, & \text{o.w} \end{cases}$$

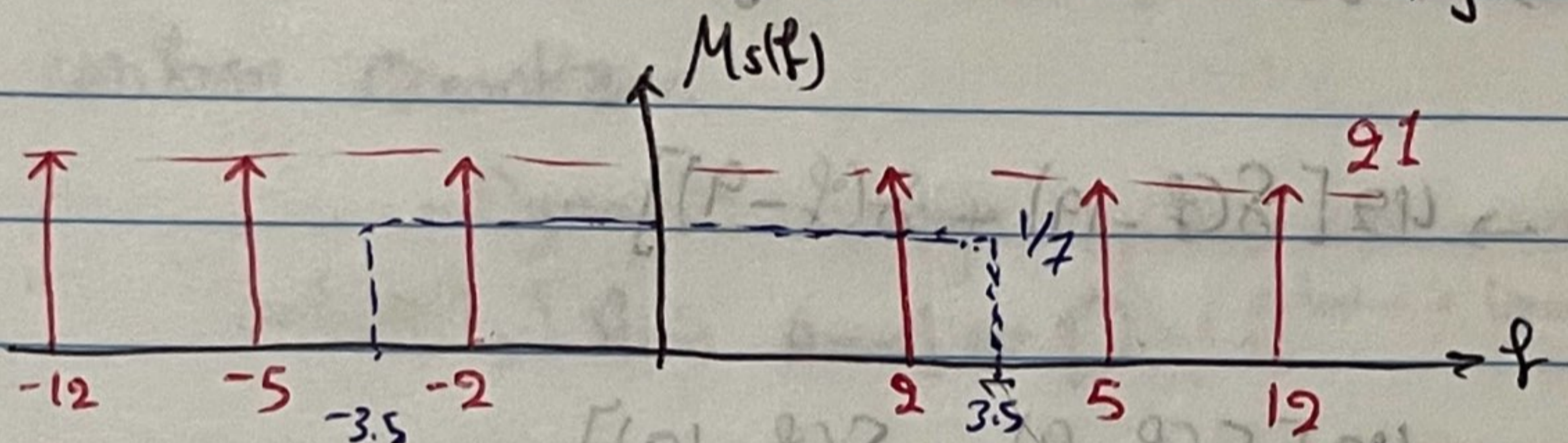
→

When

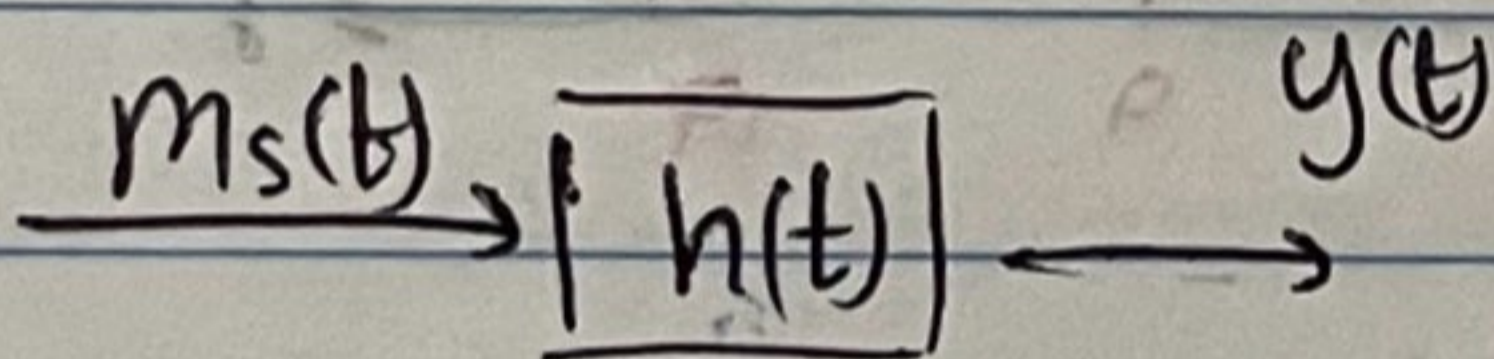
$$n=0 \rightarrow M_s(f) = 21[\delta(f-5) + \delta(f+5)]$$

$$n=1 \rightarrow M_s(f) = 21[\delta(f-12) + \delta(f+12)]$$

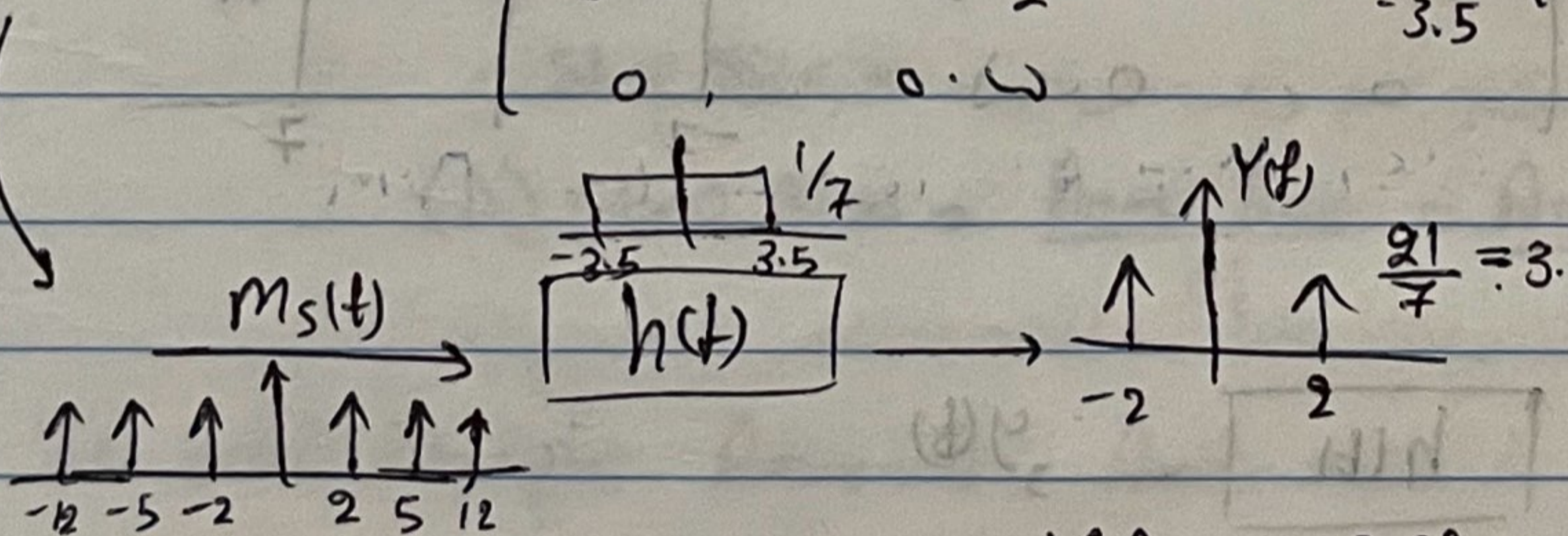
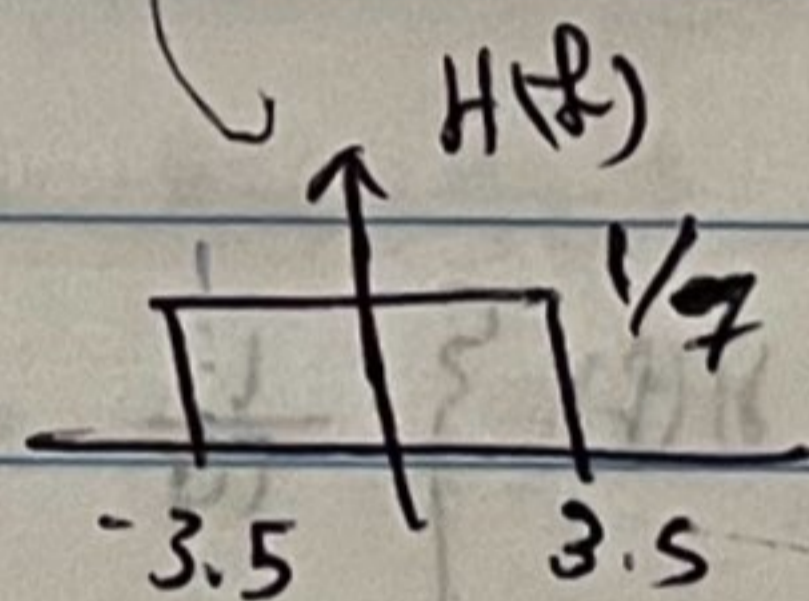
$$n=-1 \rightarrow M_s(f) = 21[\delta(f+2) + \delta(f+12)]$$



c) Plot the output of reconstruction filter.



$$H(f) = \begin{cases} \frac{1}{7}, & |f| \leq \frac{7}{2} \\ 0, & \text{o.w.} \end{cases}$$



$$Y(f) = 3\delta(f+2) + 3\delta(f-2)$$

$$y(t) = 6 \cos(2\pi t) = 6 \cos(10\pi t)$$

$$f_s < 2f_m$$

→

when $f_s = 14 \text{ Hz}$

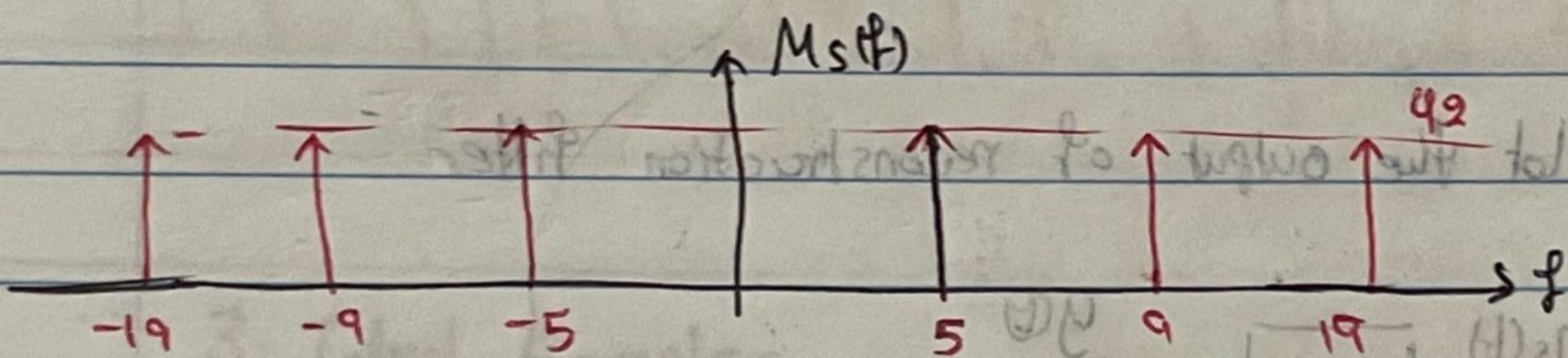
$$M_s(f) = 14 \sum_{n=-\infty}^{\infty} 3 [\delta(f - 5 - 14n) + \delta(f + 5 - 14n)]$$

when

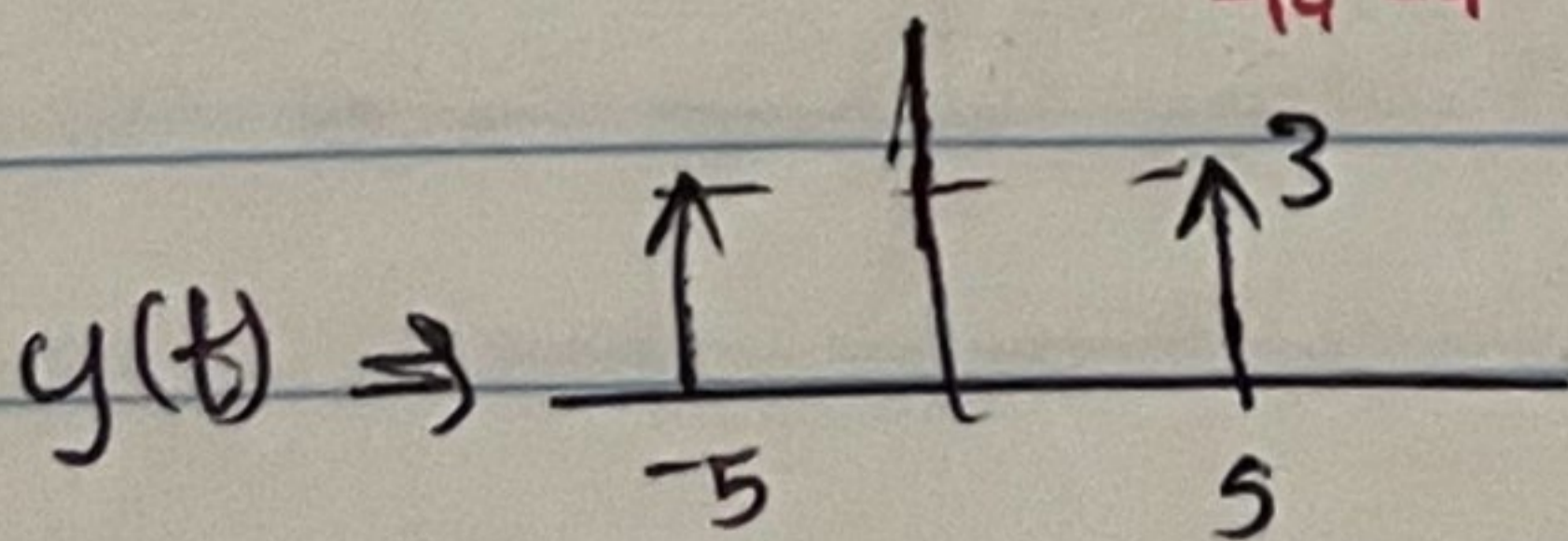
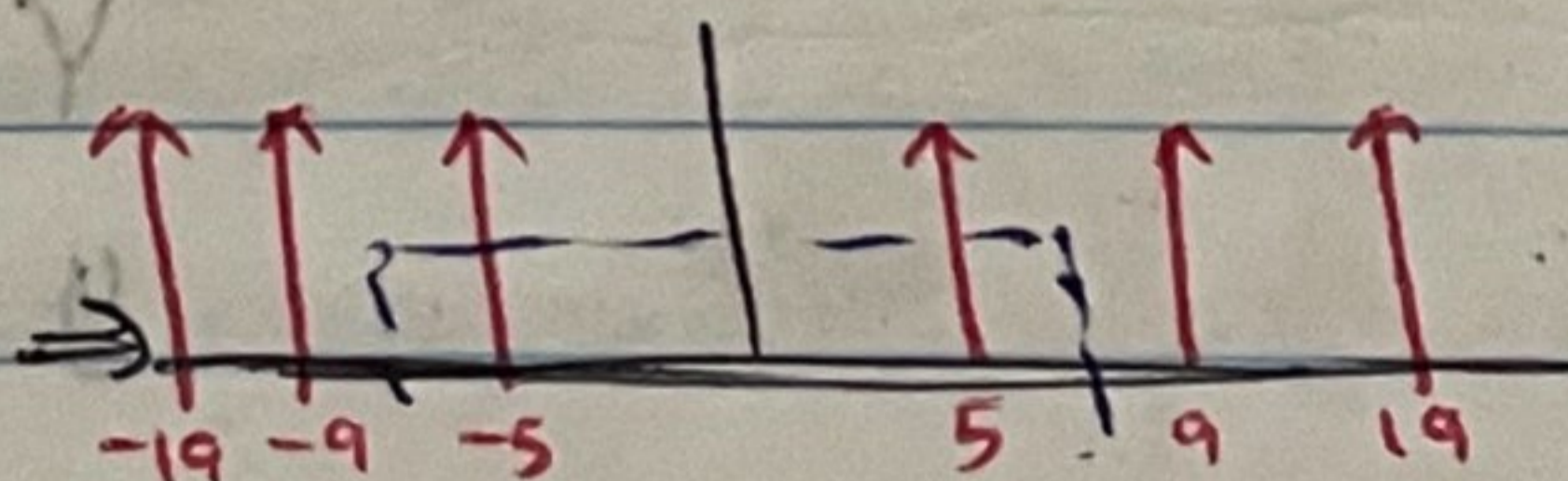
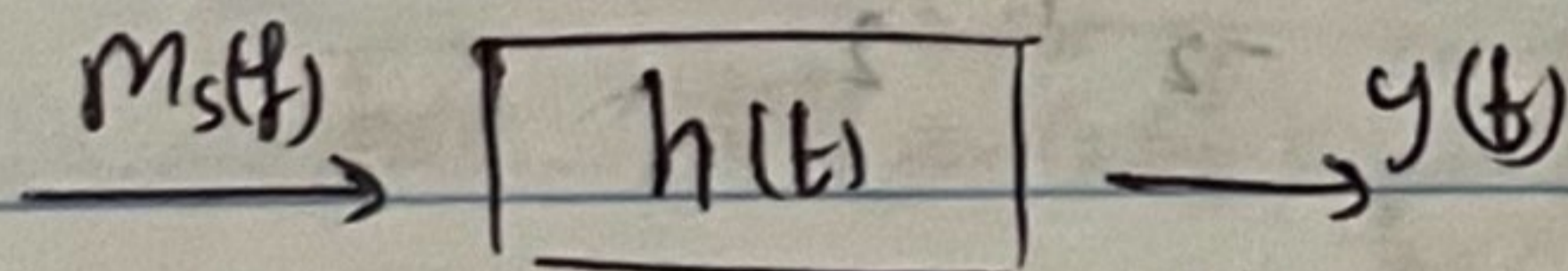
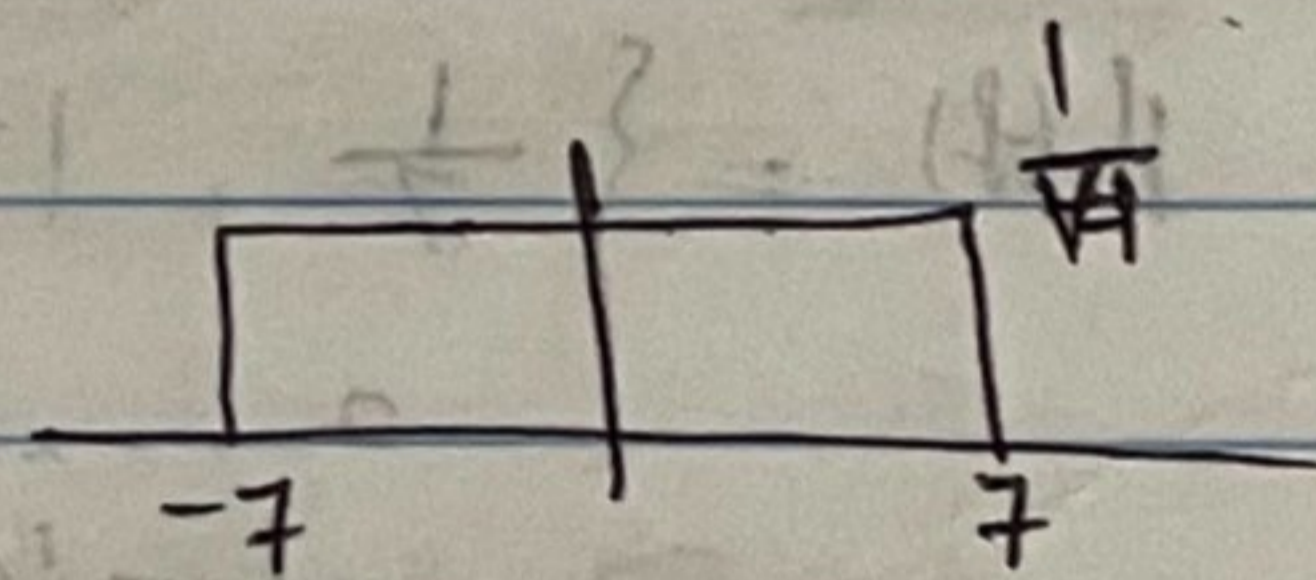
$$n=0 \rightarrow 42 [\delta(f-5) + \delta(f+5)]$$

$$n=1 \rightarrow 42 [\delta(f-19) + \delta(f-9)]$$

$$n=-1 \rightarrow 42 [\delta(f+9) + \delta(f+19)]$$



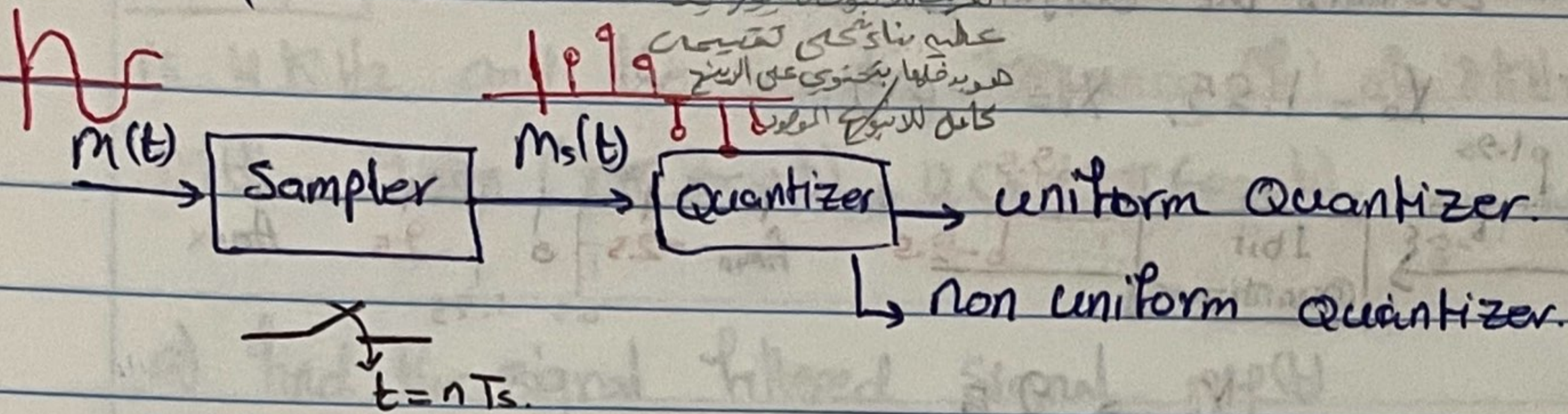
$$H(f) \begin{cases} \frac{1}{14}, & |f| \leq \frac{14}{2} \\ 0, & \text{o.w.} \end{cases}$$



$$y(t) = 3 \cos(10\pi t)$$

(L16)

≡ Quantizer.

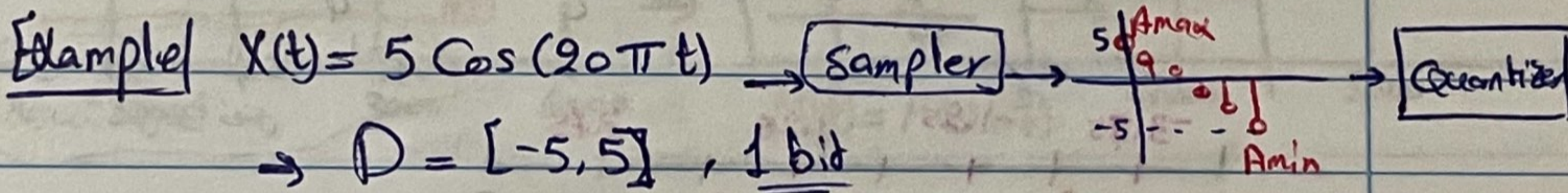


• uniform Quantizer.

- Dynamic range

هو المدى الى نصل عليه حتى نقتسم
المدى لعدد مستويات

$$\rightarrow [A_{min}, A_{max}] \equiv D$$



- M Levels = 2^n if Quantizer 1 bit

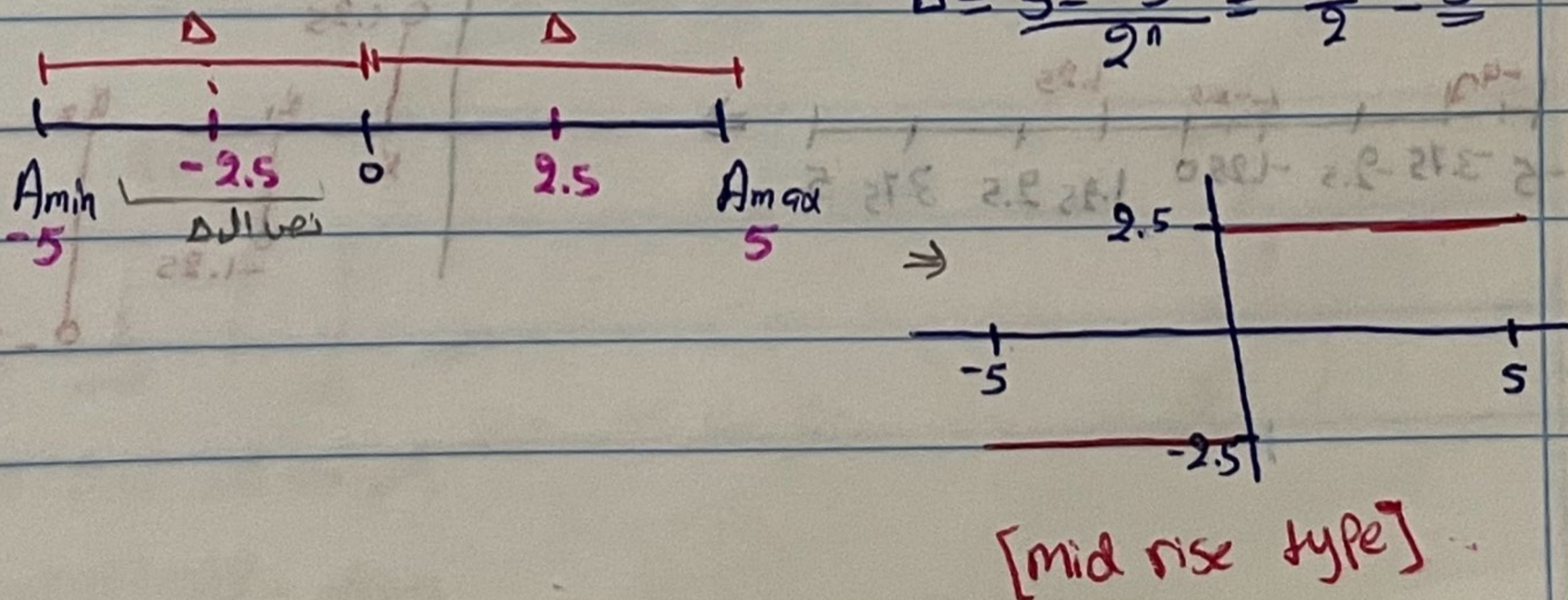
$$\Rightarrow M \text{ Levels} = 2$$

- Step size. M يا حساب على حسب M

$$(\Delta) \text{ Step size} = \frac{A_{max} - A_{min}}{M} = \frac{A_{max} - A_{min}}{2^n}$$

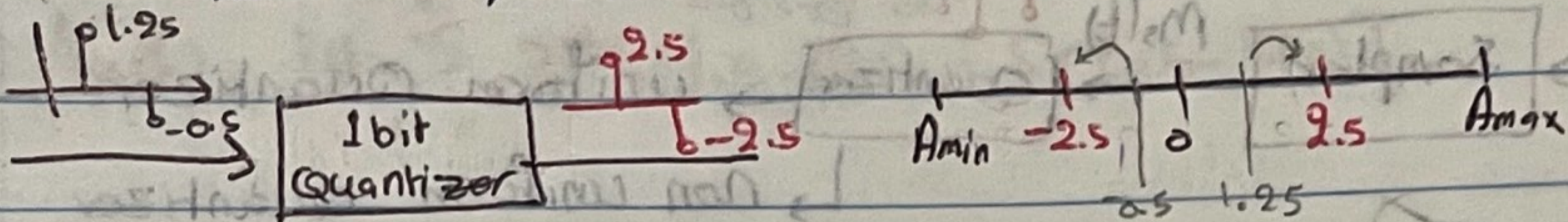
In our example $A_{max} = 5, A_{min} = -5$.

$$\Delta = \frac{5 - (-5)}{2^n} = \frac{10}{2} = 5$$



Evaluate the output of quantizer for input value

$x_0 = 1.25, x_1 = -0.5$



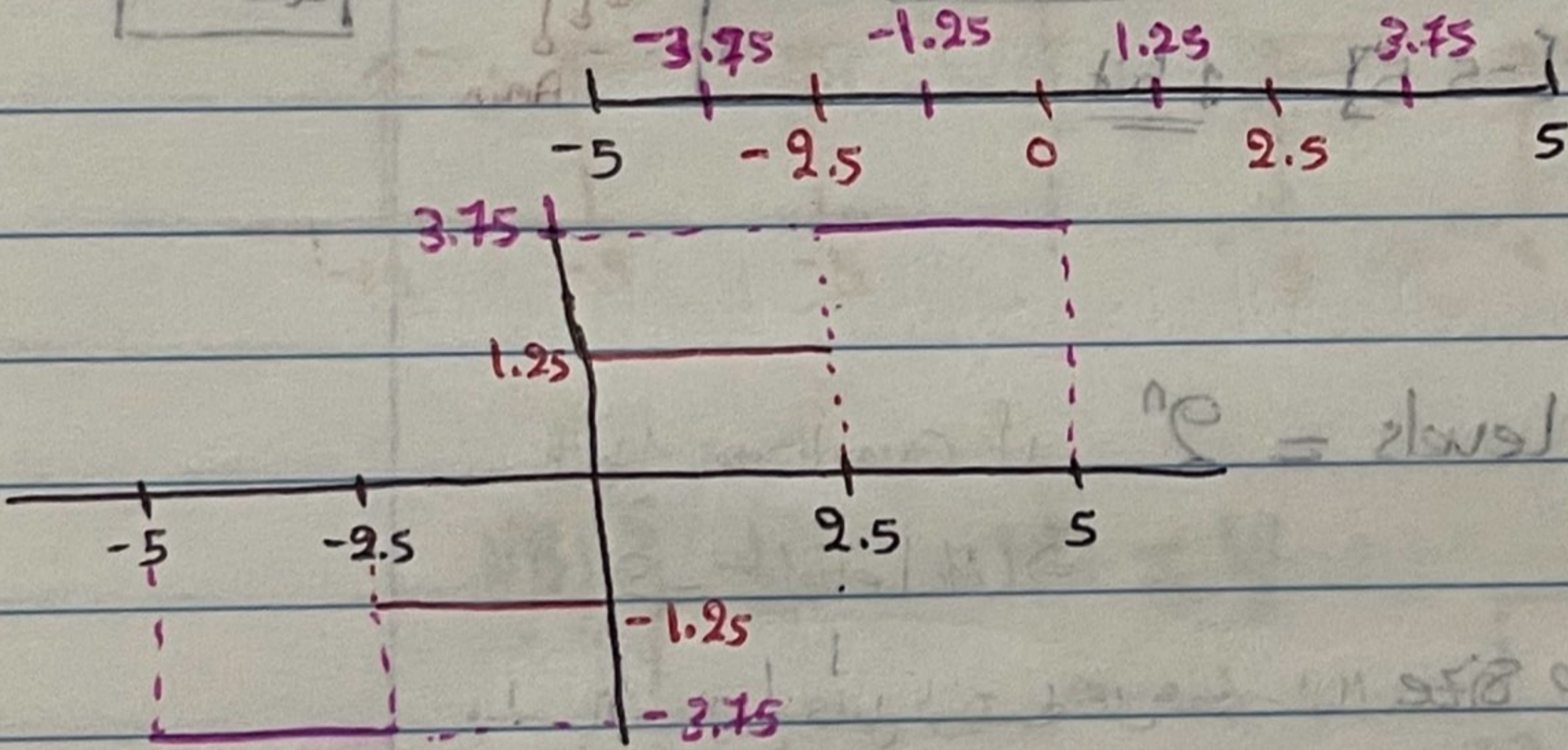
$x_0 \rightarrow 2.5$

$x_1 \rightarrow -2.5$

if we have 9bit quantizer

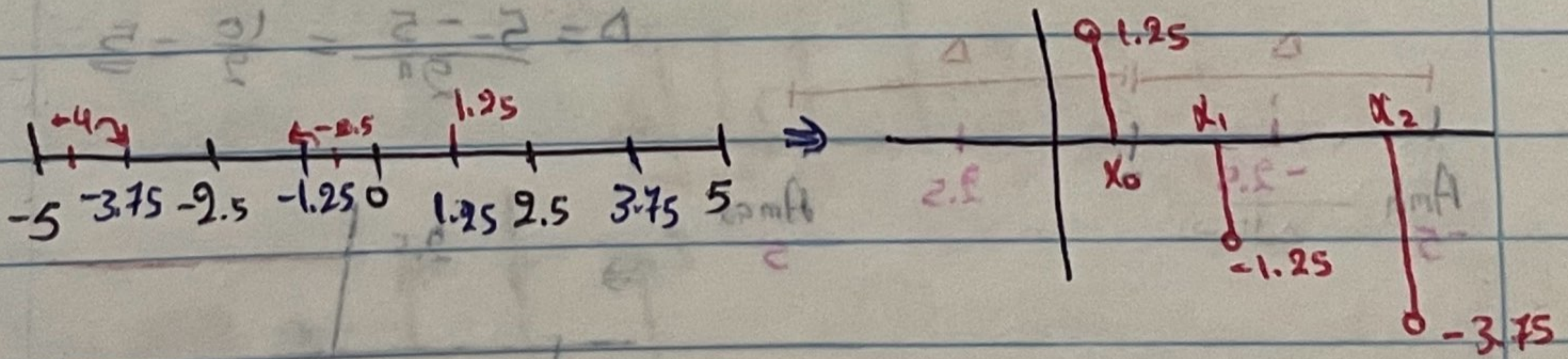
$M = 2^9 = 4 \text{ levels}$

Since $P = [-5, 5] \Rightarrow \Delta = \frac{5 - (-5)}{4} = \frac{10}{4} = 2.5$



Evaluate the output of quantizer for input value

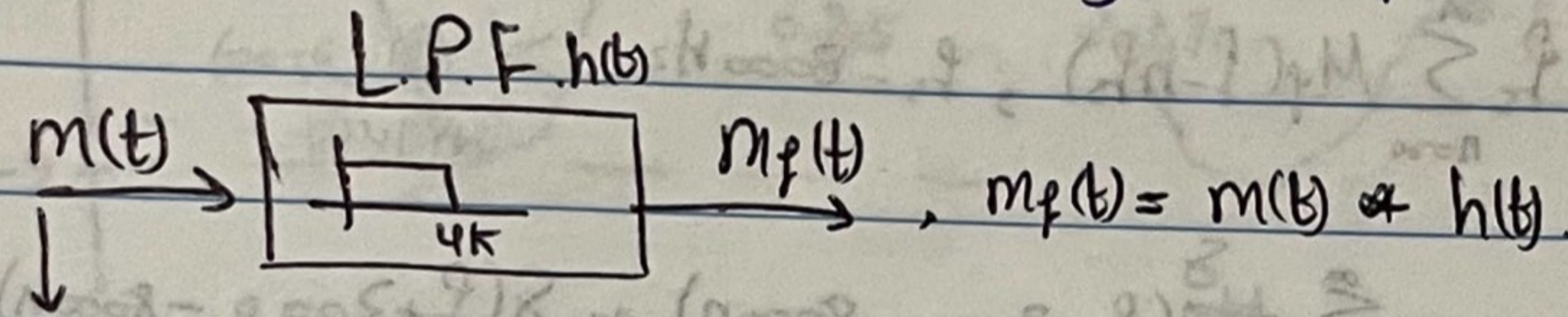
$x_0 = 1.25, x_1 = -0.5, x_2 = -4$



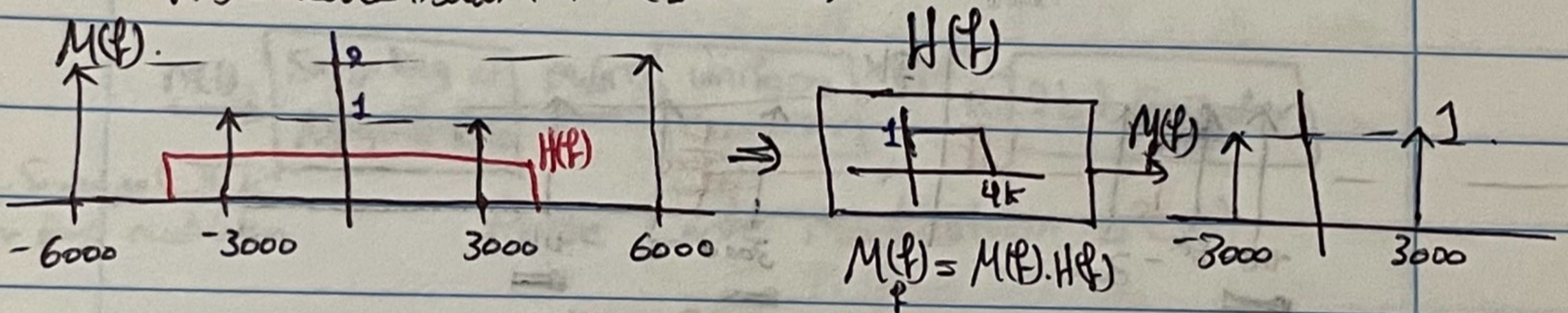
Example Passband bandwidth of the low pass filter is 4 kHz and the sampling frequency (f_s) of 8 kHz.

$$m(t) = 2 \cos(2\pi 3000t) + 4 \cos(2\pi 6000t)$$

a) Find the signal filtered signal $m_f(t)$.



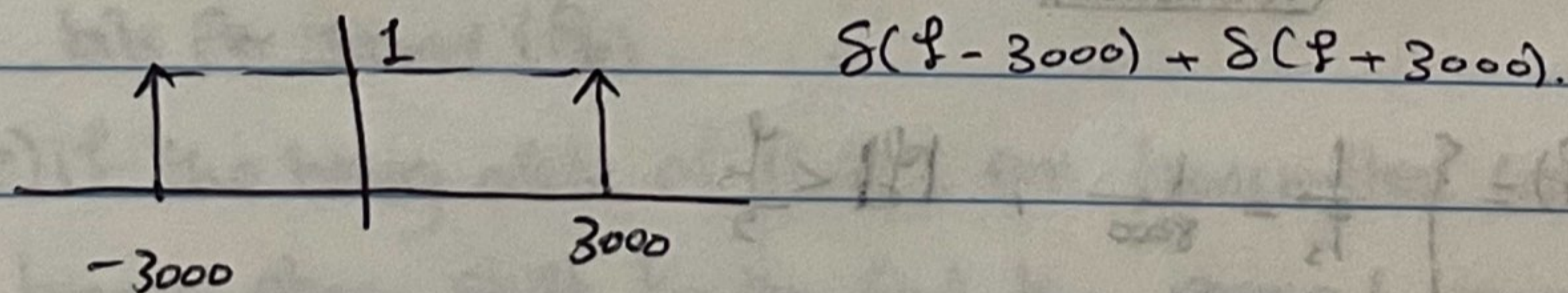
$$m(t) = 2 \cos(2\pi 3000t) + 4 \cos(2\pi 6000t)$$



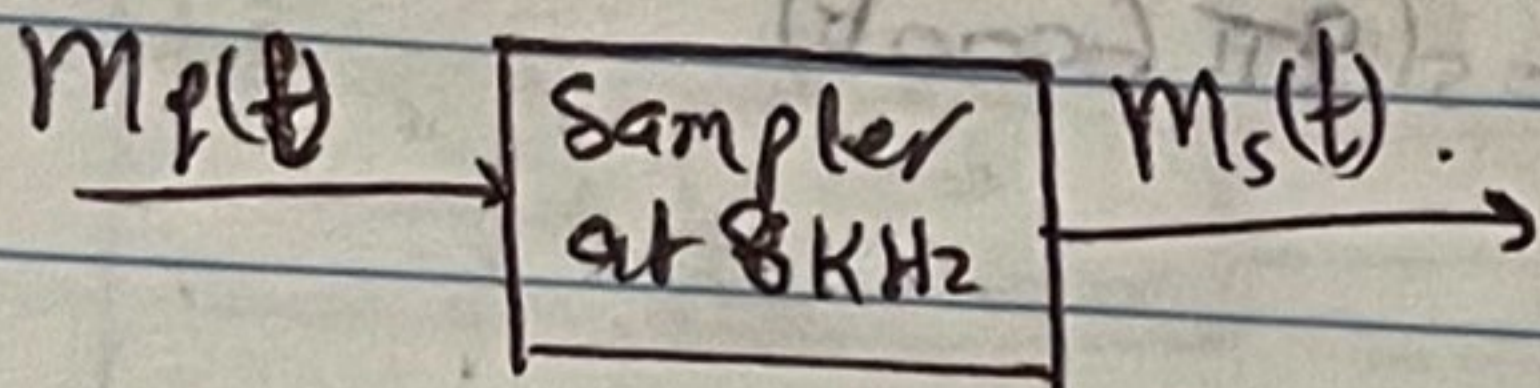
$$M_f(f) = \delta(f - 3000) + \delta(f + 3000)$$

$$m_f(t) = 2 \cos(2\pi (3000)t)$$

b) Plot the amplitude spectrum of the filtered signal $m_f(t)$.

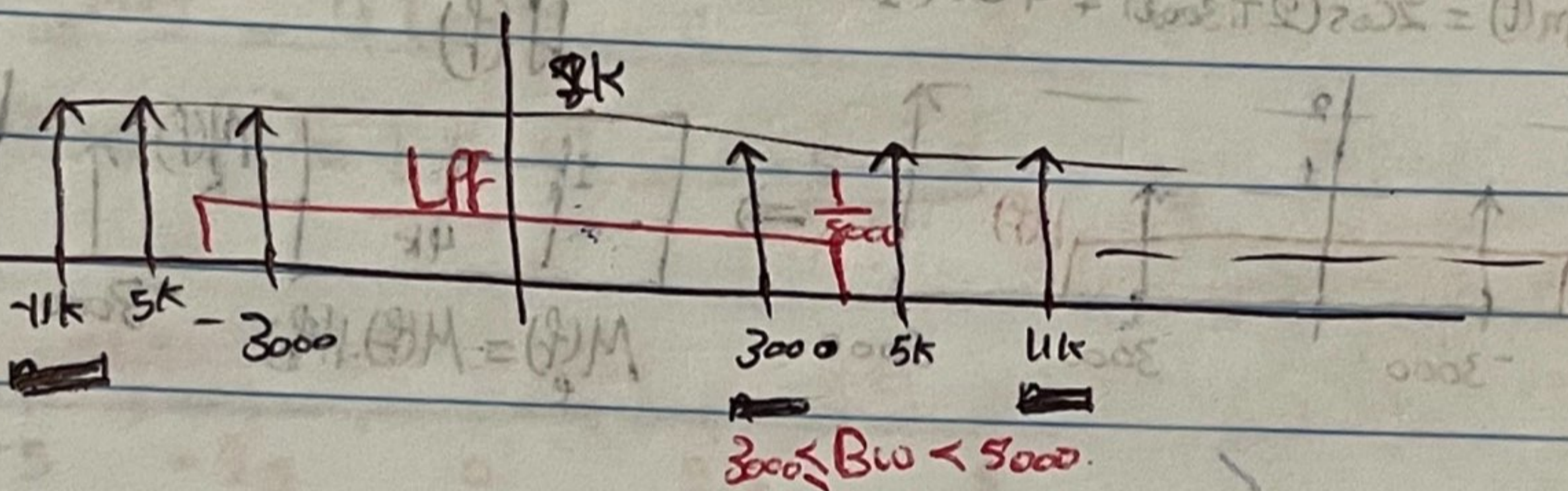


c) Plot the amplitude spectrum of the sampled signal $M_s(f)$.

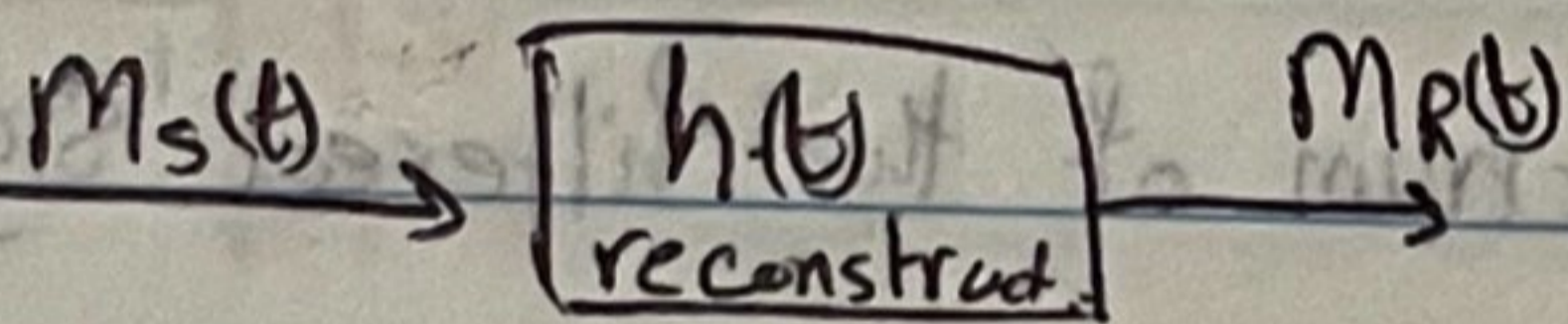


$$M_s(f) = \frac{1}{f_s} \sum_{n=-\infty}^{\infty} M_f(f - n f_s); \quad f_s = 8000 \text{ Hz}$$

$$M_s(f) = 8000 \sum_{n=-\infty}^{\infty} \delta(f - 3000 - 8000n) + \delta(f + 3000 - 8000n)$$

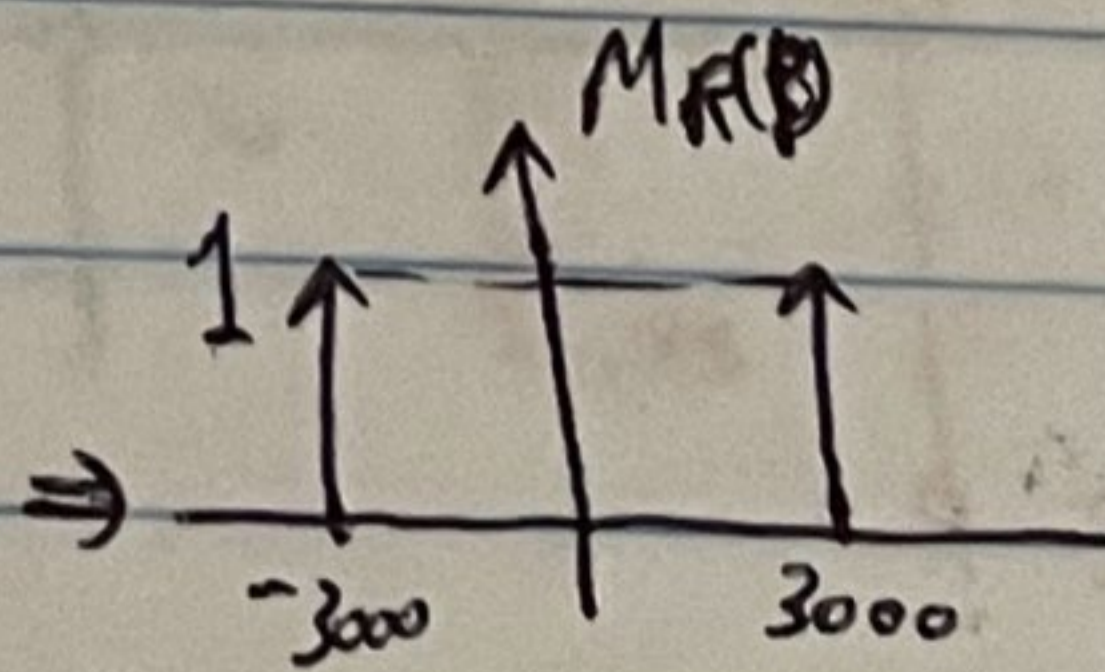


d) what is the type of the reconstruction filter at the receiver?



$$H(f) = \begin{cases} \frac{1}{f_s} = \frac{1}{8000}, & |f| < \frac{f_s}{2} \\ 0, & \text{o.w} \end{cases}$$

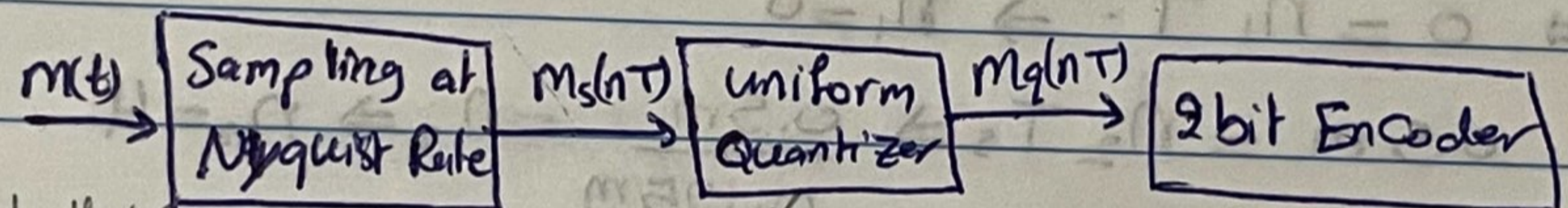
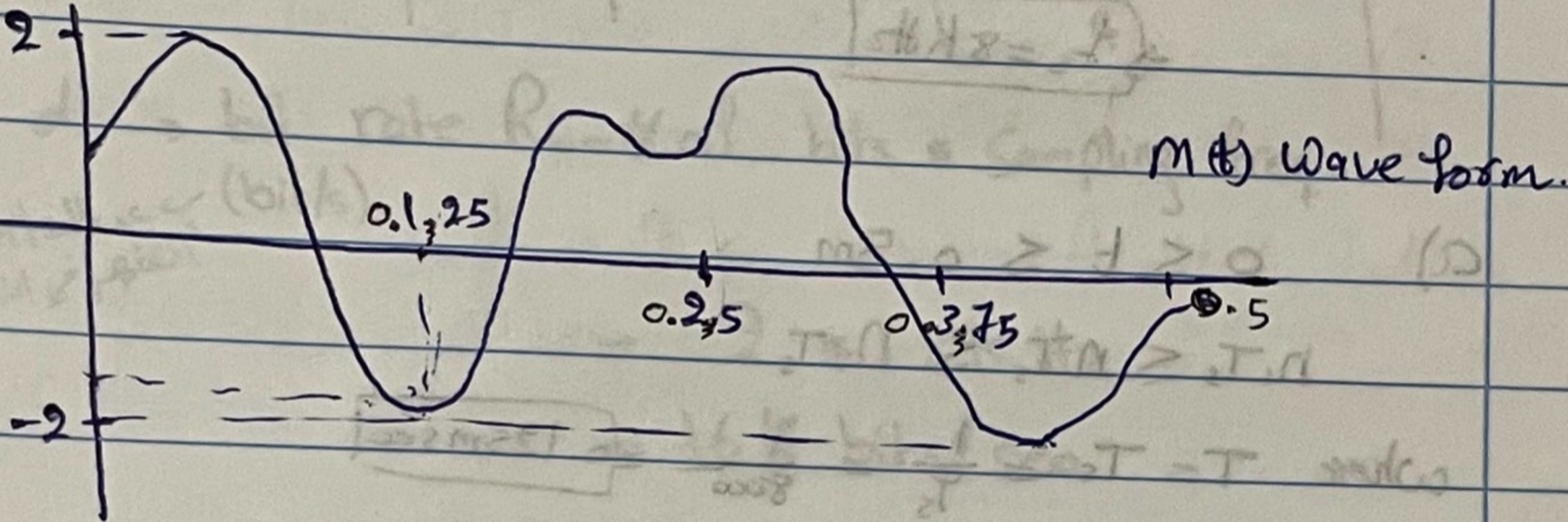
$$= \begin{cases} \frac{1}{8000}, & |f| < 4000 \\ 0, & \text{o.w} \end{cases}$$



$$M_R(f) = \delta(f - 3000) + \delta(f + 3000)$$

$$m_R(t) = 2 \cos(2\pi 3000 t)$$

Example ~~the~~ maximum freq. Component at 4KHz. The dynamic range of the uniform quantizer is from -2 to 2 Volts.



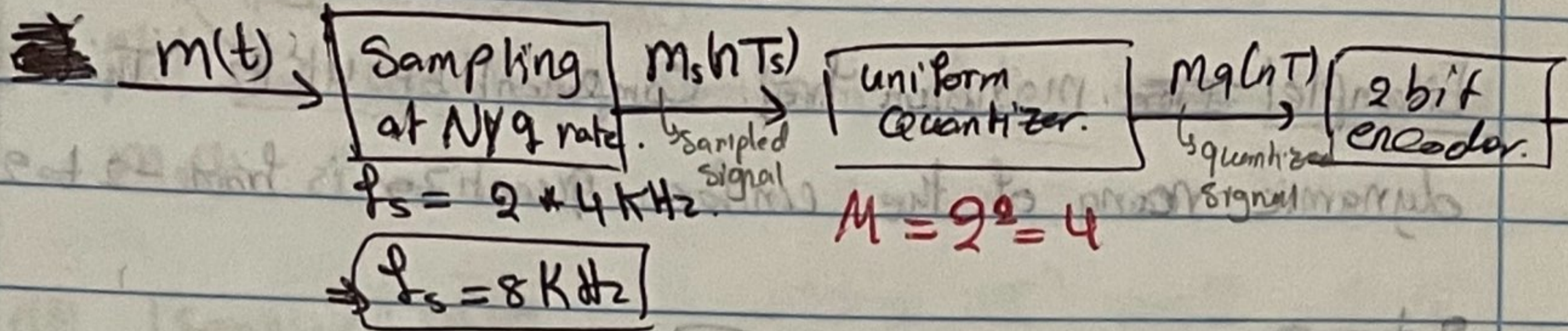
Pulse Code modulation (PCM).

- a- Determine the sampled signal value, $m_s(nT)$ for $0.5 \leq t \leq 0.5 \text{ ms}$
- b- Determine the quantizer signal value $m_q(nT)$ for $0.5 \leq t \leq 0.5 \text{ ms}$.
- c- Determine the binary signal value at the output of the 2 bit encoder for the quantized samples of part b (mb).
- d) Determine the output bit rate at the quantizer output in bits per second (R_b)
- e) if the binary data of part c are transmitted using binary phase shift Keying. find the required transmission band width.

(L7)

$0 \leq t \leq 0.5$

M level = 2^n bit encoder
Quant



a) $0 \leq t \leq 0.5m$

$n_1 T_s \leq n T_s \leq n_2 T_s$

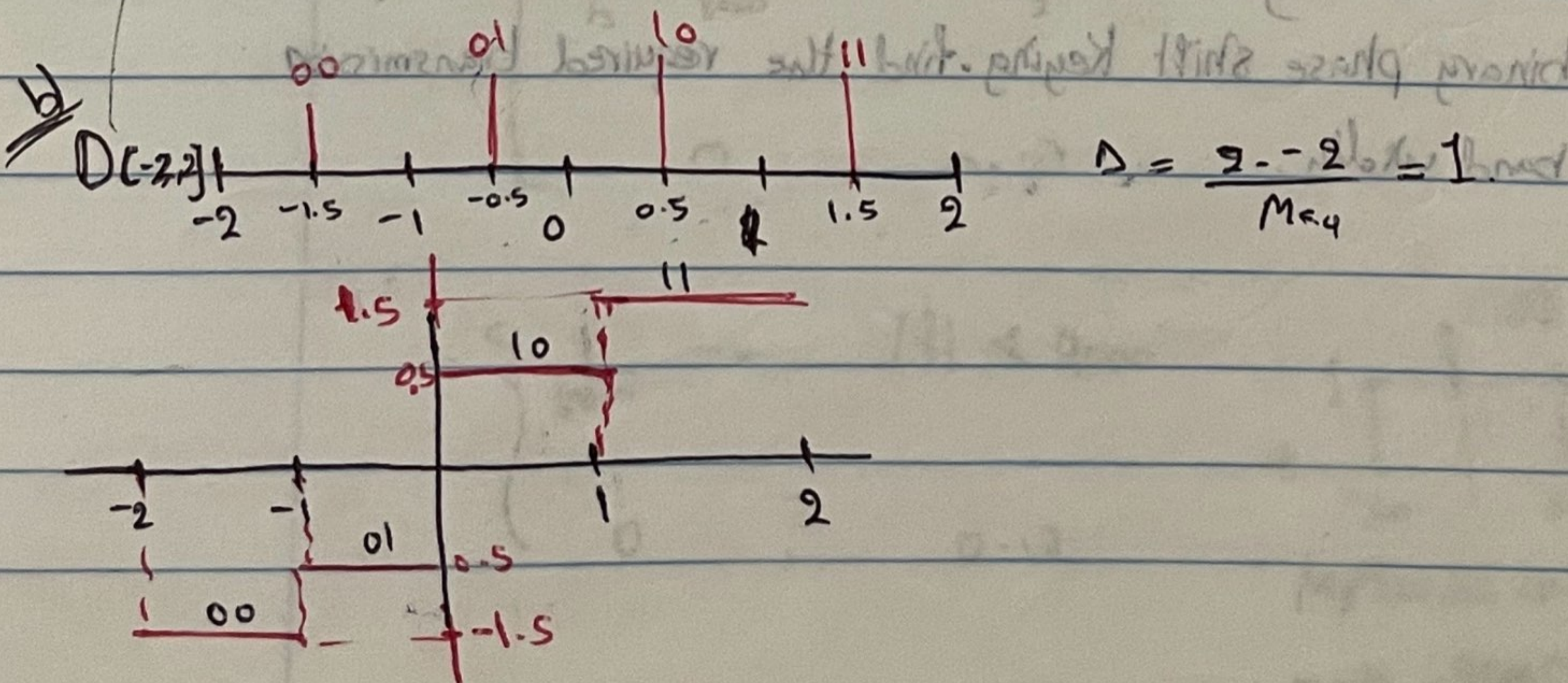
where $T_s = \frac{1}{f_s} = \frac{1}{8000} = 0.125msec$

$0 = n_1 T_s \Rightarrow n_1 = 0$

$0.5m = n_2 T_s \Rightarrow \frac{0.5m}{0.125m} = n_2 \Rightarrow n_2 = 4$

$\Rightarrow 0 \leq n T_s \leq 4$

$n T$	0	0.125	0.25	0.375	0.5
$m_s(nT)$	1.25	-1.45	0.9	-0.45	-0.2
$m_q(nT)$	1.5	-1.5	0.5	-0.5	-0.5



هيكله الجيول.

c) Binary	1.5	-1.5	0.5	-0.5	-0.5
	11	00	10	01	01

d) \rightarrow bit rate $R_b = \# \text{ of bits} * \text{Sampling freq.}$

(bit/s).

عدد البتات في كل عينة
الكلوم في الثانية

$$= 2 * 8 \text{ KHz}$$

$$= 16 \text{ K bits/sec}$$

F_s [Sampler/sec]

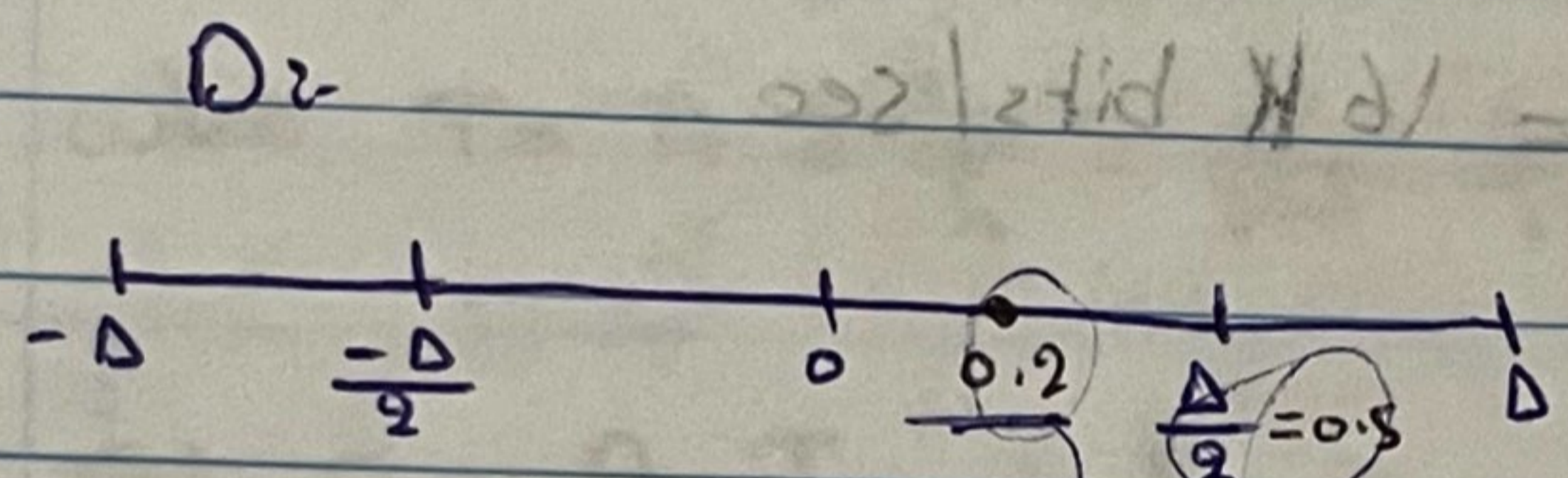
علاقة output الى موجود عنده
بالنسبة للاشارة الى مستويها

≡ SQNR: Signal quantization noise ratio.

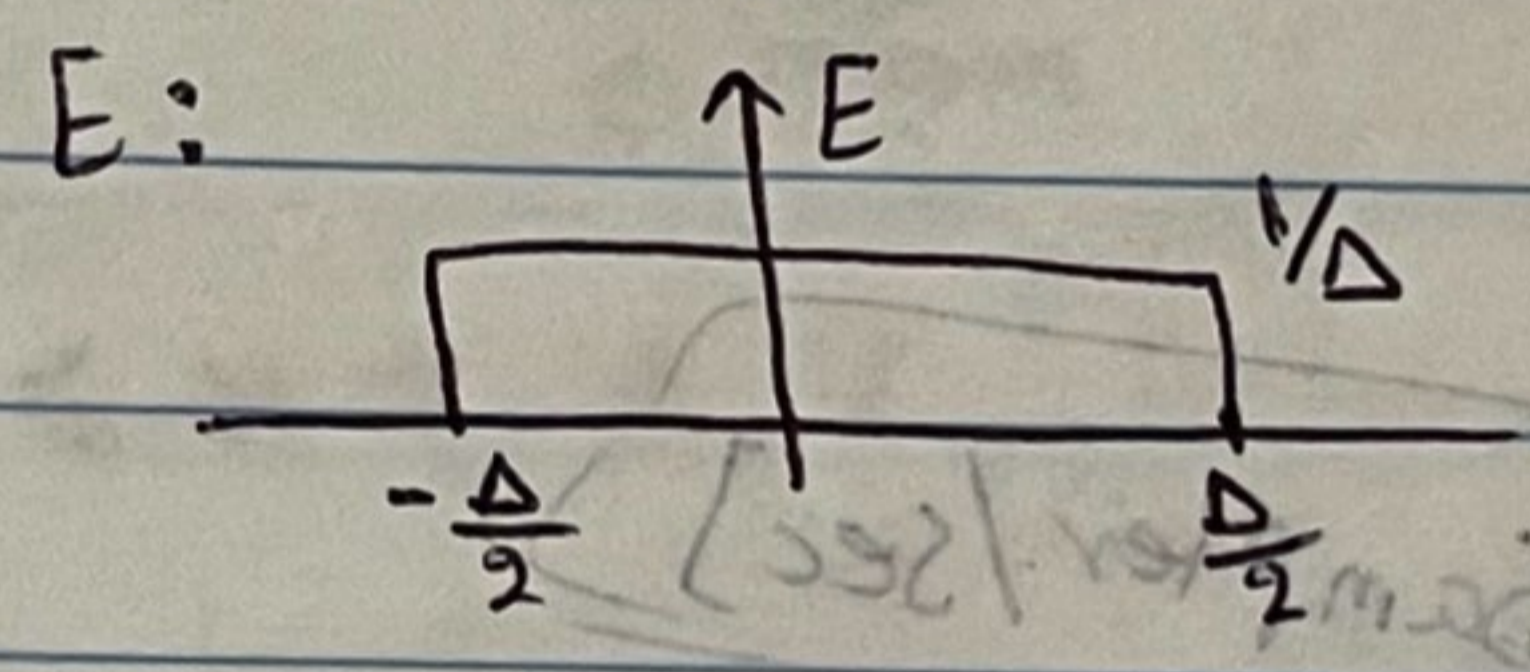
$$SQNR = \frac{P_s}{D} \rightarrow \text{Power. Rx}$$

$D \rightarrow \text{noise}$

Let $X(t) = A \cos(\omega t) \Rightarrow P_s = \frac{A^2}{2}$ (attid)



$$E = X_n - \frac{N}{2} \text{ eg. } \rightarrow E = 0.2 - 0.5 = -0.3$$



$$\Rightarrow D = \frac{\Delta^2}{12} = \frac{(2A)^2}{L=2^n} / 12$$

• $SQNR = \frac{A^2/2}{\Delta^2/12}$

∴ $SQNR = \frac{3}{2} L^2 \rightarrow \frac{3}{2} 2^{2n}$

In dB, $SQNR = 10 \log \frac{P_s}{D} = 6.02n + 1.76$

Example | $X(t) = 4 \cos(2\pi f_0 t)$ is applied to a uniform quantizer with L quantizer levels, and dynamic range $(-4, 4)$ V, find the minimum value of L that will achieve a signal to quantization noise ratio $SQNR_{dB} \geq 30$ dB.

$$SQNR_{dB} = 10 \log SQNR \Rightarrow SQNR = 10^{SQNR_{dB}/10}$$

$$30_{dB} = 10 \log SQNR \Rightarrow \boxed{SQNR = 1000}$$

$$SQNR = 1000 = \frac{P_s}{D} = \frac{A^2/2}{D^2/12} = \frac{8}{\frac{(8/L)^2}{12}}$$

$$SQNR = \frac{8 \cdot 12 \cdot L^2}{64} \Rightarrow \frac{12}{8} L^2 \geq 1000$$

$$\Rightarrow L^2 \geq \frac{8000}{12} \Rightarrow L \geq 25.8$$

$$L = 26 \text{ Levels.}$$

OR

$$6.02n + 1.76 \geq 30 \text{ dB}$$

$$\frac{30 - 1.76}{6.02} = \frac{6.02n}{6.02} \quad L = 2^n \text{ حيث } n \text{ عدد صحيح}$$

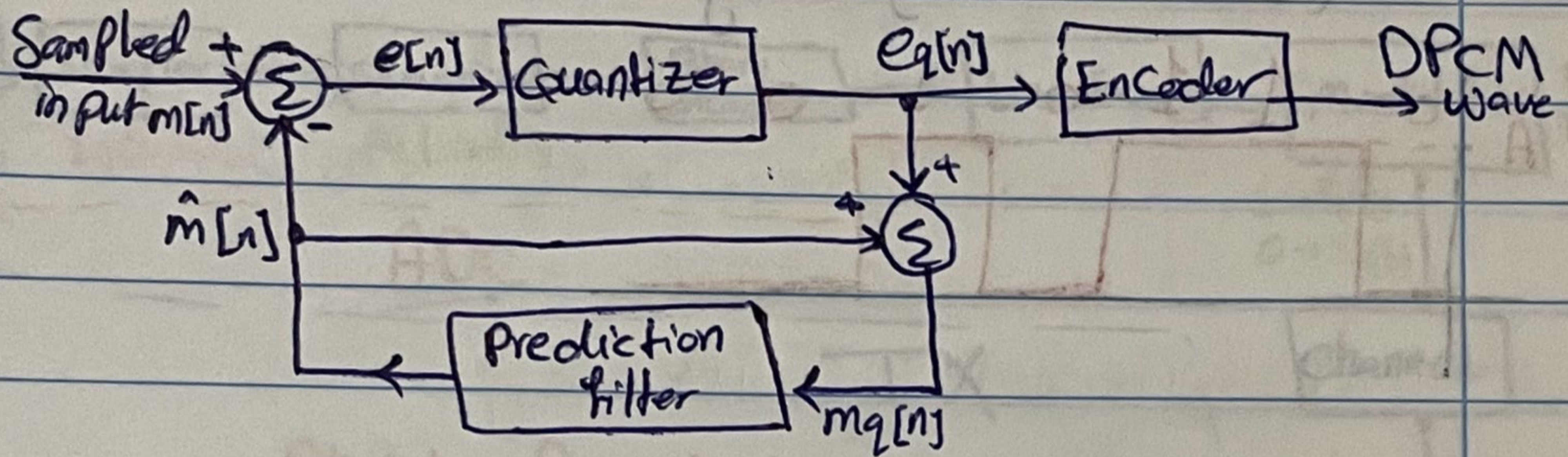
$$n = 4.69 \Rightarrow L = 2^n = 25.89$$

$$\Rightarrow \underline{\underline{L \approx 26 \text{ Level}}}$$

L(18)

25 min

Differential Pulse Code Modulation (DPCM)



Linear Prediction filter.

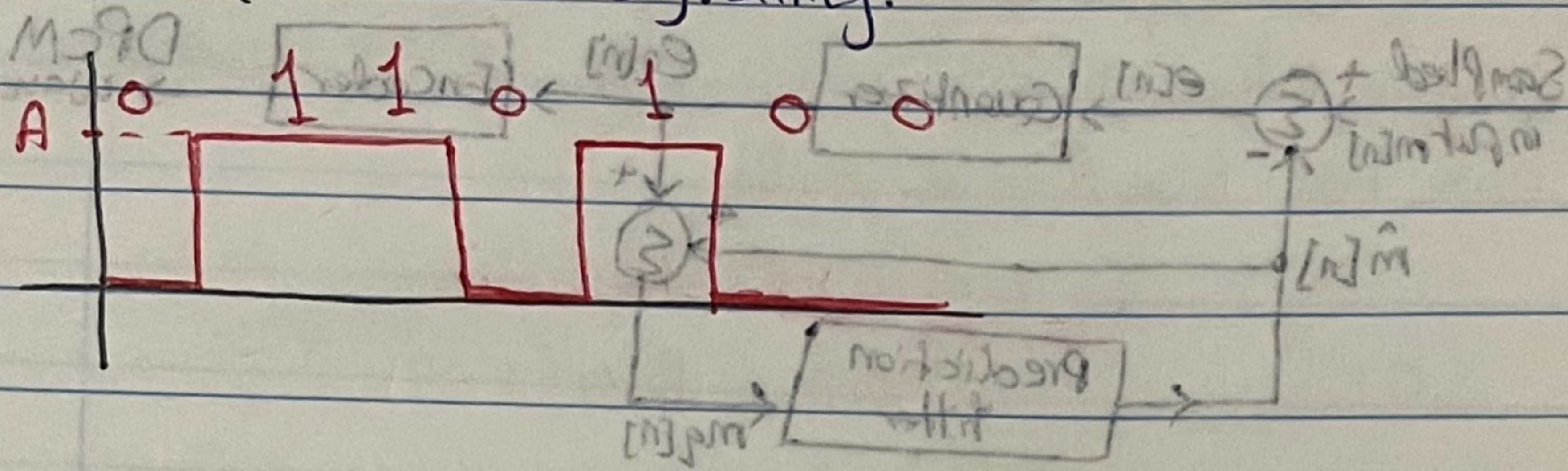
$$\hat{x}(n) = w_1 x(n-1) + w_2 x(n-2) + \dots + w_p x(n-p)$$

$$\epsilon = E(x(n) - \hat{x}(n))^2 \quad \text{Prediction error.}$$

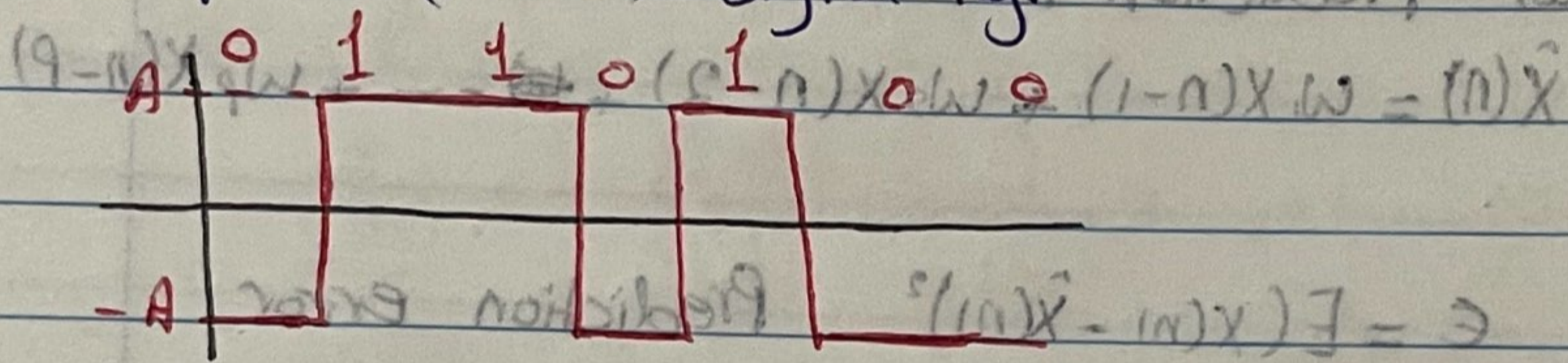
To avoid slope overload.

$$\frac{\Delta}{T_s} \geq \max \left| \frac{dm(t)}{dt} \right|$$

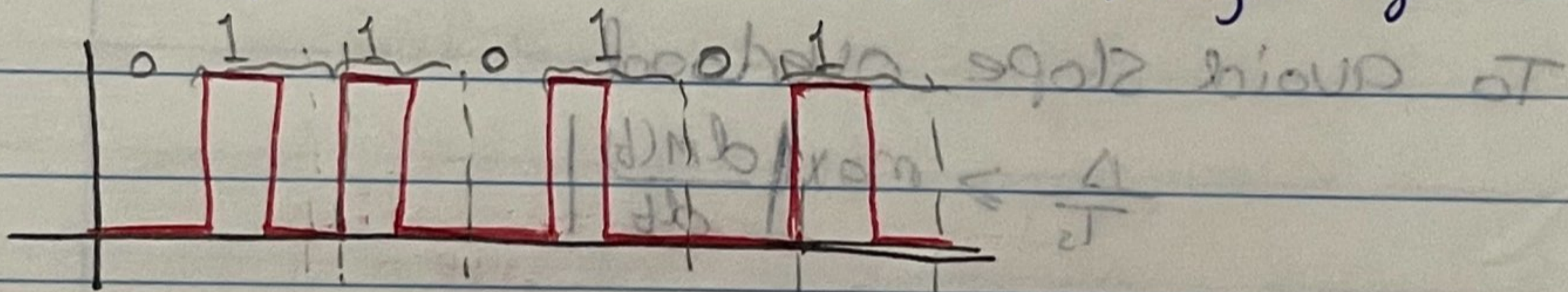
• Unipolar nonreturn-to-zero (NRZ) (on-off) signaling.



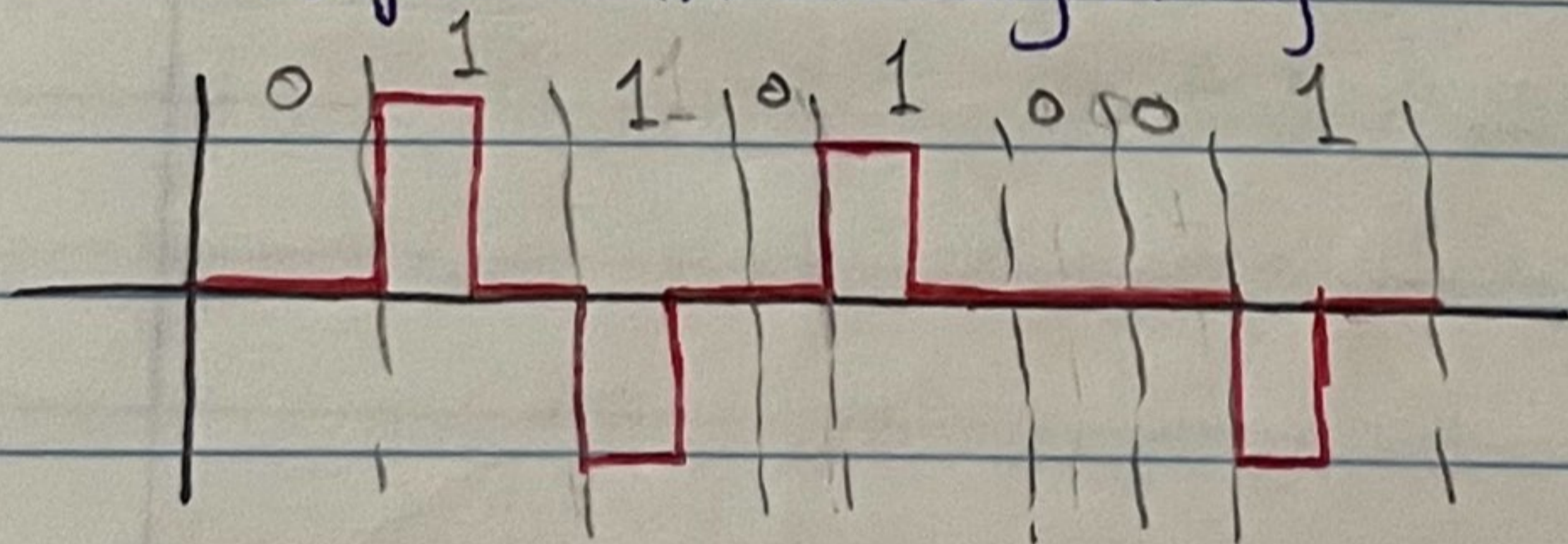
• Polar (NRZ) signaling.



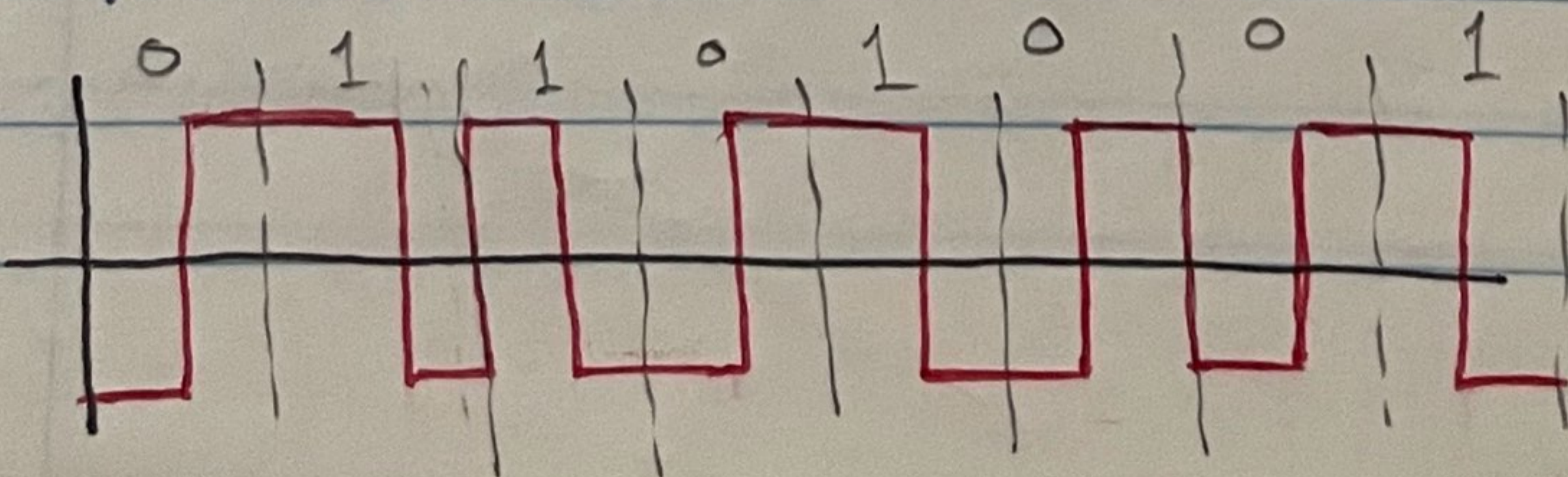
• unipolar return-to-zero (RZ) signaling.



• Bipolar (RZ) signaling

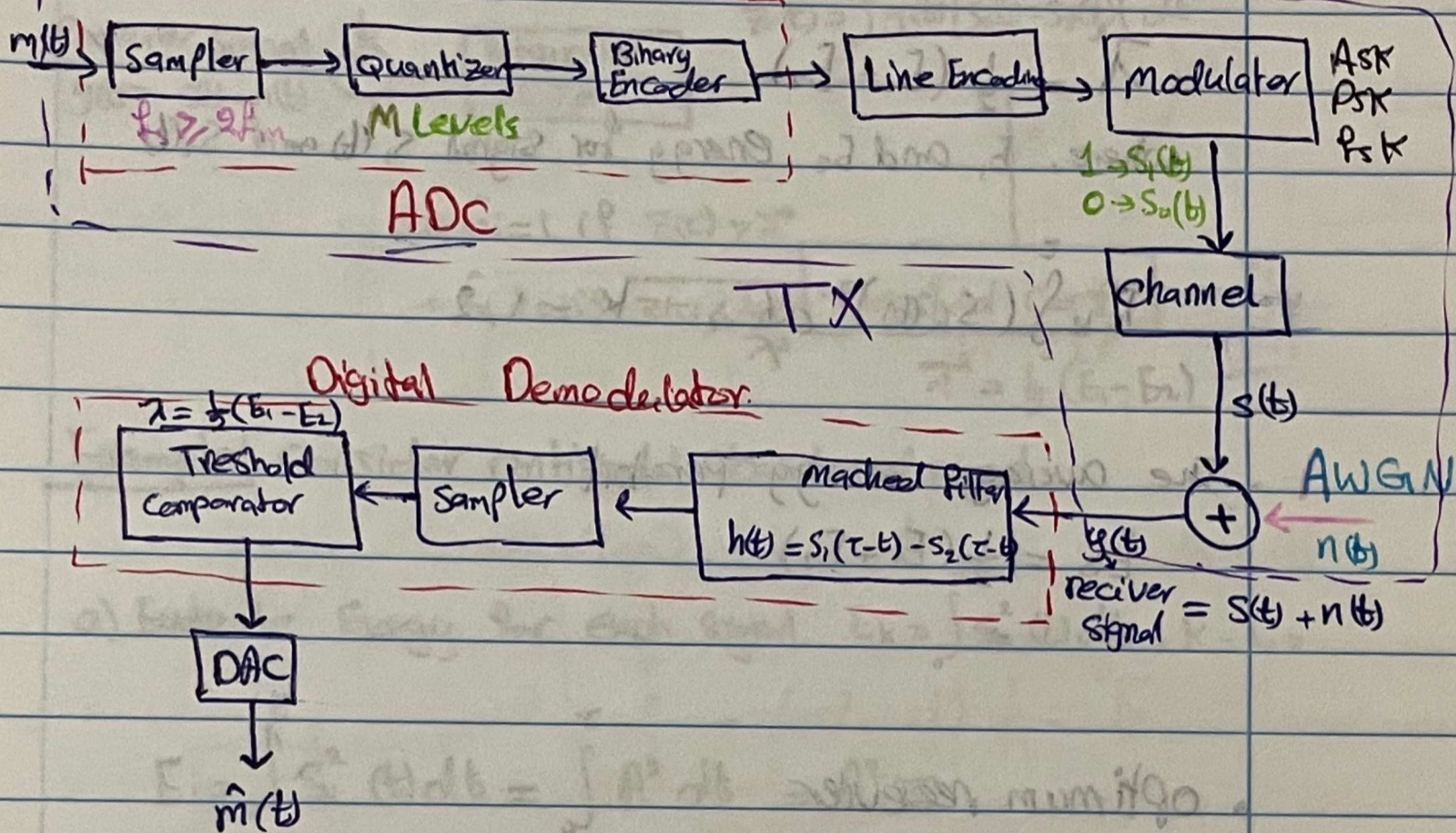


• Manchester Code.



(L19)

Optimum Receiver and Digital Binary Transmitter

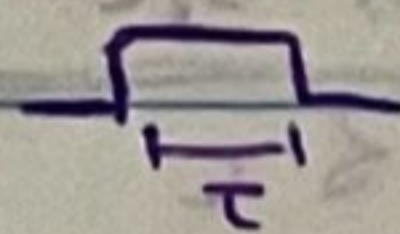


[Digital Communication System]

• Probability of error.

$$P_b^* \equiv P_e \equiv Q \left(\sqrt{\frac{\int (s_1(t) - s_2(t))^2 dt}{2N_0}} \right)$$

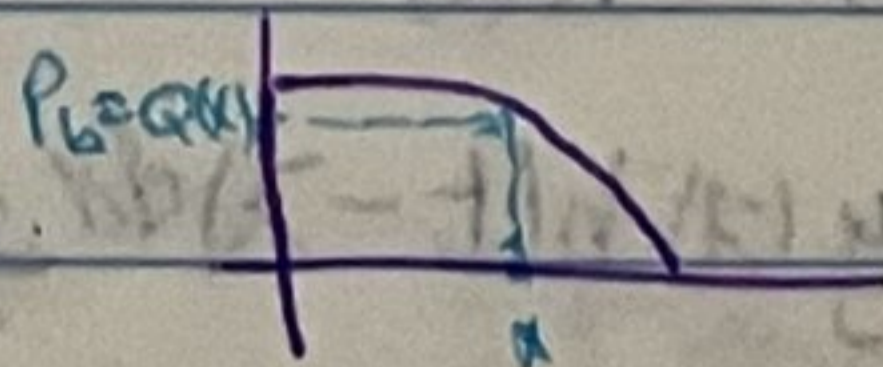
τ : bit duration



$\frac{1}{\tau}$: bit rate (R_b) or data rate.

N_0 : thermal noise.

$Q(x)$: Q function.



• Optimum Threshold of Comparator.

$$\lambda^* = \frac{1}{2} (E_1 + E_2)$$

where, E_1 and E_2 energy for signal $S_1(t)$ and $S_2(t)$

$$E_k = \int_0^T (S_k(t))^2 dt, \quad k = 1, 2$$

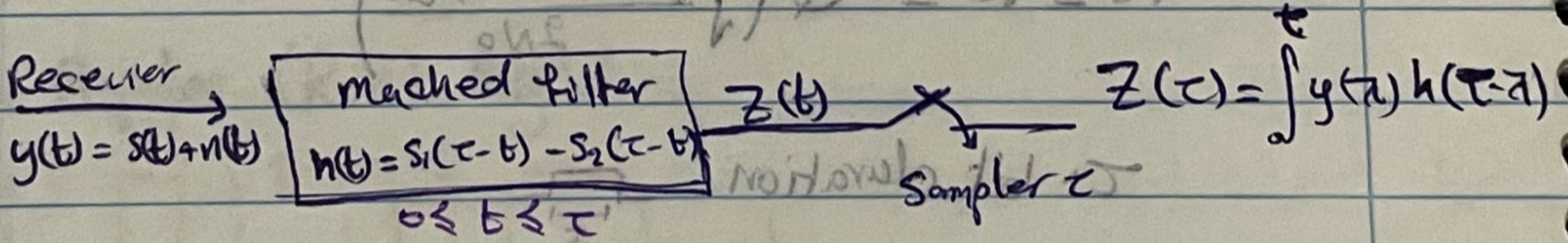
The average energy per bit

$$E_b = \frac{1}{2} (E_1 + E_2)$$

• optimum receiver

- ↳ matched filter
- ↳ correlator

→ by matched filter.



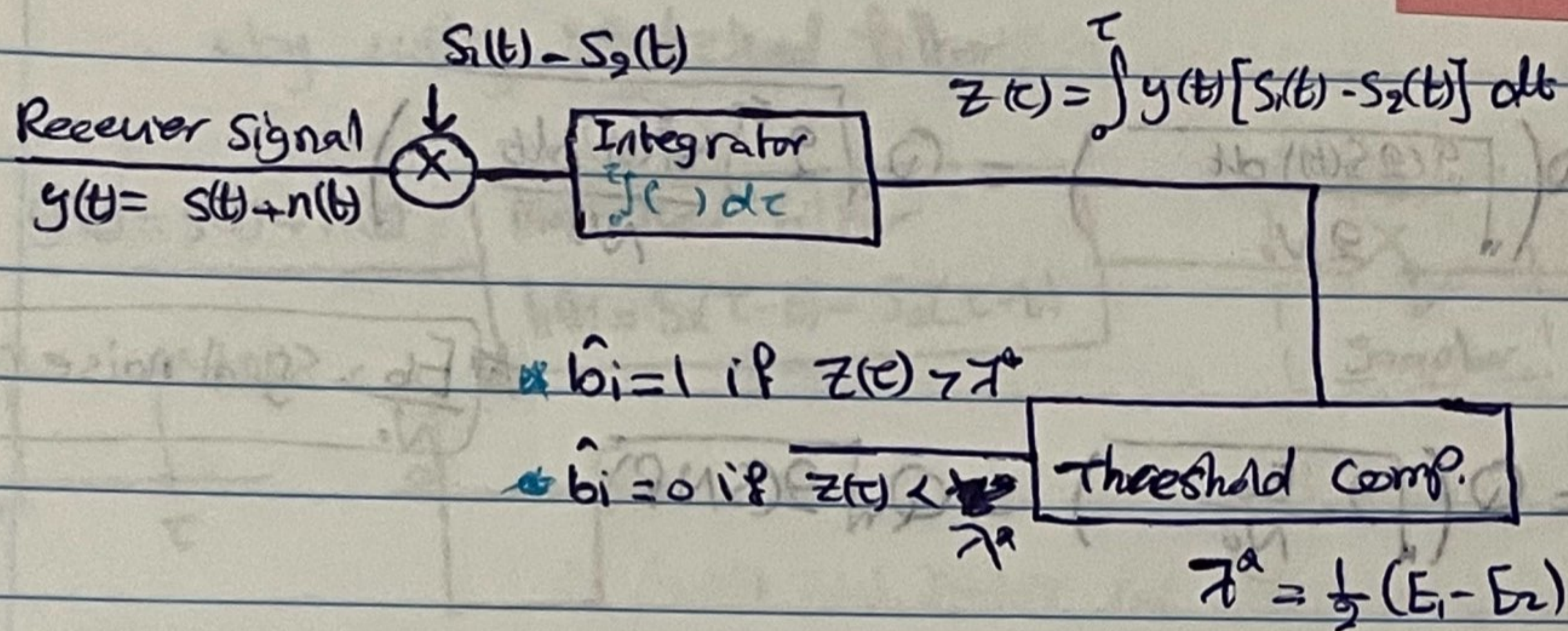
$$z(t) = y(t) * h(t)$$

$$z(t) = \int_0^t y(\tau) h(t-\tau) d\tau \quad \rightarrow \quad z(\tau) = \int_0^\tau y(t) h(\tau-t) dt$$

$$z(\tau) = \int_0^\tau y(t) [s_1(t) - s_2(t)] dt$$

anti-podal
 $s(t) = A, 0 \leq t \leq \tau$
 $s_2(t) = -A, 0 \leq t \leq \tau$
 $\Rightarrow s(t) = -s_2(t)$

or equivalently: [Correlator]



Example Consider antipodal baseband signal

a) Evaluate Energy for each signal. $E_k = \int_0^{\tau} s_k^2(t) dt, k=1,0$

$$E_1 = \int_0^{\tau} s_1^2(t) dt = \int_0^{\tau} A^2 dt = A^2 \tau$$

$$E_2 = \int_0^{\tau} s_2^2(t) dt = \int_0^{\tau} (-A)^2 dt = A^2 \tau$$

b) Evaluate the average of energy (average energy per bit).

$$E_{Avg} = \frac{E_1 + E_2}{2} = \frac{A^2 \tau + A^2 \tau}{2}$$

$$E_{Avg} = A^2 \tau = E_b$$

c) Evaluate the P_b^*

$$P_b^* = Q\left(\sqrt{\frac{\int_0^{\tau} (s_1(t) - s_2(t))^2 dt}{2N_0}}\right) = Q\left(\sqrt{\frac{\int_0^{\tau} (2s_1(t))^2 dt}{2N_0}}\right)$$

Since we have antipodal signal $\Rightarrow S_1(t) = -S_2(t)$

$$= Q\left(\sqrt{\frac{\int 2S(t) dt}{2N_0}}\right) = Q\left(\sqrt{2 \int \frac{S_1^2(t) dt}{N_0}}\right)$$

$$P_b^* = Q\left(\sqrt{2 \frac{E_b}{N_0}}\right) = Q\left(\sqrt{2(\text{SNR})}\right)$$

$\frac{E_b}{N_0}$ - Signal noise ratio

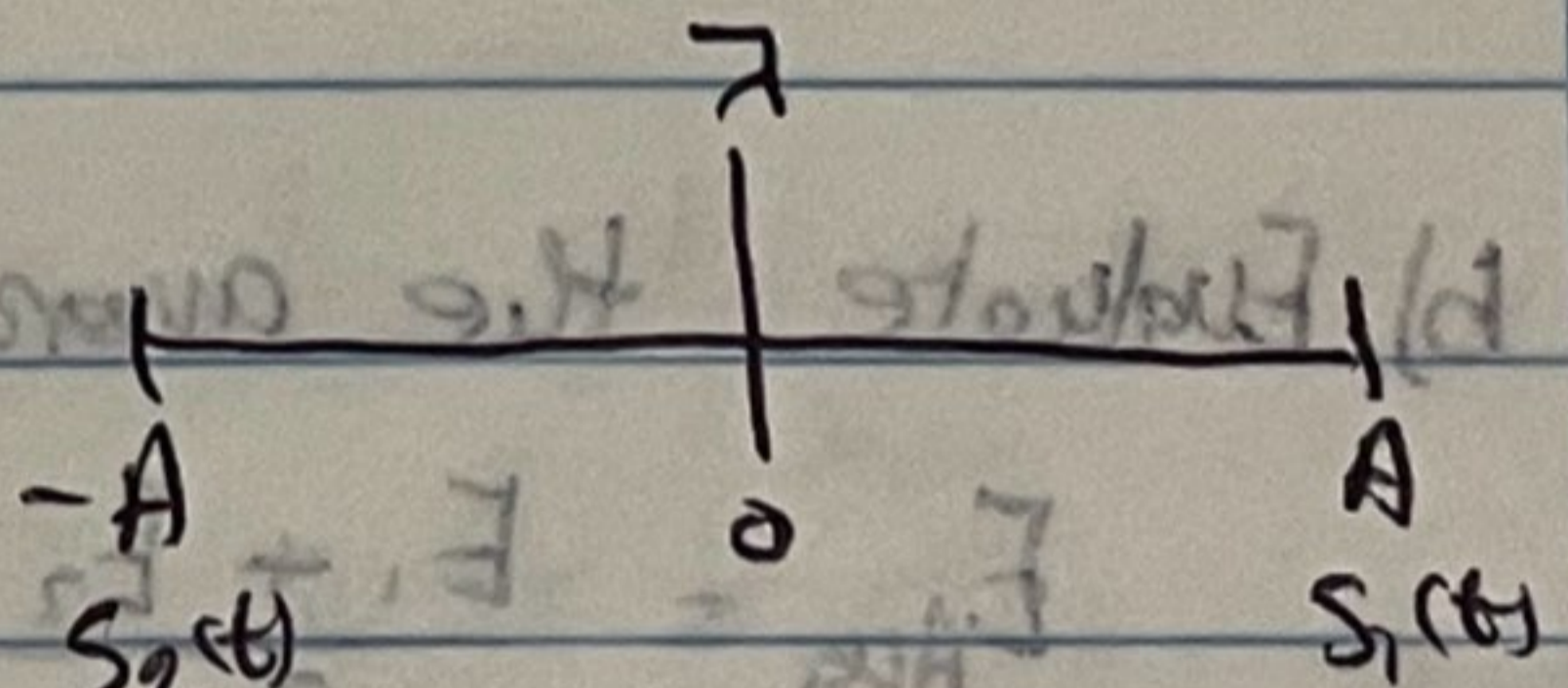
d) Evaluate the threshold Comparison.

$$\tau^* = \frac{1}{2} (E_1 - E_2) ; E_1 = E_2$$

$$\Rightarrow \tau^* = \text{zero}$$

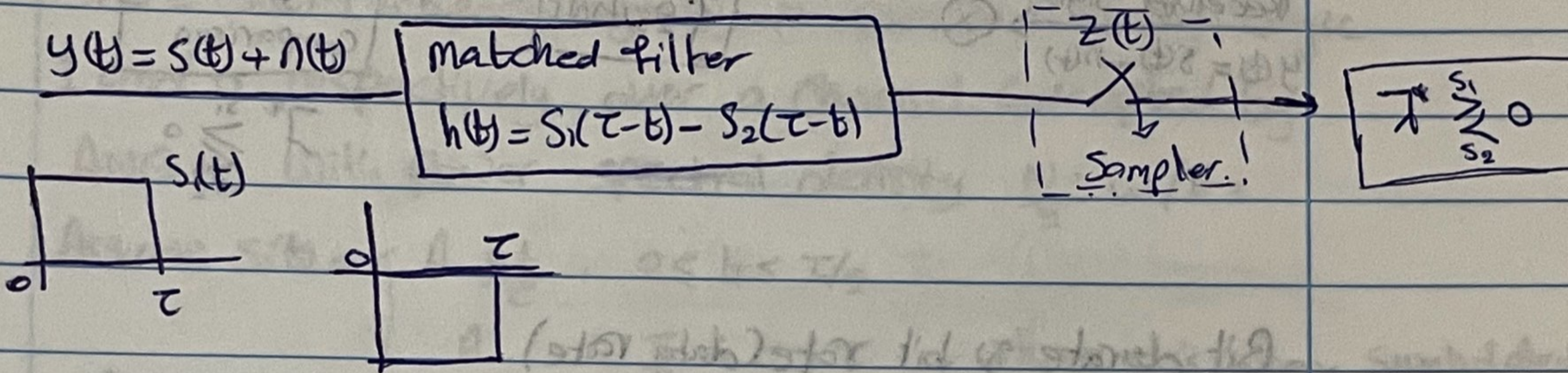
$$\rightarrow \hat{b}_i = 1 \Rightarrow Z(t) > 0$$

$$\rightarrow \hat{b}_i = 0 \Rightarrow Z(t) < 0$$

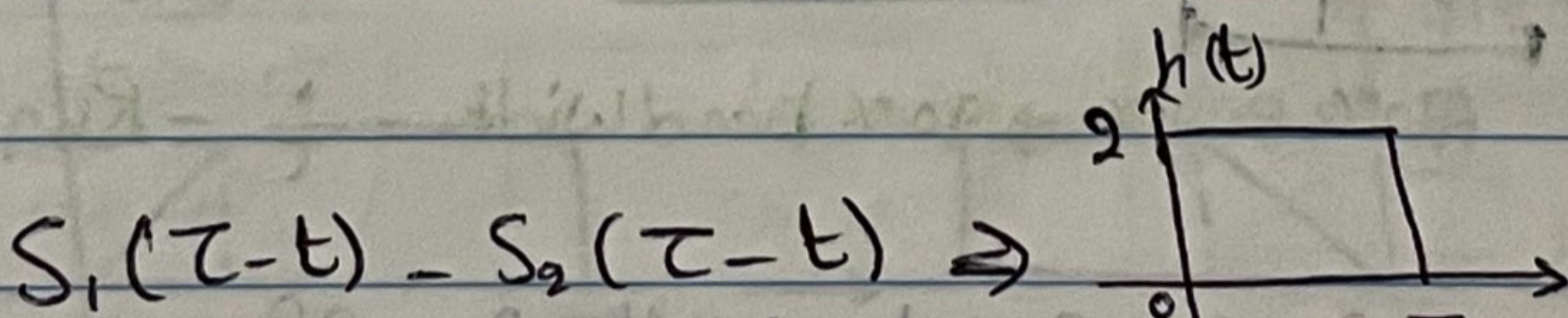
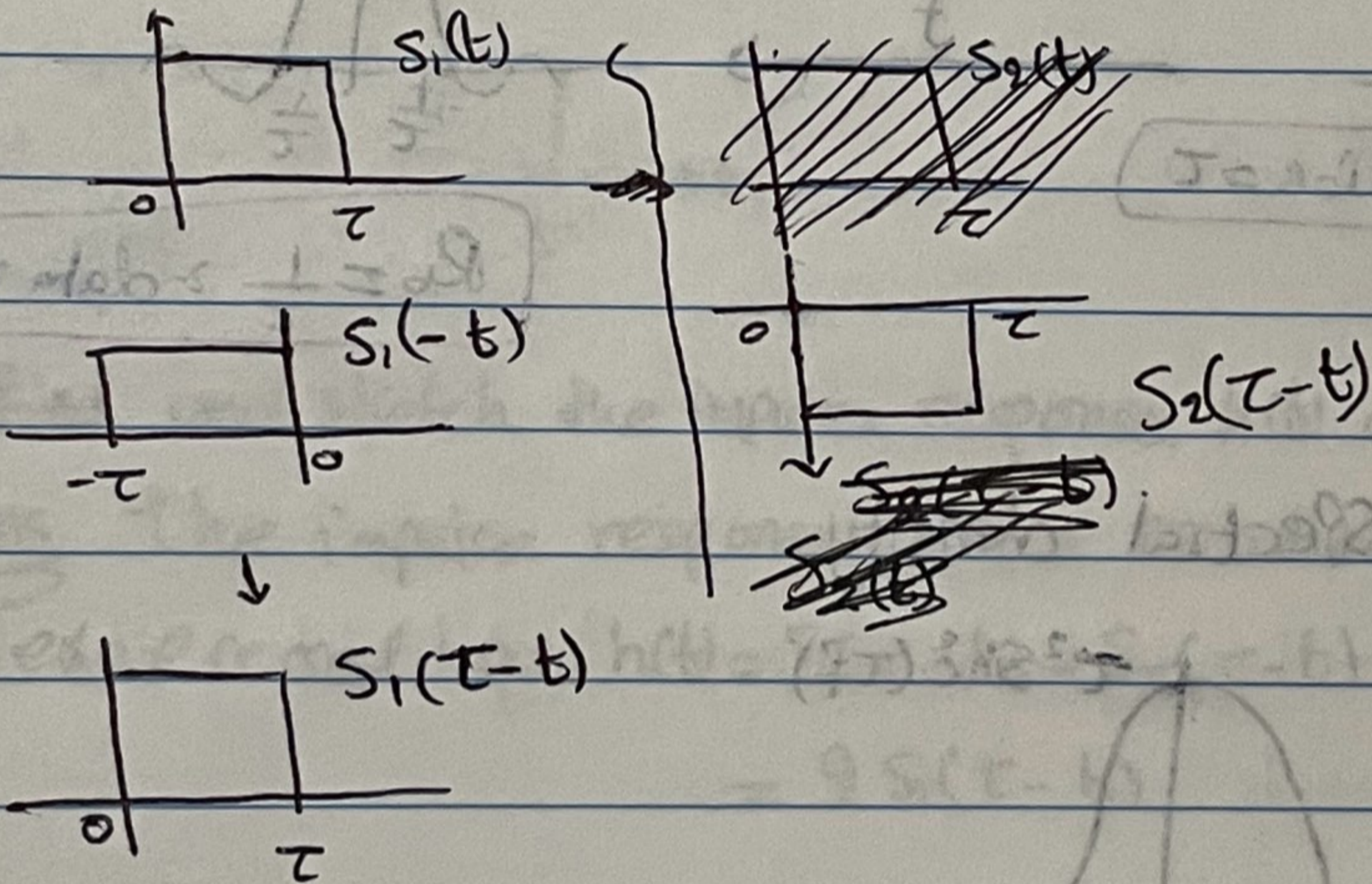


e) Implement optimum Receiver

- by using matched filter.



- Evaluate $h(t)$.



• By using Correlator:

$$s_1(t) - s_2(t) = 2s(t)$$

Received signal
 $y(t) = s(t) + n(t)$



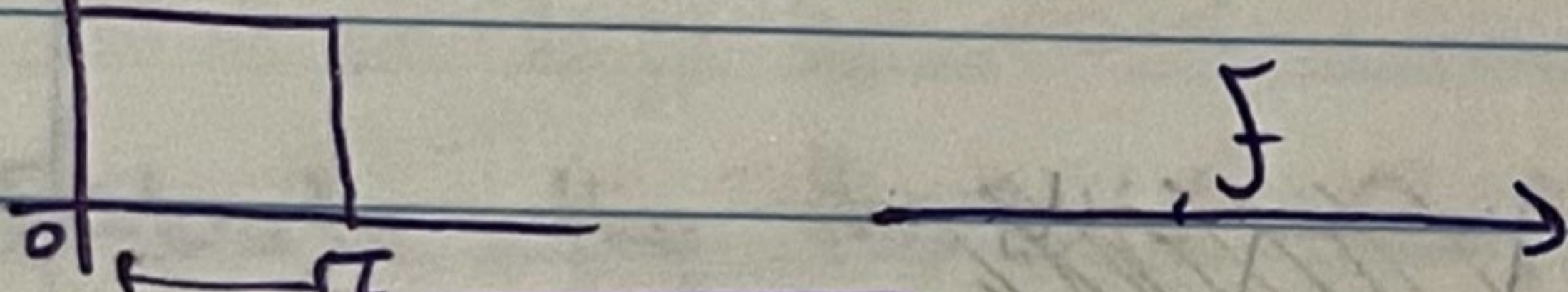
$$\int_0^T 2s_1(t) dt$$

Threshold Comparison

$$\int_0^T \sum_{s_1}^0$$

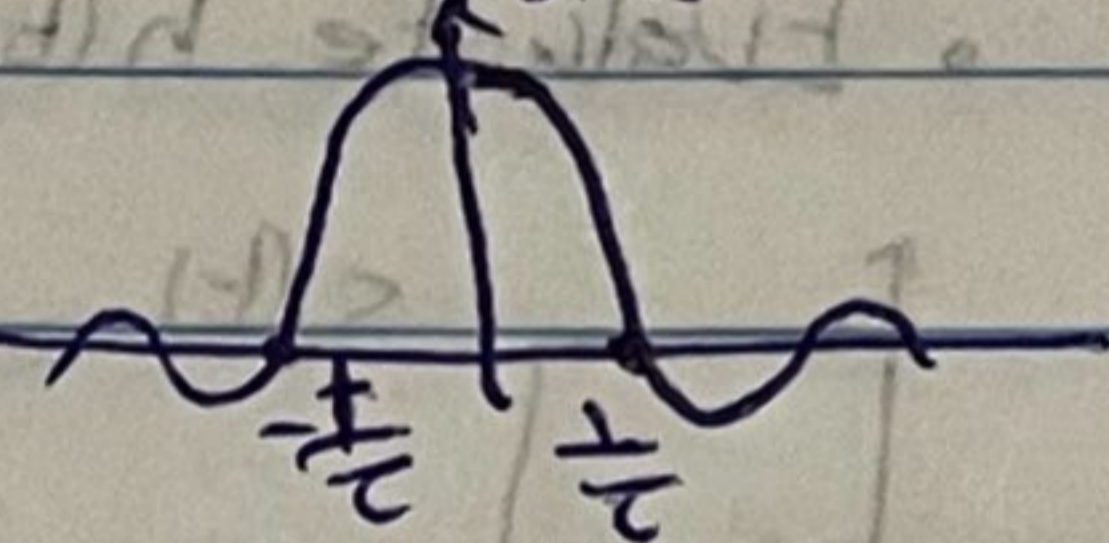
• Bit duration & bit rate (data rate)

$$s_1(t) = \pi \left(\frac{t}{T} \right)$$



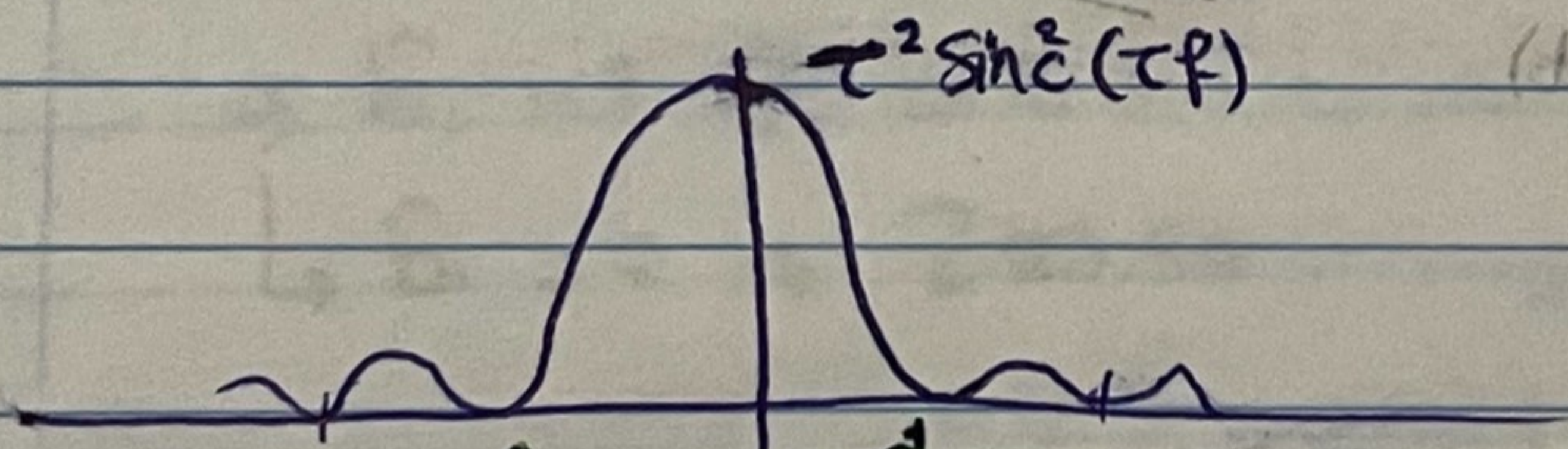
• bit duration = T

$$S_1(f) = \text{sinc}(\tau f)$$



$R_b = \frac{1}{T}$ = data rate

Power Spectral density



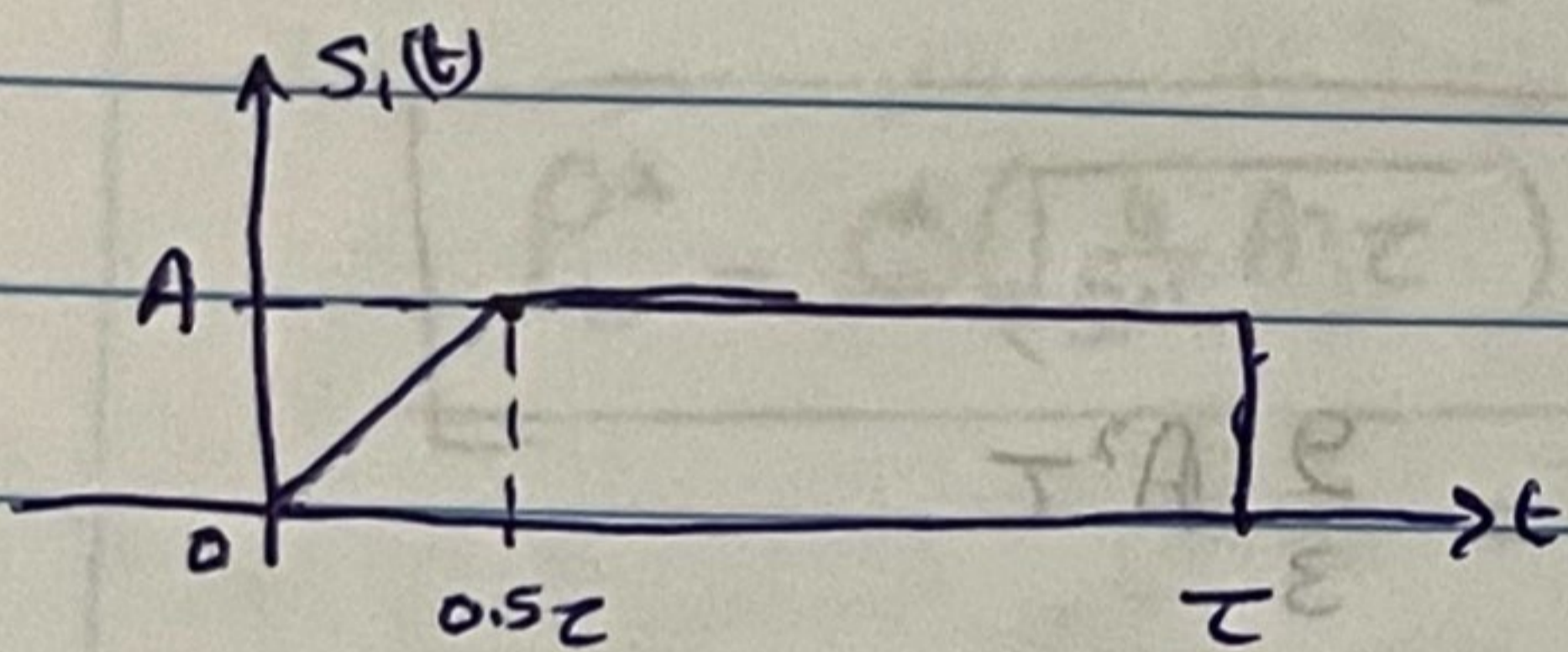
90% power \Rightarrow 90% bandwidth = $\frac{1}{T} = R_b$

95% power \Rightarrow 95% bandwidth = $\frac{2}{T} = 2R_b$

(Q20)

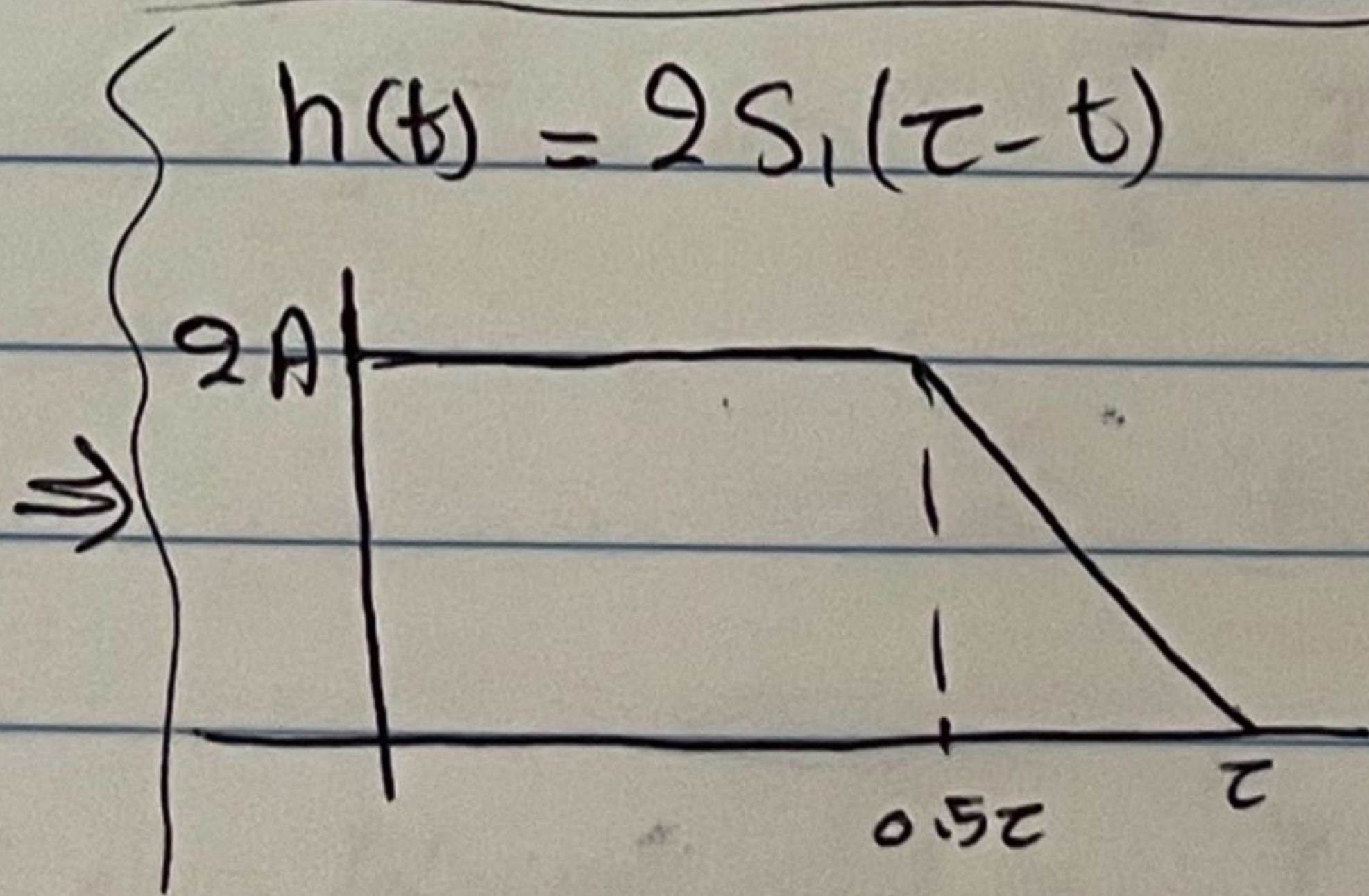
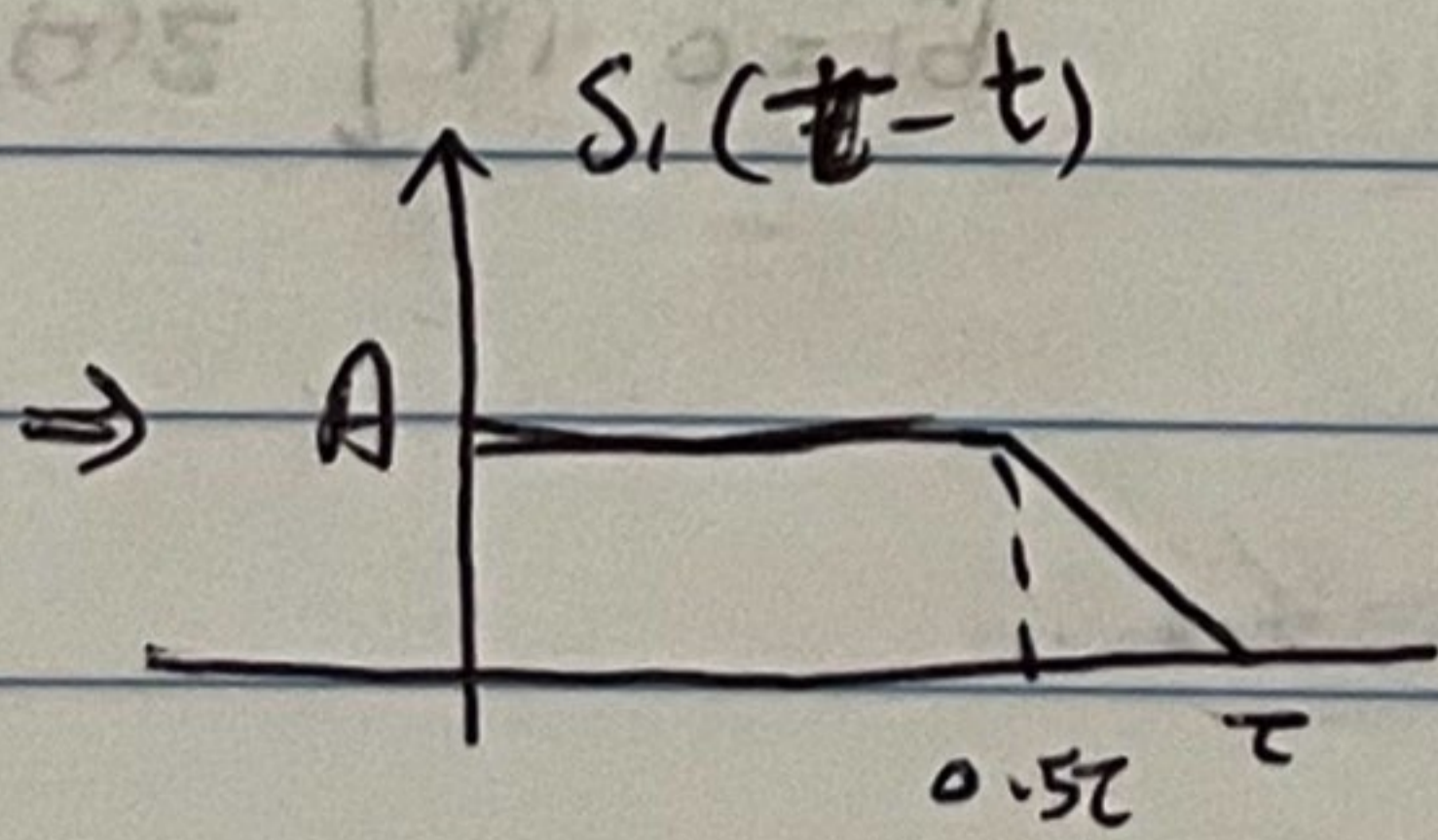
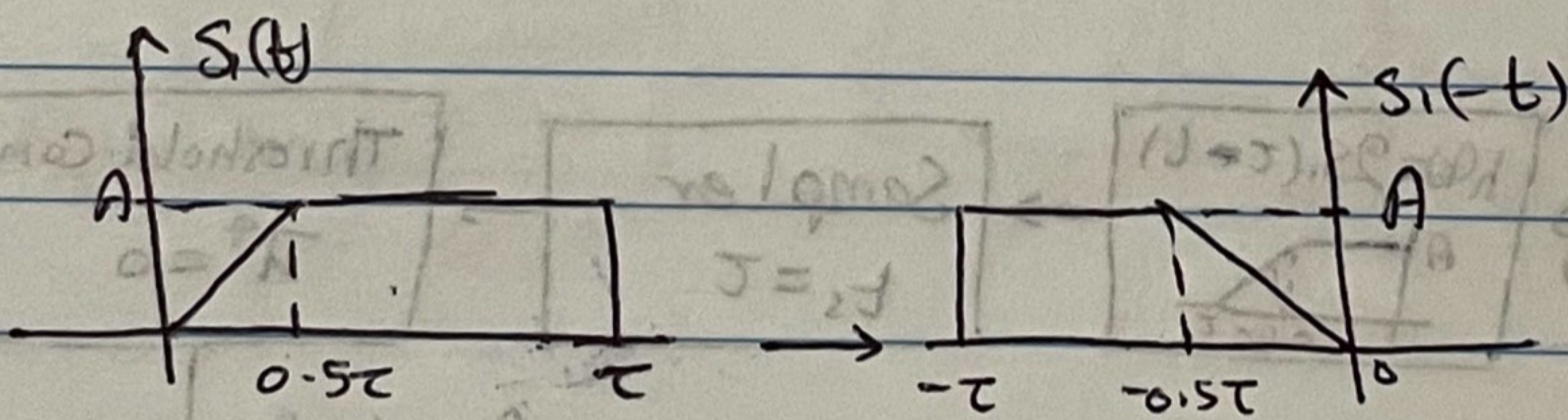
Example | The binary digital communication signal scheme, employs the following two equally probable signals $S_1(t)$ and $S_2(t) = -S_1(t)$ [antipodal signals], to represent binary logic 1 and 0 respectively over a channel corrupted by AWGN with power spectral density $\frac{N_0}{2}$ W/Hz.

Assume $S_1(t) = \begin{cases} A \cdot \frac{2t}{\tau} & , 0 \leq t \leq \tau/2 \\ A & , \tau/2 \leq t \leq \tau \end{cases}$, where τ is binary symbol duration



a) Find and sketch the impulse response, $h(t)$ of the matched filter

Ans The impulse response of the matched filter can be expressed as $h(t) = S_1(\tau - t) - S_2(\tau - t)$
 $= 2S_1(\tau - t)$



b) Find the optimum threshold used at the receiver

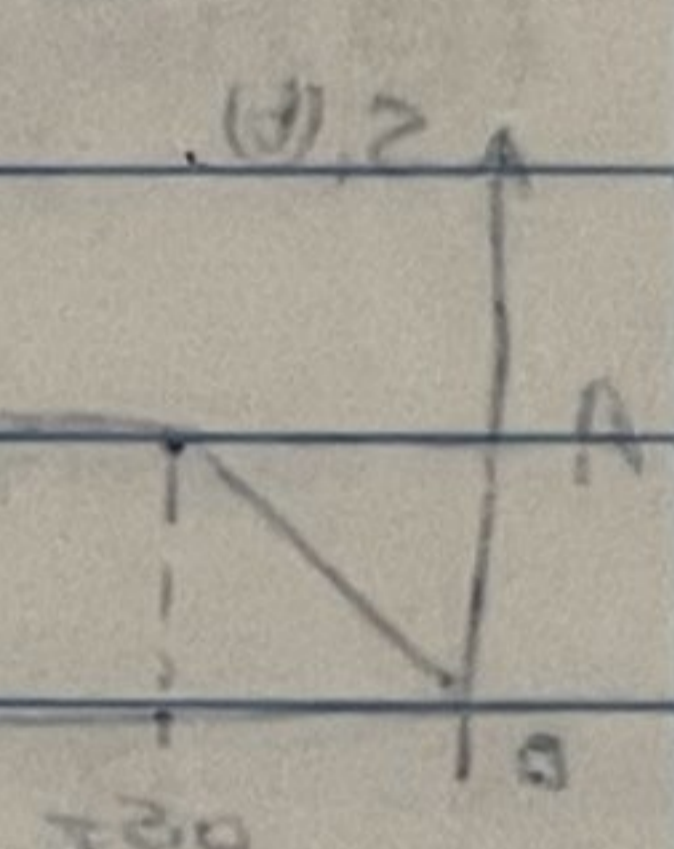
$$\tau^* = \frac{1}{2} (E_1 - E_2)$$

$$E_1 = \int_0^{\tau} s_1^2(t) dt = \int_0^{0.5\tau} \left(\frac{2A}{\tau}\right)^2 t^2 dt + \int_{0.5\tau}^{\tau} A^2 dt$$

$$= \frac{4A^2}{\tau^2} \left(\frac{\tau}{2}\right)^3 + A^2 \frac{\tau}{2}$$

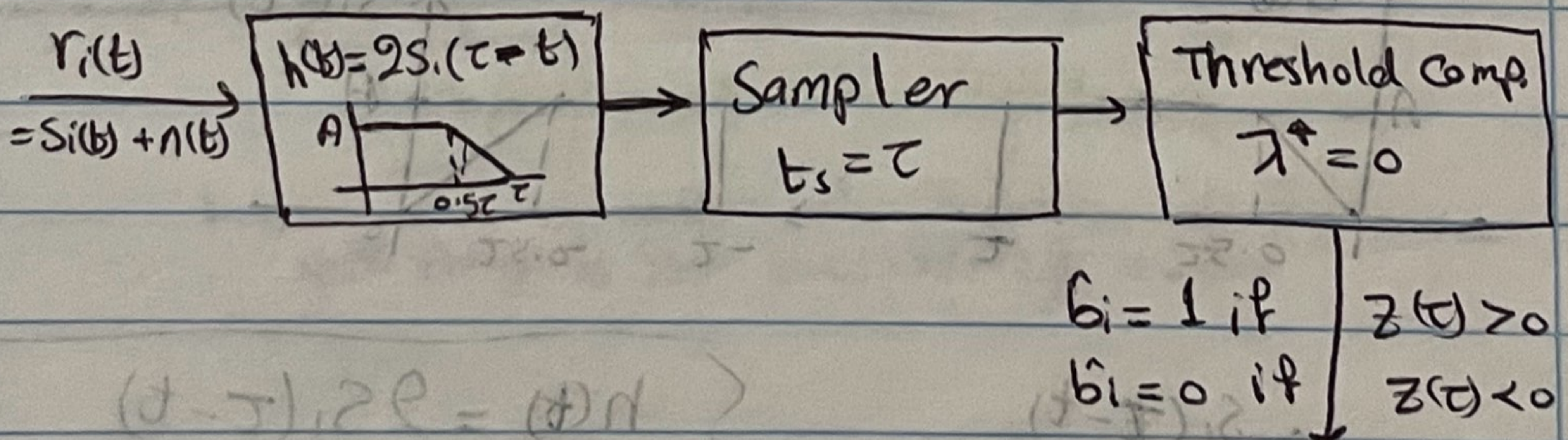
$$E_1 = \frac{2}{3} A^2 \tau = E_2$$

$$E_b = \frac{1}{2} [E_1 + E_2] = E_1 = \frac{2}{3} A^2 \tau$$



$$\Rightarrow \tau^* = 0$$

c) sketch the optimum receiver highlighting its basic components.



d) Evaluate the minimum prob. of error.

$$P_b^* = Q\left(\sqrt{\frac{\int (s_1(t) - s_2(t))^2 dt}{2N_0}}\right) = Q\left(\sqrt{\frac{\int (2s_1(t))^2 dt}{2N_0}}\right)$$

$$= Q\left(\sqrt{\frac{4 \int s_1^2(t) dt}{2N_0}}\right) = Q\left(\sqrt{\frac{2 E_b}{N_0}}\right)$$

$$P_b^* = Q\left(\sqrt{\frac{2}{N_0} \cdot \frac{2}{3} A^2 T}\right)$$

$$P_b^* = Q\left(\sqrt{\frac{4}{3N_0} A^2 T}\right)$$

≡ Binary Digital Bandpass Modulation

↳ ASK: Amplitude Shift Keying

↳ PSK: Phase Shift Keying

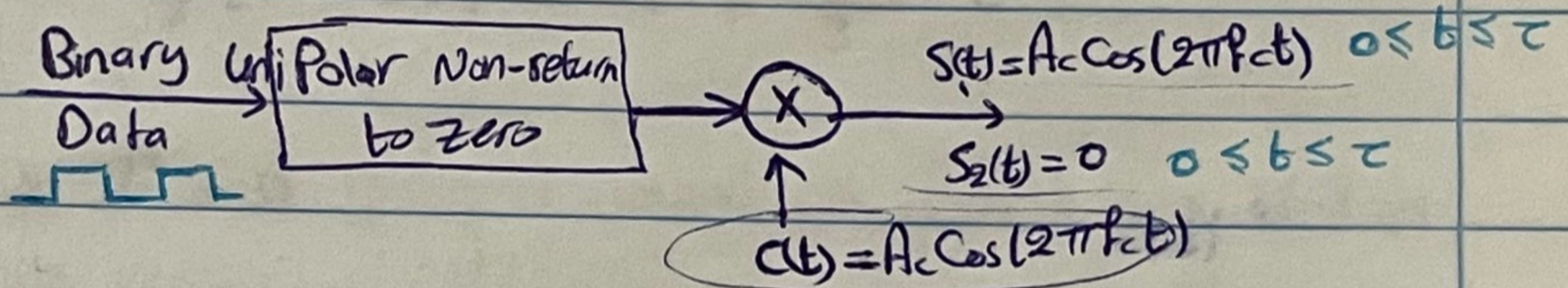
↳ FSK: Freq " " " "

= Amplitude Shift Keying (ASK):

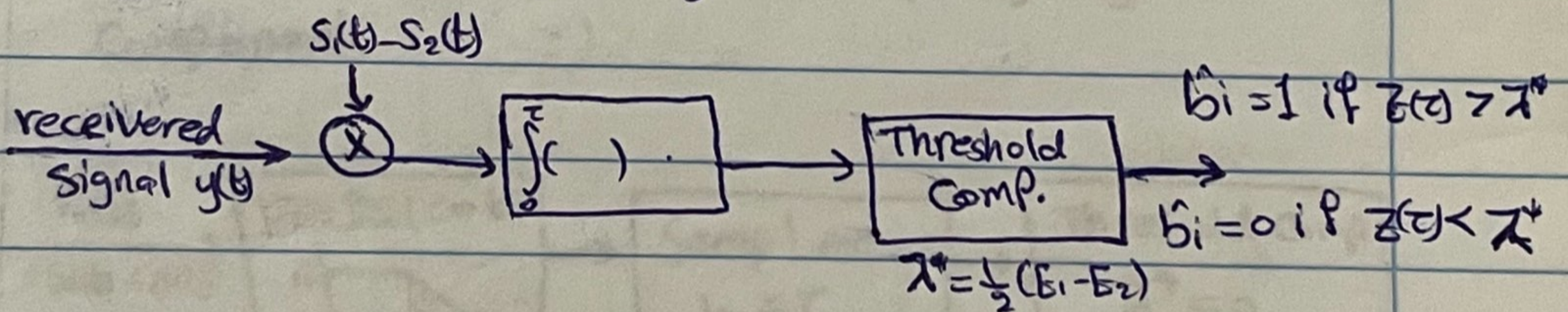
• Signal Representation

bit 1 $\rightarrow S_1(t) = A_c \cos(2\pi f_c t)$ $0 \leq t \leq \tau$

bit 0 $\rightarrow S_2(t) = 0$ $0 \leq t \leq \tau$



Optimum Receiver by using Correlator.



where

$$E_1 = \int_0^{\tau} S_1^2(t) dt = \int_0^{\tau} A_c^2 \cos^2(2\pi f_c t) dt = \int_0^{\tau} \left[\frac{A_c^2}{2} + \frac{A_c^2}{2} \cos(4\pi f_c t) \right] dt$$

$$E_1 = \frac{A_c^2}{2} \tau$$

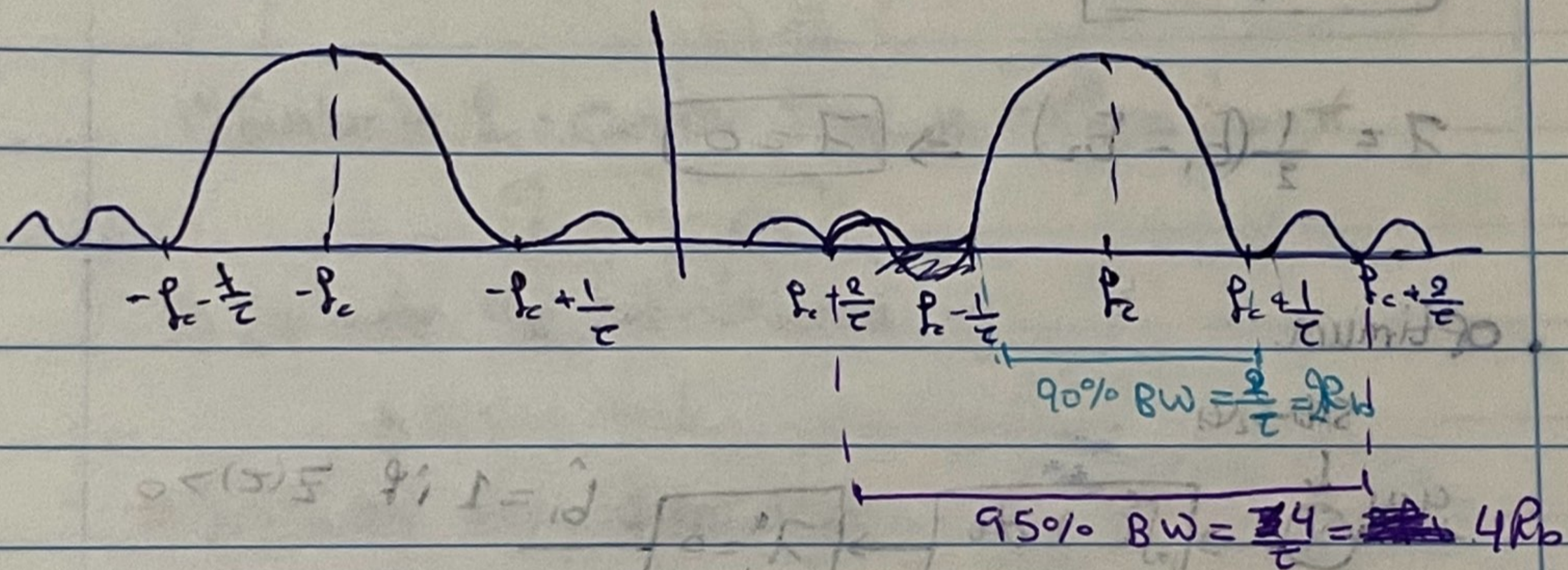
$$E_2 = 0 \text{ [No signals]} \Rightarrow \lambda^* = \frac{1}{4} A_c^2 \tau = E_b$$

$$\Rightarrow P_b^* = Q\left(\sqrt{\frac{\int (S_1(t) - S_2(t))^2 dt}{2 N_0}}\right) = Q\left(\sqrt{\frac{\int S_1^2(t) dt}{2 N_0}}\right)$$

$$= Q\left(\sqrt{\frac{E_b}{2 N_0}}\right) = Q\left(\sqrt{\frac{A^2 \tau}{4 N_0}}\right)$$

$$P_b^* = Q\left(\sqrt{\frac{E_b}{N_0}}\right)$$

• Power Spectral density.

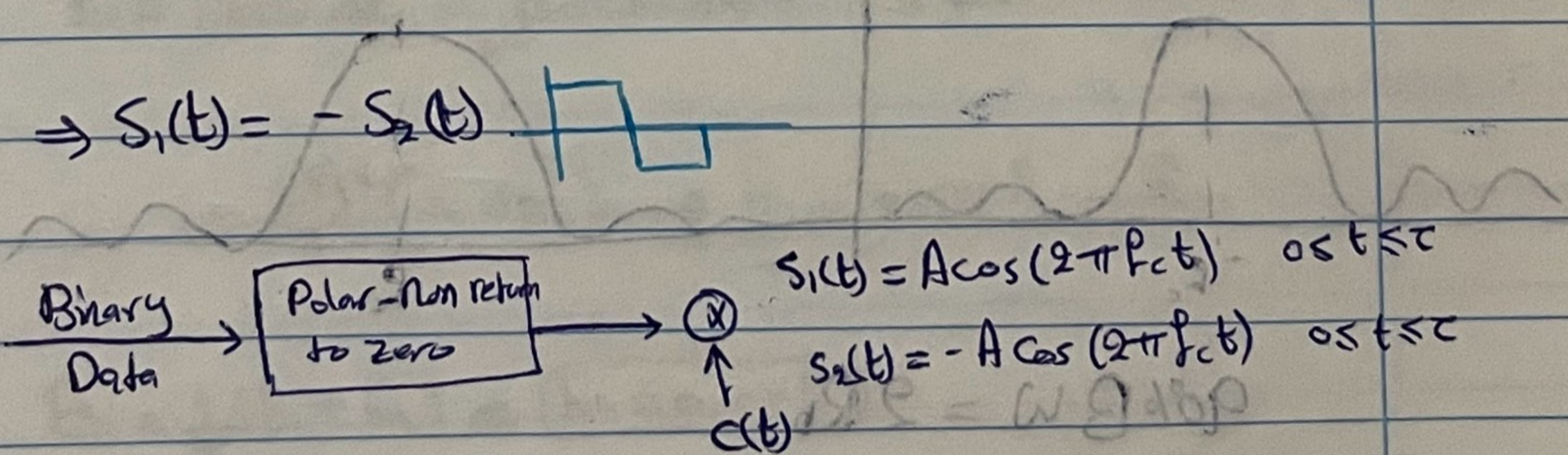


= Binary phase shift keying (BPSK).

bit 1 $\Rightarrow S_1(t) = A \cos(2\pi f_c t)$

bit 0 $\Rightarrow S_2(t) = A \cos(2\pi f_c t + \pi) = -A \cos(2\pi f_c t)$

$$\Rightarrow S_1(t) = -S_2(t)$$



$$E_1 = \int_0^T s_1^2(t) dt = \int_0^T A^2 \cos^2(2\pi f_c t) dt$$

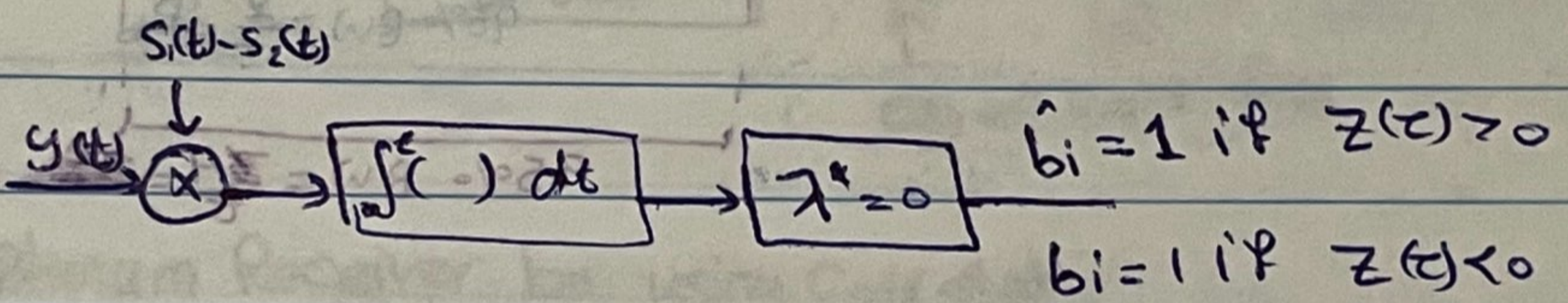
$$E_1 = \frac{A^2 T}{2}$$

$$E_2 = \int_0^T s_2^2(t) dt = \int_0^T A^2 \cos^2(2\pi f_c t) dt$$

$$E_2 = \frac{A^2 T}{2}$$

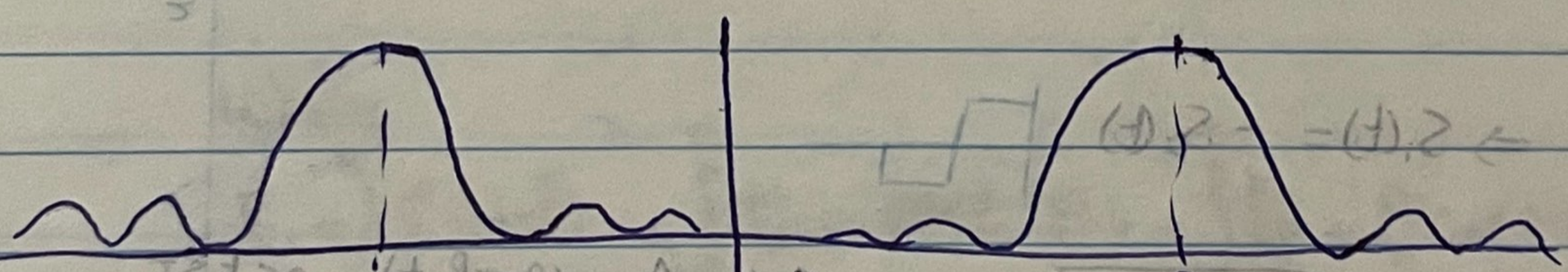
$$\gamma = \frac{1}{2}(E_1 - E_2) \Rightarrow \gamma = 0$$

• optimum.



$$P_b^* = Q\left(\sqrt{\frac{A^2 T}{N_0}}\right) \Rightarrow P_b^* = Q\left(\sqrt{\frac{2E_b}{N_0}}\right)$$

• Power Spectral density



$$90\% BW = 2 R_b$$

$$95\% BW = 4 R_b$$

Example Binary Phase Shift Keying modulation scheme. Employ the following two equally probable signals $s_1(t)$ and $s_2(t)$ to represent binary logic 1 and 0 respectively, over a channel corrupted by AWGN with power spectral density $\frac{N_0}{2} = 0.5 \times 10^{-4} \text{ W/Hz}$.

$$s_1(t) = \begin{cases} 2 \cos(2000\pi t), & 0 \leq t \leq 0.001 \\ 0, & \text{o.w.} \end{cases}$$

1) Evaluate f_c : Carrier freq. $\Rightarrow 2\pi f_c = 2000\pi$

$$\boxed{f_c = 1000}$$

2) Evaluate the bit duration.

$$\Rightarrow \tau = 0.001$$

3) Evaluate the data rate.

$$R_b = \frac{1}{\tau} = \frac{1}{0.001} \Rightarrow \boxed{R_b = 1000}$$

4) Evaluate the avg energy per bit.

$$E_1 = \int_0^{\tau} s_1^2(t) dt = \int_0^{\tau} (2 \cos(2000\pi t))^2 dt$$

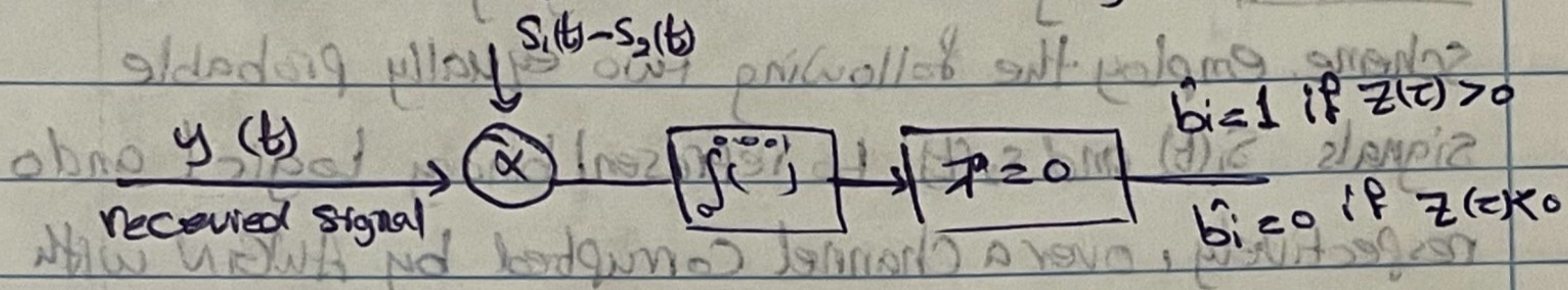
$$= \frac{(2)^2}{2} (0.001) \Rightarrow E_1 = 0.002 = E_2$$

$$E_b = \frac{1}{2} (E_1 + E_2) \Rightarrow \boxed{E_b = 0.002}$$

5) Evaluate the optimum threshold.

$$\gamma^* = \frac{1}{2} (E_1 - E_2) \Rightarrow \gamma^* = 0 \rightarrow$$

6) sketch the optimum receiver using ~~matched filter~~ ^{Correlator.}



7) Evaluate the minimum prob. of error.

$$P_b^* = Q\left(\sqrt{\frac{\int_0^T 2s^2(t) dt}{2N_0}}\right) = Q\left(\sqrt{\frac{2 \int_0^T S^2(t) dt}{N_0}}\right)$$

$$P_b^* = Q\left(\sqrt{\frac{2E_b}{N_0}}\right) = Q\left(\sqrt{\frac{2(0.002)}{N_0}}\right)$$

$$= Q\left(\sqrt{\frac{0.004}{10^{-4}}}\right) \approx Q(6.32)$$

بطلع القيمة من جداول Q

* انا ما كانت القيمة موجودة باخذ القيمة اى كبر منها والقيمة اى اصغر واخذ الاكبر اهم